

OCRE-CTR-2012-25

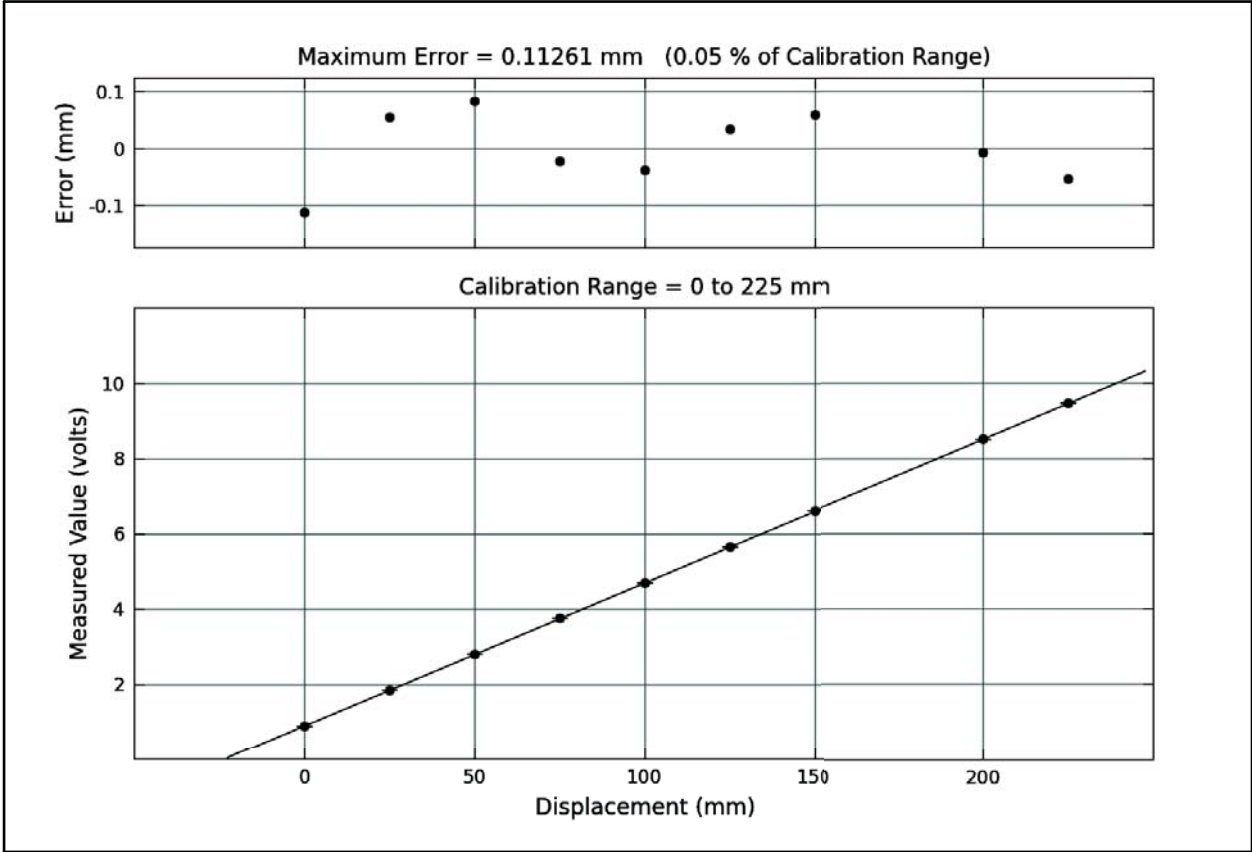
APPENDIX A
Instrumentation Calibration Information

JSS
Calibration of Sinkage
Calibrated 2012-05-31 11:10Z

Test Facility: CWT	Serial #: A56015	Filter Frequency: 10
Data Source: daspc49:50001 Channel 1	Programmable Gain:	Excitation: 10
Sensor Model: PT101-0010-111-1110	Plug-In Gain:	

Data Point #	Physical Value (mm)	Measured Value (volts)	Fitted Curve Value (mm)	Error (mm)	Definition of Calibration Curve
1	0.0000	0.89254	-0.11261	-0.11261	
2	25.000	1.8502	25.056	0.055555	
3	50.000	2.8026	50.084	0.083767	
4	75.000	3.7498	74.977	-0.022728	
5	100.00	4.7005	99.962	-0.037969	
6	125.00	5.6546	125.03	0.034499	
7	150.00	6.6068	150.06	0.059648	
8	200.00	8.5069	199.99	-0.0067488	
9	225.00	9.4564	224.95	-0.053413	

Polynomial Degree = 1 (Linear Fit)
 $Y = C_0 + C_1 \cdot V$
 where $Y(t)$ = Displacement (mm),
 $V(t)$ = measured value (volts),
 $C_0 = -23.569$ mm,
 $C_1 = 26.28$ mm/volt,

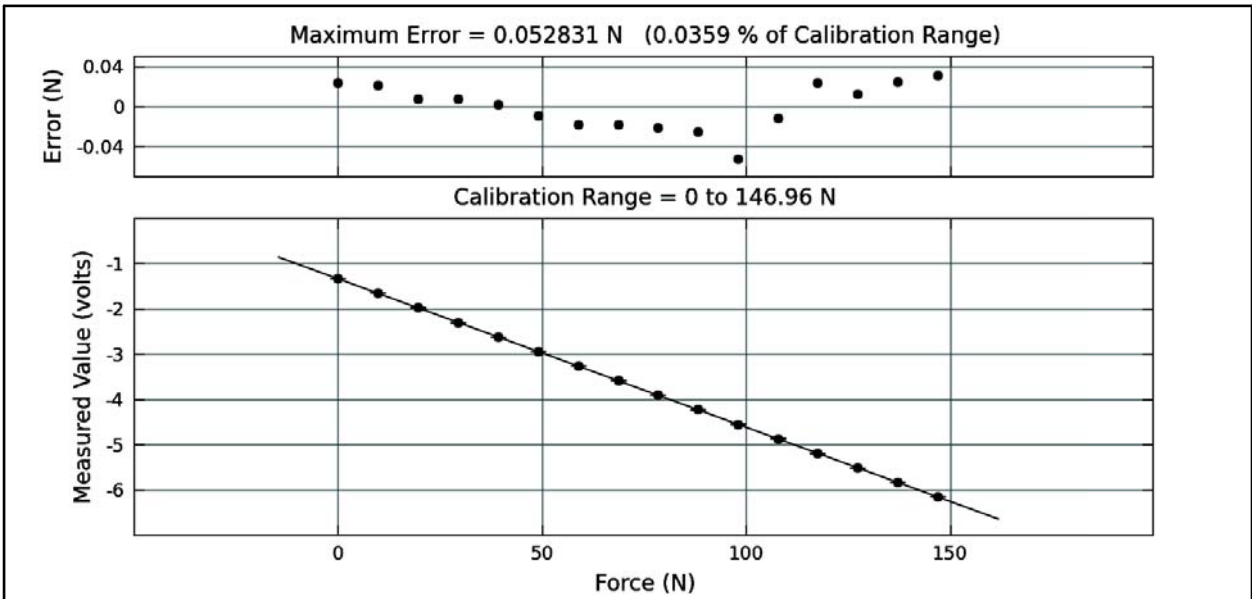


JSS
Calibration of Thrust
Calibrated 2012-05-18 15:25Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 2	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (N)	Measured Value (volts)	Fitted Curve Value (N)	Error (N)	Definition of Calibration Curve
1	0.0000	-1.3327	0.024033	0.024033	
2	9.8082	-1.6540	9.8298	0.021621	
3	19.616	-1.9749	19.624	0.0077156	
4	29.425	-2.2963	29.433	0.0079857	
5	39.234	-2.6175	39.236	0.0023079	
6	49.007	-2.9374	48.998	-0.0090418	
7	58.815	-3.2585	58.797	-0.017610	
8	68.623	-3.5799	68.605	-0.018216	
9	78.431	-3.9011	78.410	-0.021140	
10	88.240	-4.2224	88.215	-0.025588	
11	98.049	-4.5429	97.996	-0.052831	
12	107.73	-4.8614	107.72	-0.011190	
13	117.53	-5.1839	117.56	0.023531	
14	127.34	-5.5050	127.36	0.012640	
15	137.15	-5.8267	137.18	0.024478	

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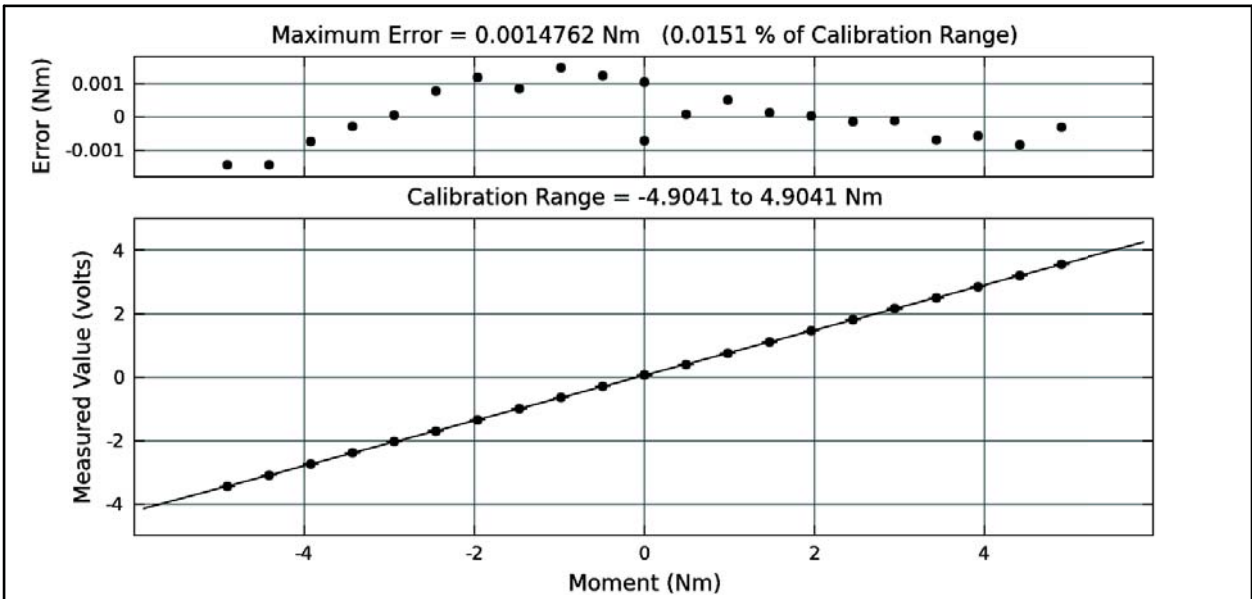


JSS
Calibration of Torque
Calibrated 2012-05-18 14:31Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: daspc49:50001 Channel 3	Programmable Gain:	Excitation: +/-15V
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (Nm)	Measured Value (volts)	Fitted Curve Value (Nm)	Error (Nm)	Definition of Calibration Curve
1	-4.9041	-3.4407	-4.9055	-0.0014364	
2	-4.4137	-3.0912	-4.4151	-0.0014571	
3	-3.9233	-2.7411	-3.9240	-0.00075121	
4	-3.4329	-2.3911	-3.4331	-0.00027909	
5	-2.9425	-2.0413	-2.9424	5.3042e-05	
6	-2.4520	-1.6912	-2.4513	0.00076318	
7	-1.9616	-1.3413	-1.9605	0.0011771	
8	-1.4712	-0.99192	-1.4704	0.00085123	
9	-0.98082	-0.64187	-0.97934	0.0014762	
10	-0.49041	-0.29245	-0.48918	0.0012321	
11	0.0000	0.057022	0.0010462	0.0010462	
12	0.0000	0.055761	-0.00072226	-0.00072226	
13	0.49041	0.40592	0.49047	6.2798e-05	
14	0.98082	0.75584	0.98133	0.00051009	
15	1.4712	1.1052	1.4713	0.00011274	

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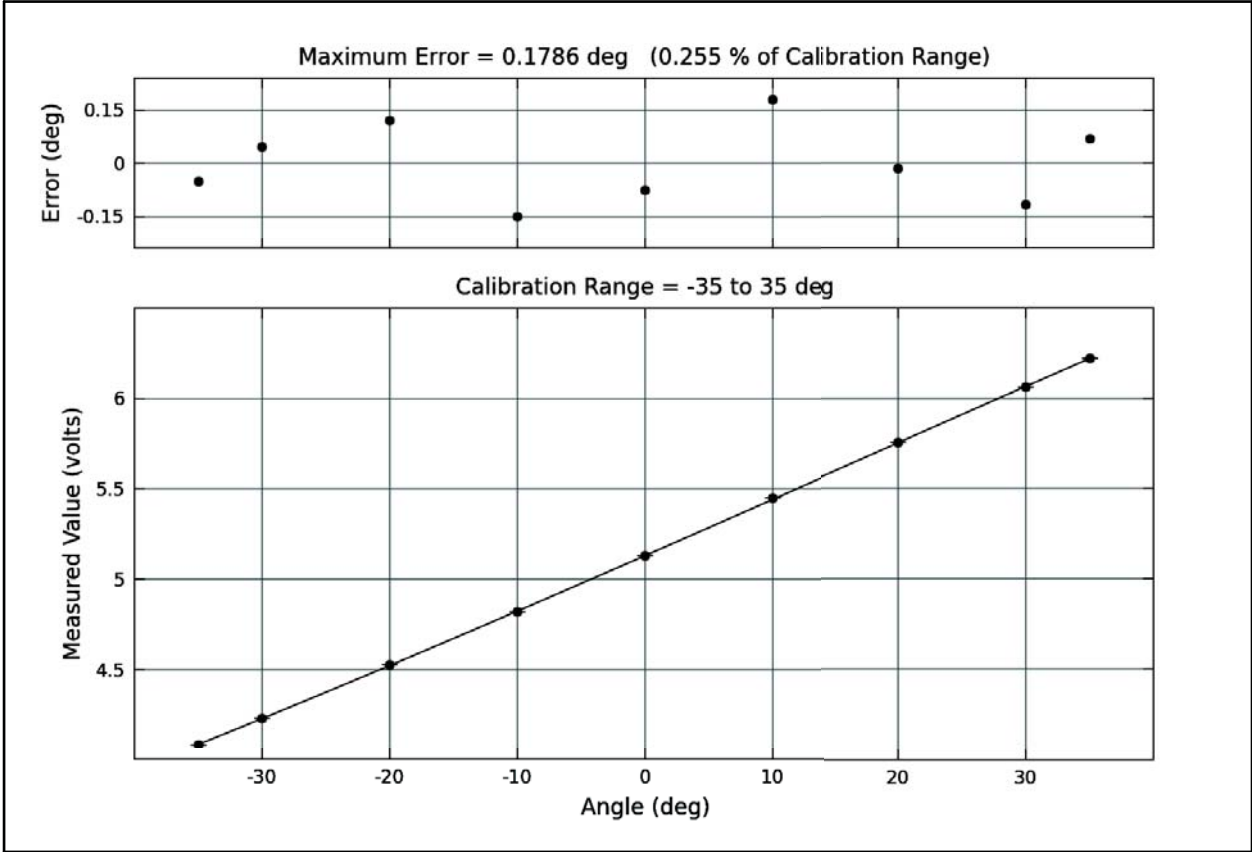
JSS

Calibration of Rudder Angle

Calibrated 2012-06-07 20:23Z

Test Facility: CWT	Serial #: 1392909	Filter Frequency: 10
Data Source: daspc49:50001 Channel 5	Programmable Gain:	Excitation:
Sensor Model: 60001A50-1000	Plug-In Gain: 496	

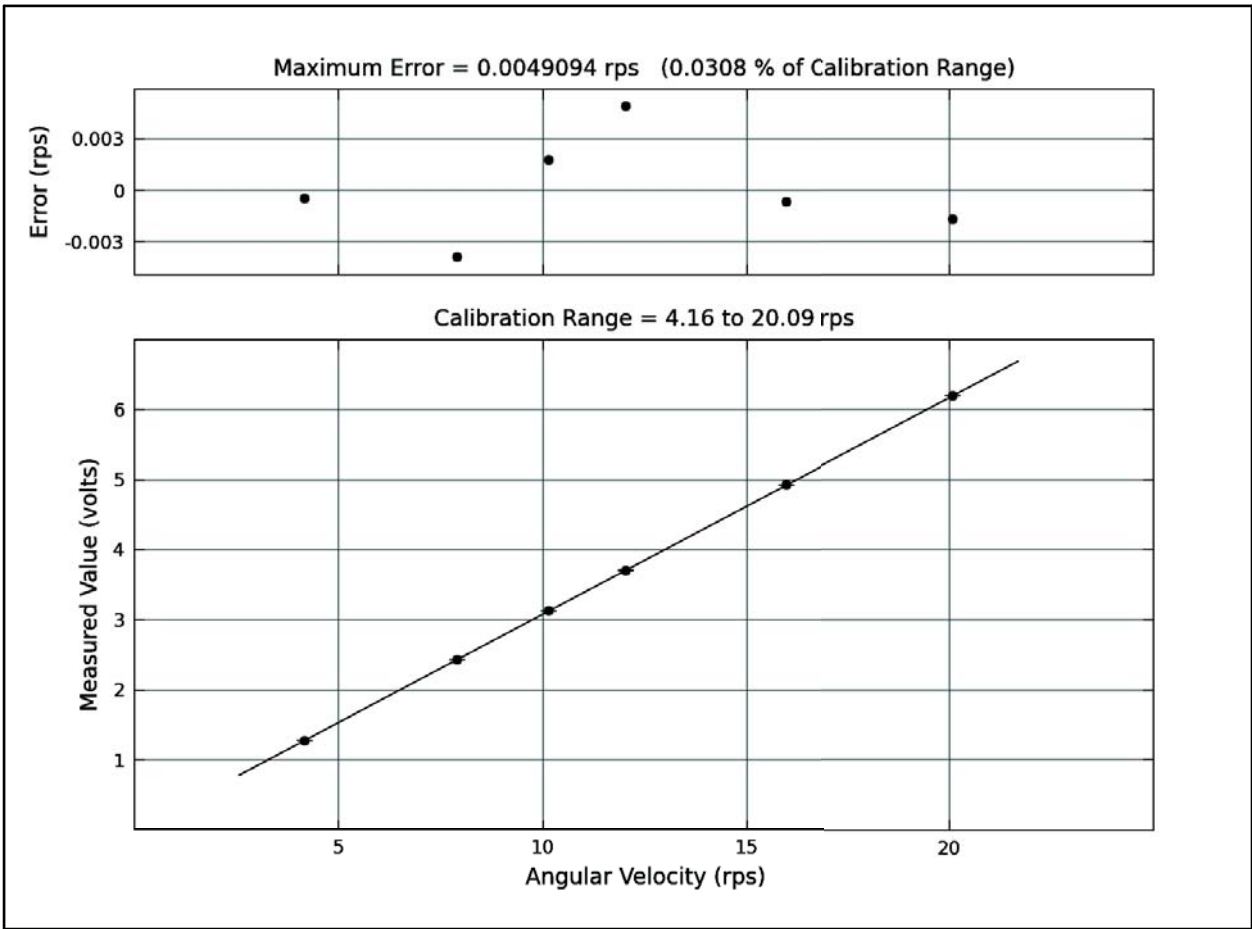
Data Point #	Physical Value (deg)	Measured Value (volts)	Fitted Curve Value (deg)	Error (deg)	Definition of Calibration Curve
1	-35.000	4.0837	-35.051	-0.051328	Polynomial Degree = 3 $Y = C_0 + \sum (C_i \cdot V^i)$ where $Y(t)$ = Angle (deg), $V(t)$ = measured value (volts), $C_0 = -240.2$ deg, $C_1 = 72.467$ deg/volt, $C_2 = -7.1774$ deg/volt ² , $C_3 = 0.42448$ deg/volt ³ ,
2	-30.000	4.2301	-29.956	0.044360	
3	-20.000	4.5261	-19.880	0.11982	
4	-10.000	4.8191	-10.150	-0.15000	
5	0.0000	5.1283	-0.076463	-0.076463	
6	10.000	5.4470	10.179	0.17860	
7	20.000	5.7532	19.984	-0.016094	
8	30.000	6.0614	29.884	-0.11609	
9	35.000	6.2217	35.067	0.067199	



JSS
Calibration of Shaft Speed
Calibrated 2012-05-25 17:18Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 6	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

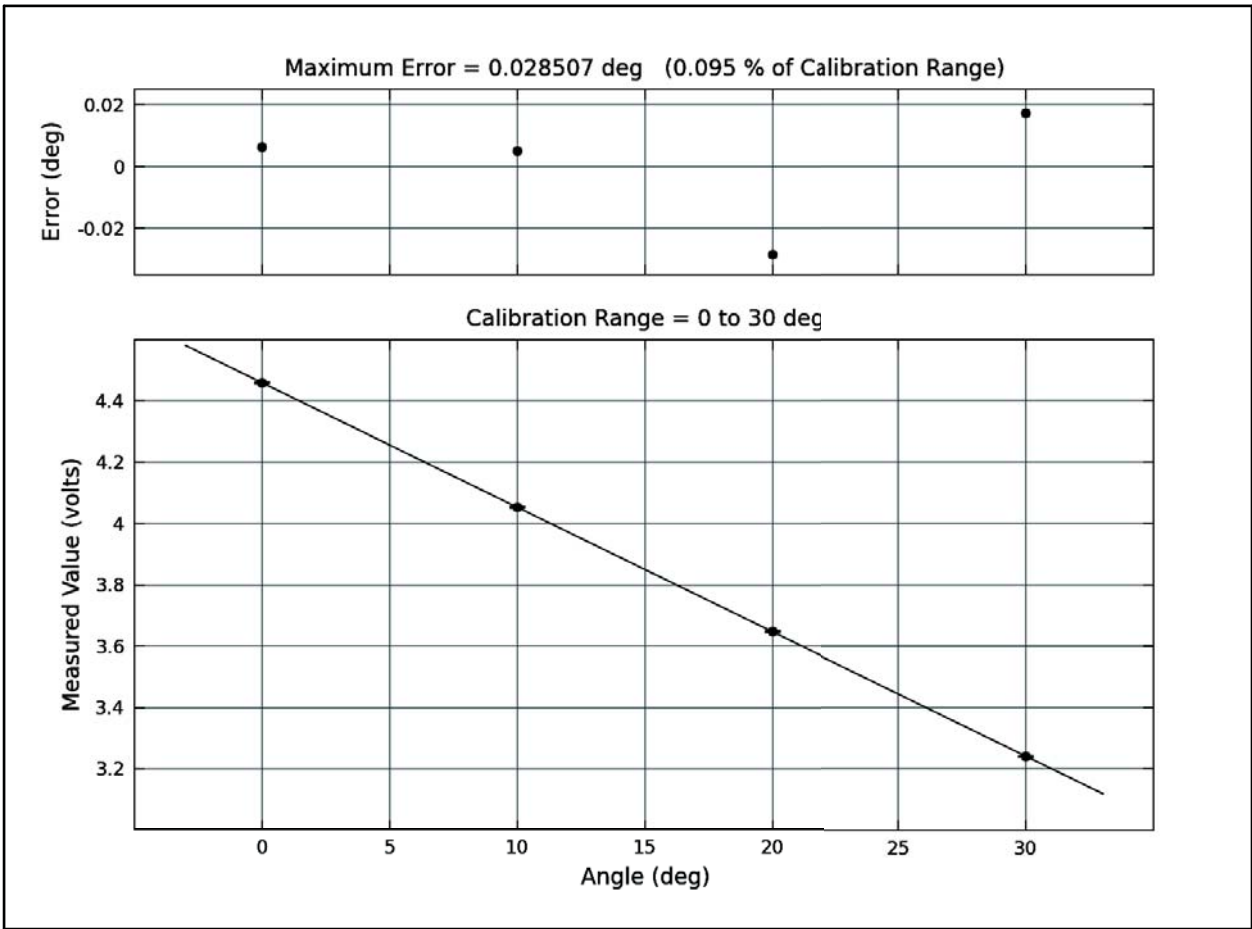
Data Point #	Physical Value (rps)	Measured Value (volts)	Fitted Curve Value (rps)	Error (rps)	Definition of Calibration Curve
1	4.1600	1.2790	4.1596	-0.00044708	Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Angular Velocity (rps), $V(t)$ = measured value (volts), $C_0 = 0.016423$ rps, $C_1 = 3.2393$ rps/volt,
2	7.9100	2.4356	7.9061	-0.0038819	
3	10.150	3.1289	10.152	0.0017632	
4	12.020	3.7071	12.025	0.0049094	
5	15.960	4.9217	15.959	-0.00065271	
6	20.090	6.1963	20.088	-0.0016909	



JSS
Calibration of PMM Yaw
Calibrated 2012-06-12 17:45Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 8	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (deg)	Measured Value (volts)	Fitted Curve Value (deg)	Error (deg)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Angle (deg), $V(t)$ = measured value (volts), $C_0 = 109.81$ deg, $C_1 = -24.628$ deg/volt,
1	0.0000	4.4585	0.0062555	0.0062555	
2	10.000	4.0525	10.005	0.0049287	
3	20.000	3.6478	19.971	-0.028507	
4	30.000	3.2399	30.017	0.017322	

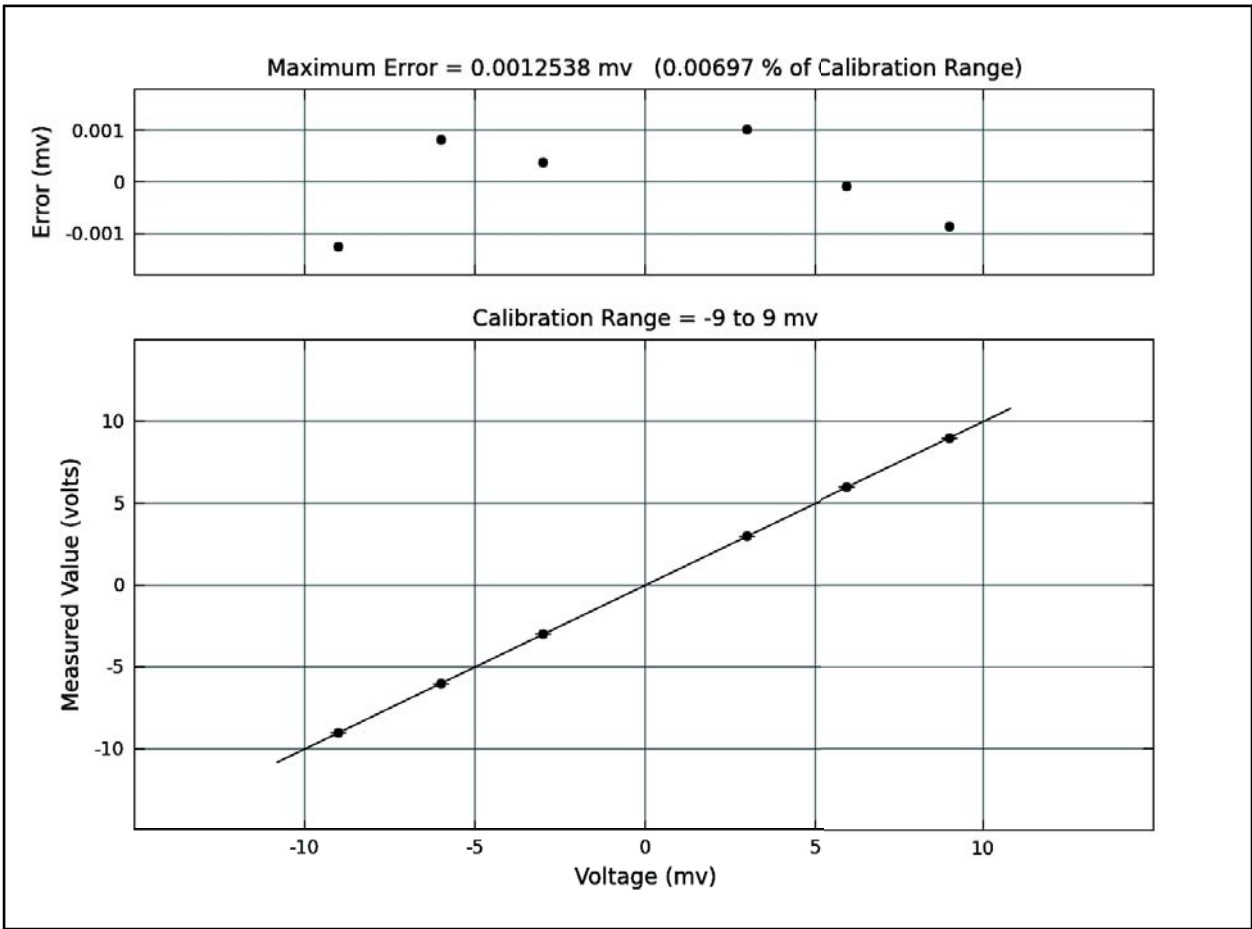


JSS
Calibration of Z1
Calibrated 2011-12-03 01:49Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 17	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (mv)	Measured Value (volts)	Fitted Curve Value (mv)	Error (mv)	Definition of Calibration Curve
1	-9.0000	-9.0367	-9.0013	-0.0012538	
2	-6.0000	-6.0333	-5.9992	0.00081146	
3	-3.0000	-3.0324	-2.9996	0.00038204	
4	3.0000	2.9710	3.0010	0.0010155	
5	6.0000	5.9712	5.9999	-9.2368e-05	
6	9.0000	8.9717	8.9991	-0.00086283	

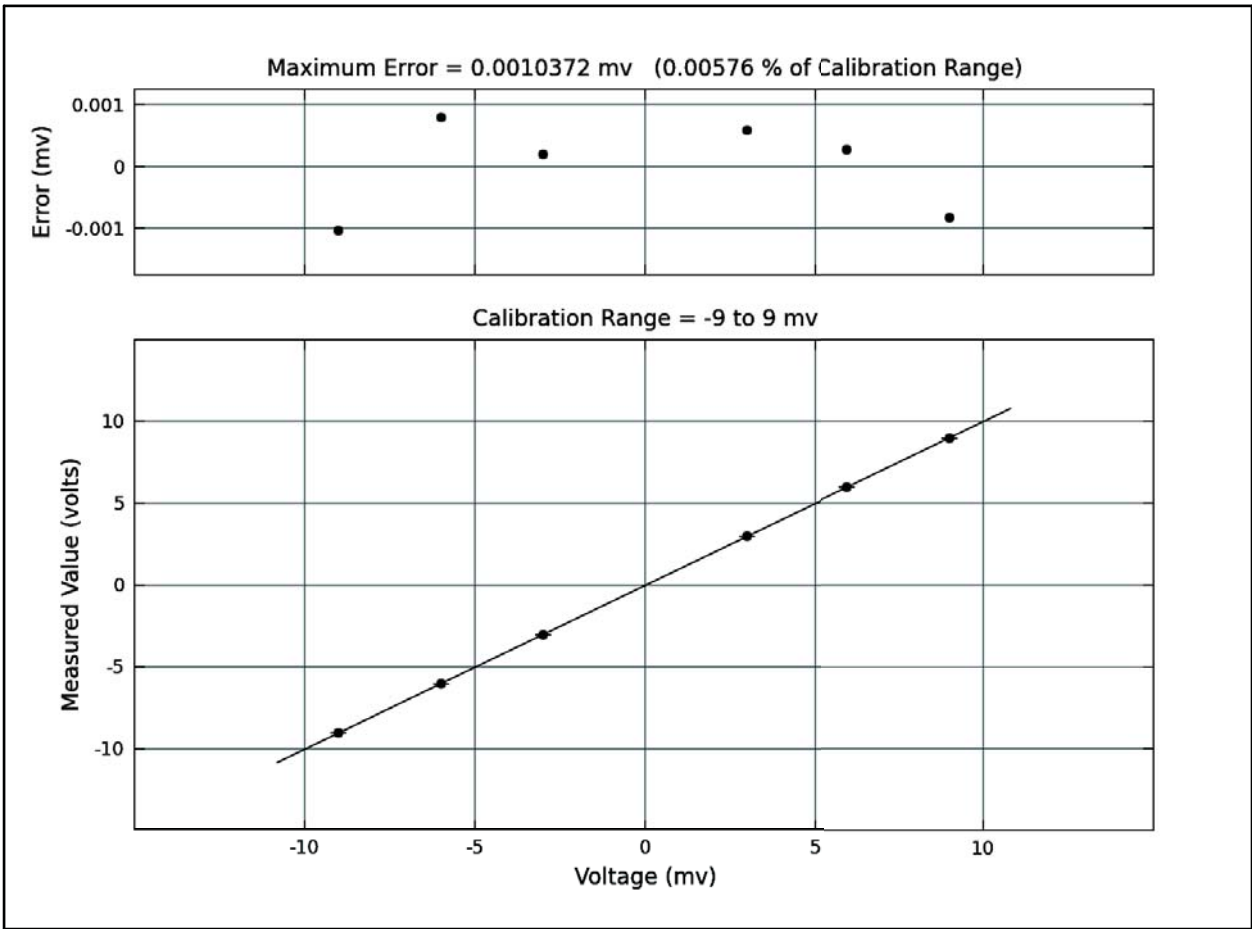
Polynomial Degree = 1 (Linear Fit)
 $Y = C_0 + C_1 \cdot V$
where $Y(t)$ = Voltage (mv),
 $V(t)$ = measured value (volts),
 $C_0 = 0.031386$ mv,
 $C_1 = 0.99956$ mv/volt,



JSS
Calibration of Z2
Calibrated 2011-12-03 01:53Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 18	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

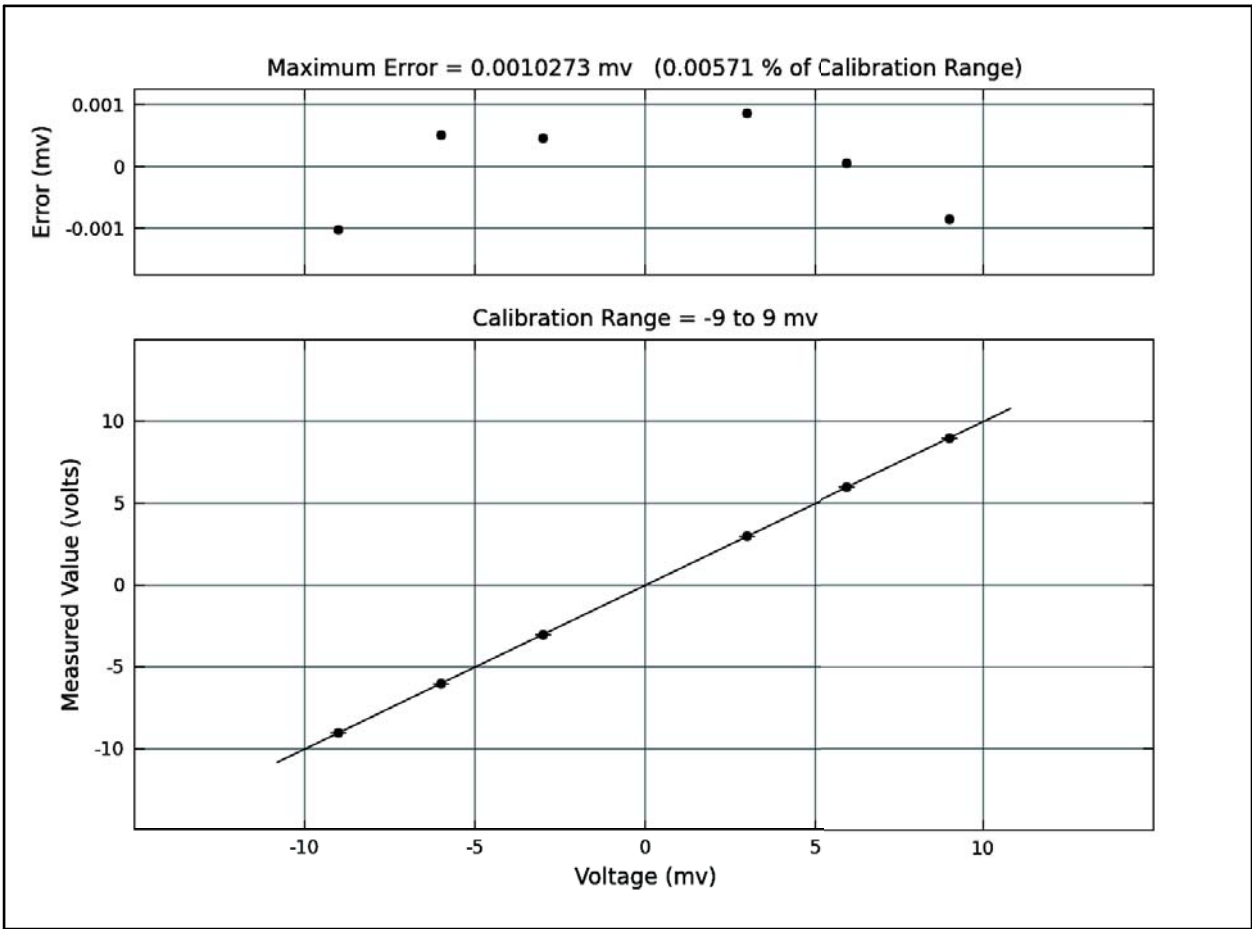
Data Point #	Physical Value (mv)	Measured Value (volts)	Fitted Curve Value (mv)	Error (mv)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Voltage (mv), $V(t)$ = measured value (volts), $C_0 = 0.038274$ mv, $C_1 = 0.99883$ mv/volt,
1	-9.0000	-9.0499	-9.0010	-0.0010372	
2	-6.0000	-6.0445	-5.9992	0.00079177	
3	-3.0000	-3.0416	-2.9998	0.00020349	
4	3.0000	2.9658	3.0006	0.00058580	
5	6.0000	5.9690	6.0003	0.00027979	
6	9.0000	8.9714	8.9992	-0.00082364	



JSS
Calibration of Z3
Calibrated 2011-12-03 01:57Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 19	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (mv)	Measured Value (volts)	Fitted Curve Value (mv)	Error (mv)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Voltage (mv), $V(t)$ = measured value (volts), $C_0 = 0.033925$ mv, $C_1 = 0.99953$ mv/volt,
1	-9.0000	-9.0392	-9.0010	-0.0010273	
2	-6.0000	-6.0363	-5.9995	0.00051385	
3	-3.0000	-3.0349	-2.9995	0.00045418	
4	3.0000	2.9683	3.0009	0.00085950	
5	6.0000	5.9690	6.0001	5.9817e-05	
6	9.0000	8.9695	8.9991	-0.00086005	

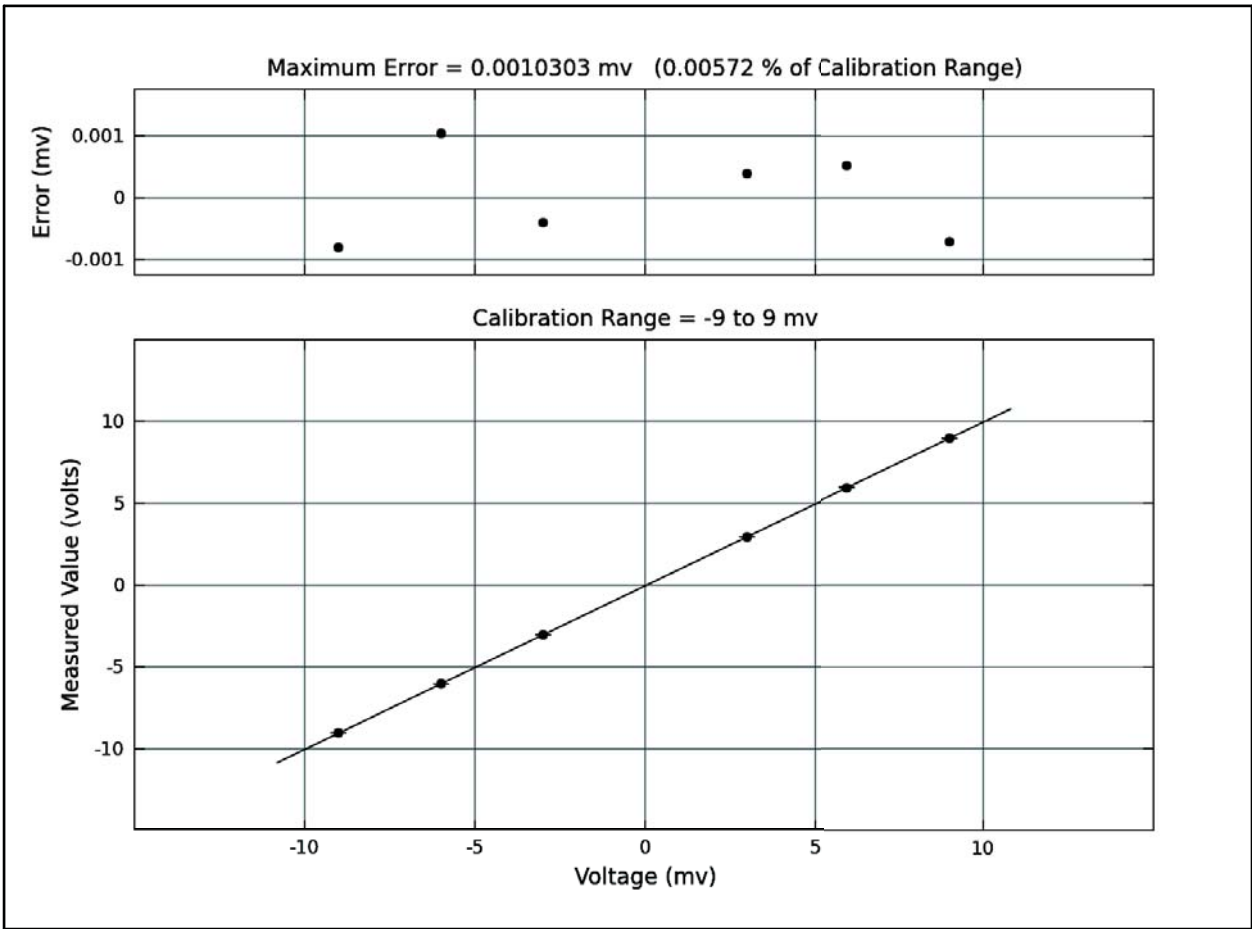


JSS
Calibration of Y1
Calibrated 2011-12-03 02:05Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 20	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (mv)	Measured Value (volts)	Fitted Curve Value (mv)	Error (mv)	Definition of Calibration Curve
1	-9.0000	-9.0617	-9.0008	-0.00080516	
2	-6.0000	-6.0597	-5.9990	0.0010303	
3	-3.0000	-3.0611	-3.0004	-0.00040022	
4	3.0000	2.9398	3.0004	0.00038374	
5	6.0000	5.9401	6.0005	0.00051389	
6	9.0000	8.9389	8.9993	-0.00072253	

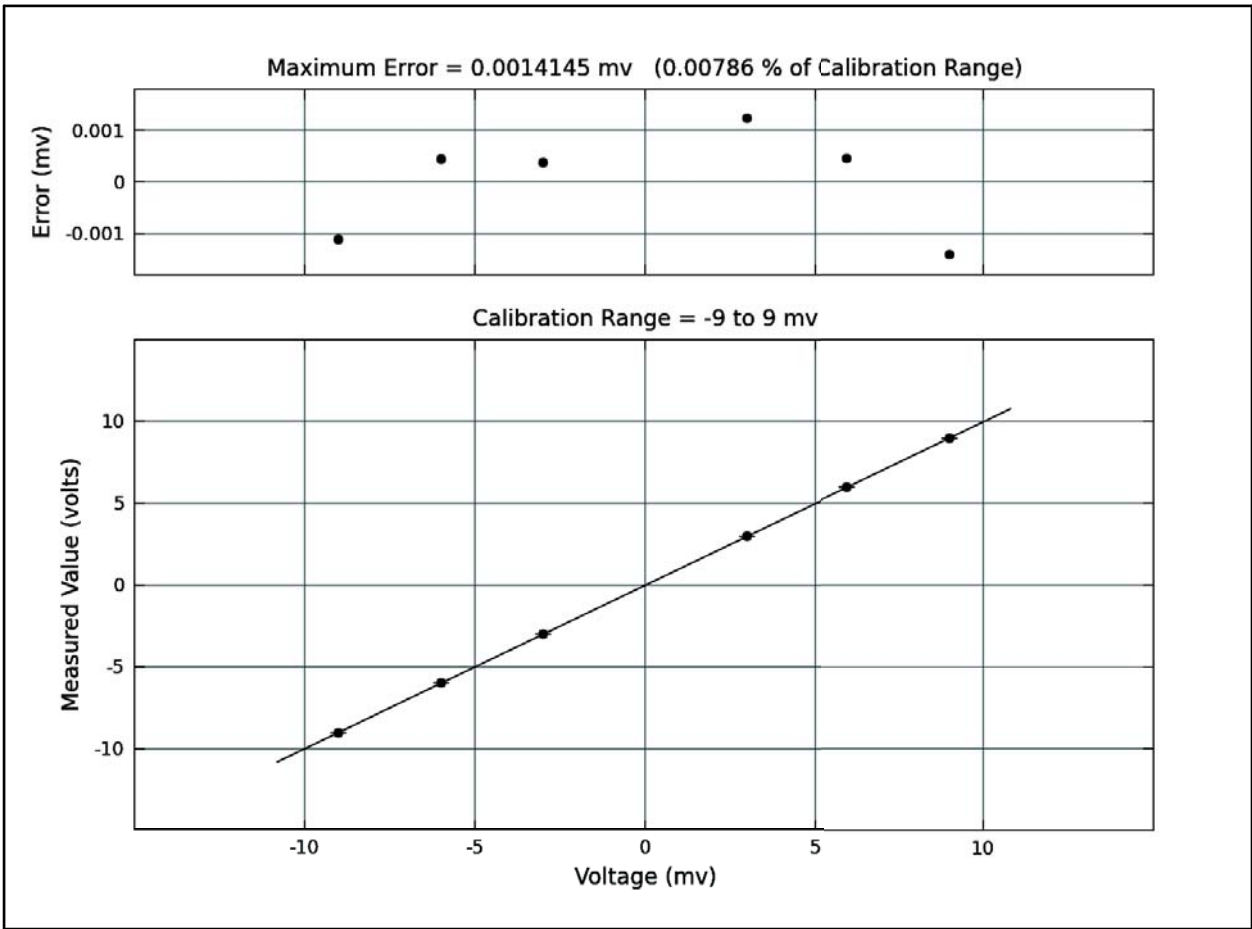
Polynomial Degree = 1 (Linear Fit)
 $Y = C_0 + C_1 \cdot V$
 where $Y(t)$ = Voltage (mv),
 $V(t)$ = measured value (volts),
 $C_0 = 0.060616$ mv,
 $C_1 = 0.99997$ mv/volt,



JSS
Calibration of Y2
Calibrated 2011-12-03 02:09Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 21	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

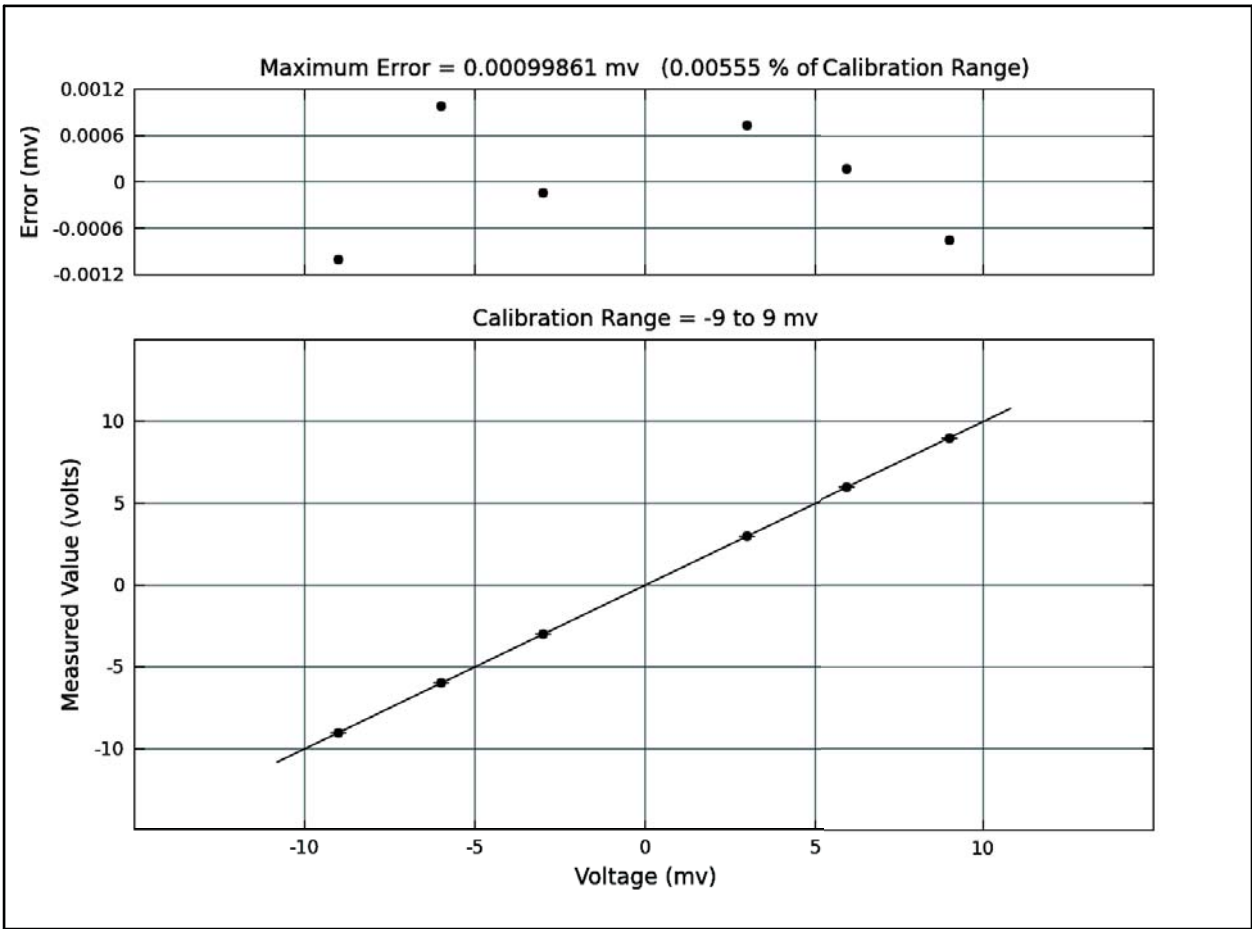
Data Point #	Physical Value (mv)	Measured Value (volts)	Fitted Curve Value (mv)	Error (mv)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Voltage (mv), $V(t)$ = measured value (volts), $C_0 = 0.031336$ mv, $C_1 = 1.0014$ mv/volt,
1	-9.0000	-9.0203	-9.0011	-0.0011193	
2	-6.0000	-6.0227	-5.9995	0.00045032	
3	-3.0000	-3.0269	-2.9996	0.00038259	
4	3.0000	2.9659	3.0012	0.0012348	
5	6.0000	5.9611	6.0005	0.00046605	
6	9.0000	8.9551	8.9986	-0.0014145	



JSS
Calibration of X1
Calibrated 2011-12-03 02:15Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 22	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

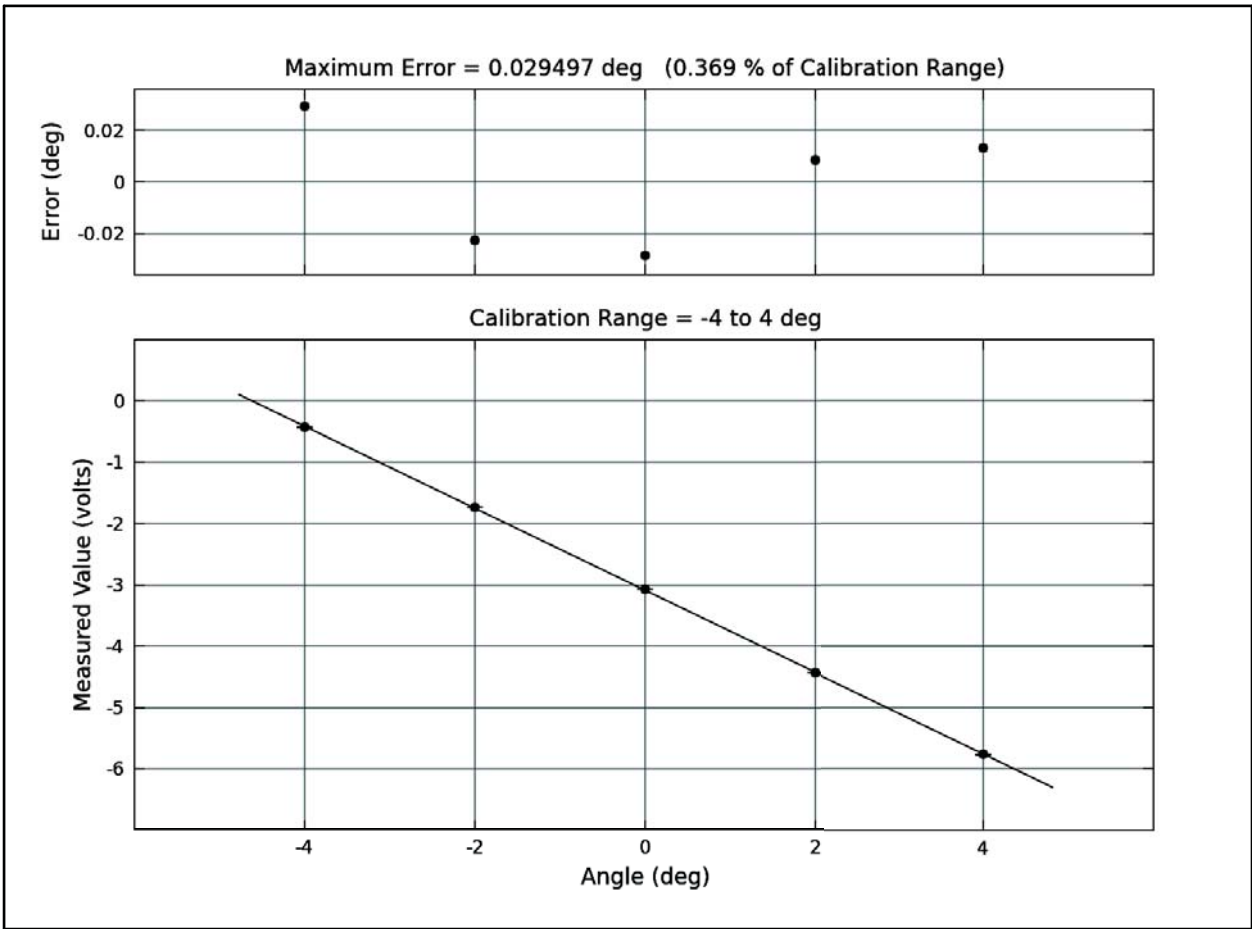
Data Point #	Physical Value (mv)	Measured Value (volts)	Fitted Curve Value (mv)	Error (mv)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Voltage (mv), $V(t)$ = measured value (volts), $C_0 = 0.024188$ mv, $C_1 = 1.0002$ mv/volt,
1	-9.0000	-9.0236	-9.0010	-0.00099861	
2	-6.0000	-6.0221	-5.9990	0.00098186	
3	-3.0000	-3.0238	-3.0001	-0.00014071	
4	3.0000	2.9760	3.0007	0.00073734	
5	6.0000	5.9749	6.0002	0.00017153	
6	9.0000	8.9734	8.9992	-0.00075141	



JSS
Calibration of PMM Pitch
Calibrated 2012-06-07 21:06Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 23	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

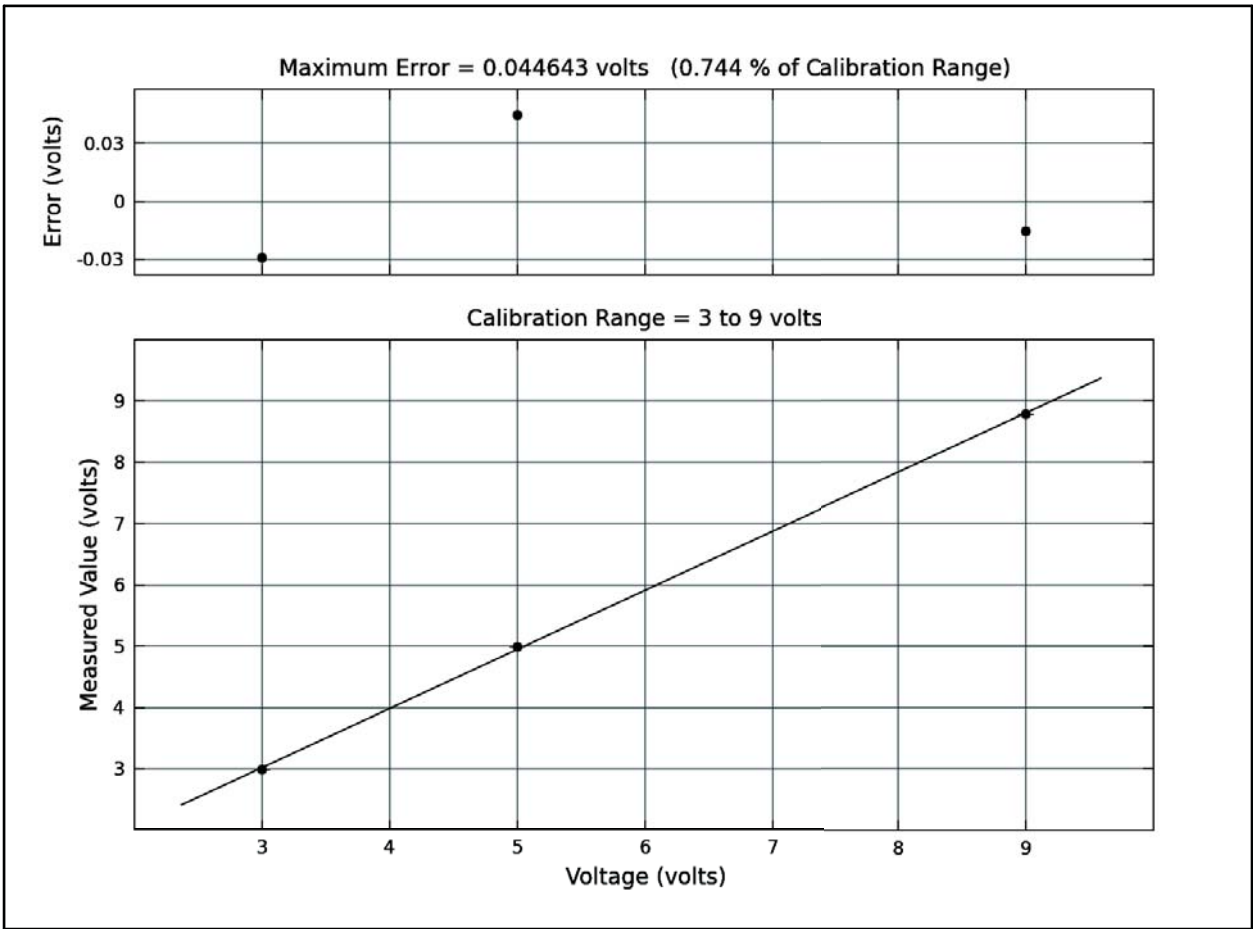
Data Point #	Physical Value (deg)	Measured Value (volts)	Fitted Curve Value (deg)	Error (deg)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Angle (deg), $V(t)$ = measured value (volts), $C_0 = -4.621$ deg, $C_1 = -1.4964$ deg/volt,
1	-4.0000	-0.43472	-3.9705	0.029497	
2	-2.0000	-1.7364	-2.0227	-0.022707	
3	0.0000	-3.0690	-0.028597	-0.028597	
4	2.0000	-4.4303	2.0086	0.0085528	
5	4.0000	-5.7700	4.0133	0.013254	



JSS
Calibration of PMM Start
Calibrated 2012-06-12 18:11Z

Test Facility: CWT	Serial #:	Filter Frequency:
Data Source: daspc49:50001 Channel 24	Programmable Gain:	Excitation:
Sensor Model:	Plug-In Gain:	

Data Point #	Physical Value (volts)	Measured Value (volts)	Fitted Curve Value (volts)	Error (volts)	Definition of Calibration Curve
1	3.0000	2.9939	2.9708	-0.029247	Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Voltage (volts), $V(t)$ = measured value (volts), $C_0 = -0.13771$ volts, $C_1 = 1.0383$ volts/volt,
2	5.0000	4.9913	5.0446	0.044643	
3	9.0000	8.7861	8.9846	-0.015395	



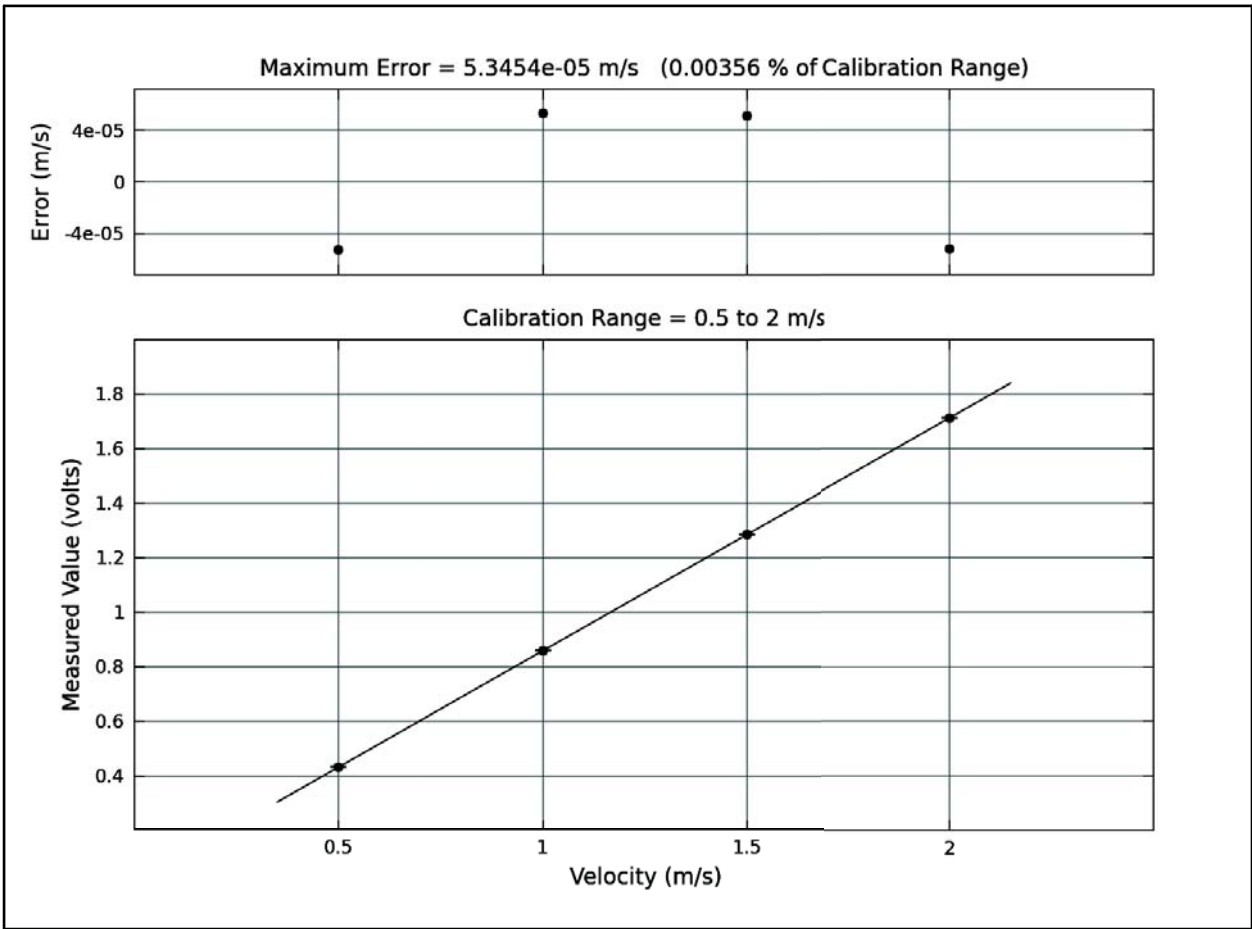
JSS

Calibration of Tachogenerator

Calibrated 2011-12-13 17:20Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: towdas:50001 Channel 1	Programmable Gain: 1	Excitation:
Sensor Model:	Plug-In Gain:	

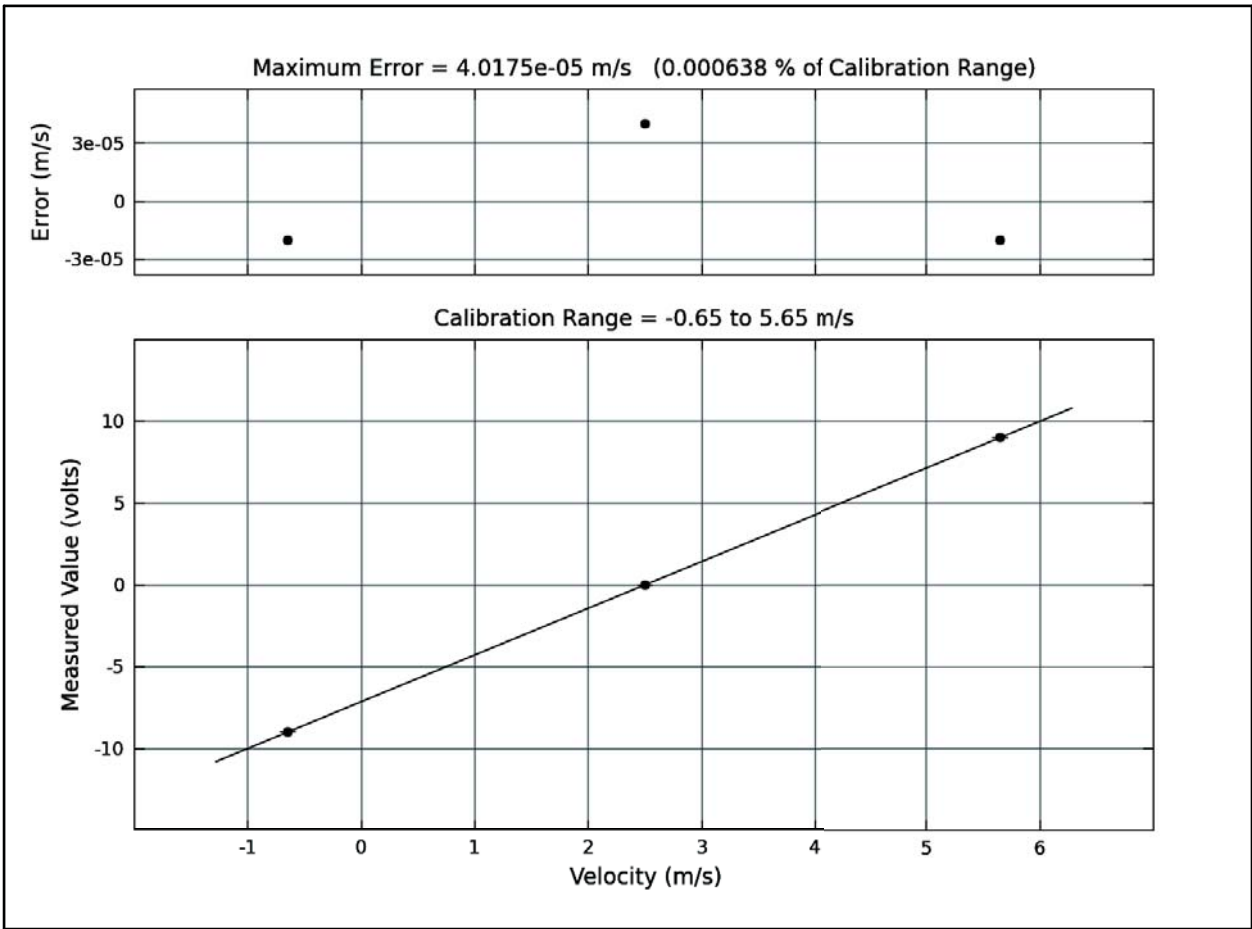
Data Point #	Physical Value (m/s)	Measured Value (volts)	Fitted Curve Value (m/s)	Error (m/s)	Definition of Calibration Curve
1	0.50000	0.43194	0.49995	-5.2873e-05	Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Velocity (m/s), $V(t)$ = measured value (volts), $C_0 = -0.0064425$ m/s, $C_1 = 1.1724$ m/s/volt,
2	1.0000	0.85853	1.0001	5.3454e-05	
3	1.5000	1.2850	1.5001	5.1733e-05	
4	2.0000	1.7114	1.9999	-5.2314e-05	



JSS
Calibration of Carriage Speed
Calibrated 2012-04-16 11:49Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: towdas:50001 Channel 2	Programmable Gain: 1	Excitation:
Sensor Model:	Plug-In Gain: 1	

Data Point #	Physical Value (m/s)	Measured Value (volts)	Fitted Curve Value (m/s)	Error (m/s)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Velocity (m/s), $V(t)$ = measured value (volts), $C_0 = 2.5002$ m/s, $C_1 = 0.35012$ m/s/volt,
1	-0.65000	-8.9975	-0.65002	-2.0087e-05	
2	2.5000	-0.00031922	2.5000	4.0175e-05	
3	5.6500	8.9965	5.6500	-2.0088e-05	

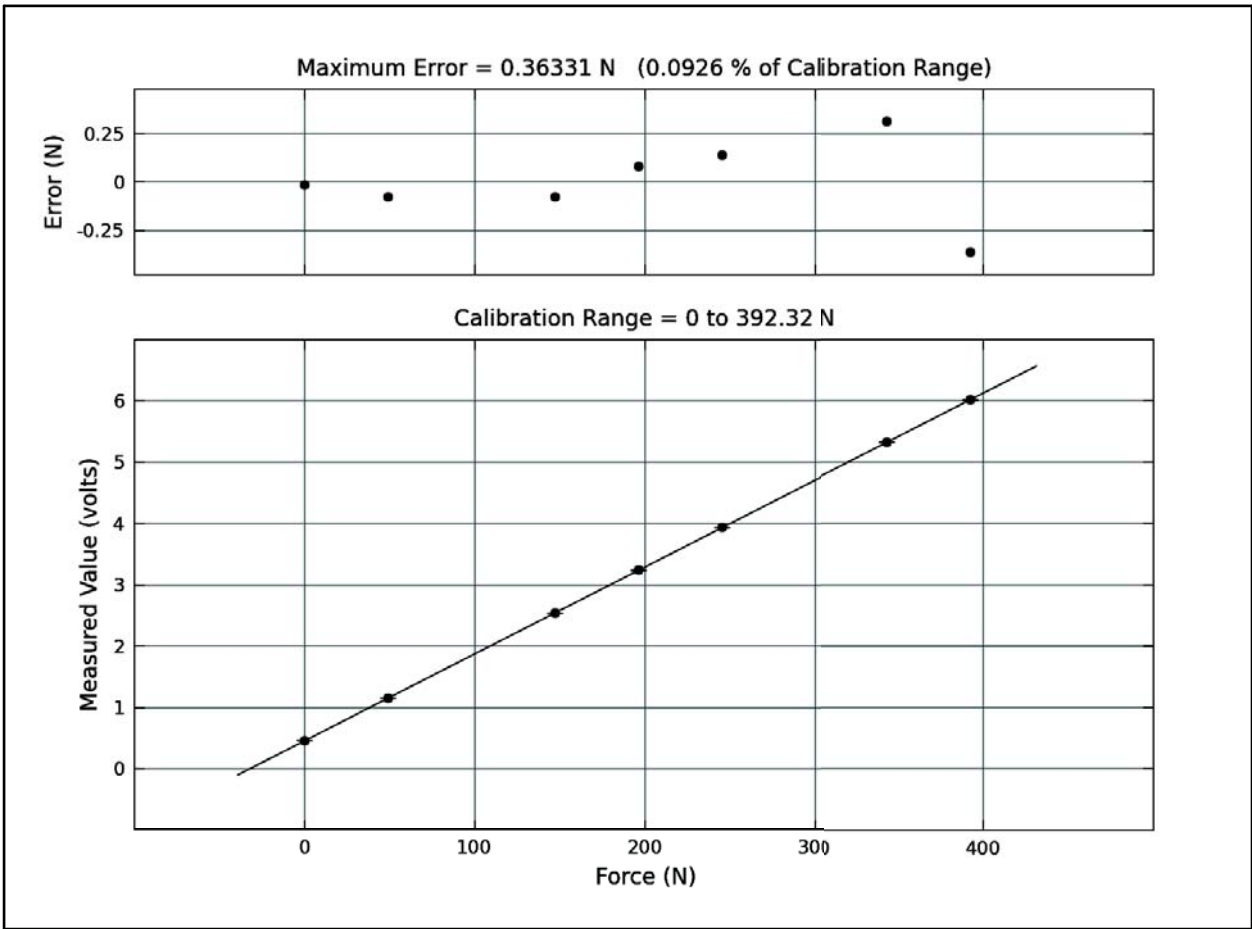


JSS
Calibration of Inline Load
Calibrated 2012-04-19 16:43Z

Test Facility: CWT	Serial #: A10656	Filter Frequency: 10
Data Source: towdas:50001 Channel 10	Programmable Gain: 1	Excitation: 10v
Sensor Model: Sensotronics 0001A100-1000	Plug-In Gain: 200	

Data Point #	Physical Value (N)	Measured Value (volts)	Fitted Curve Value (N)	Error (N)	Definition of Calibration Curve
1	0.0000	0.45865	-0.016217	-0.016217	
2	49.040	1.1524	48.965	-0.075335	
3	147.12	2.5415	147.04	-0.077776	
4	196.16	3.2383	196.24	0.080099	
5	245.20	3.9337	245.34	0.13925	
6	343.28	5.3254	343.59	0.31329	
7	392.32	6.0104	391.96	-0.36331	

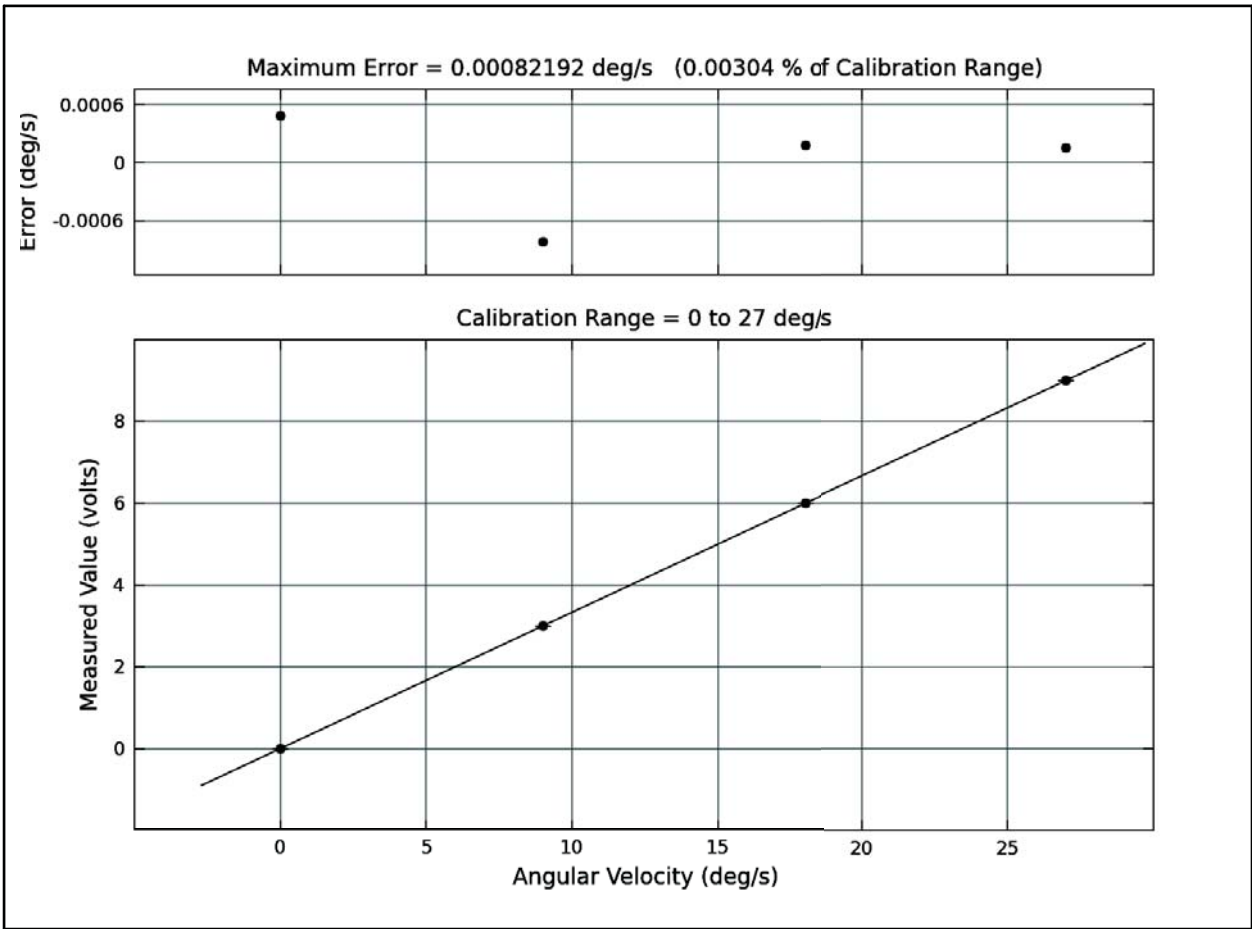
Polynomial Degree = 1 (Linear Fit)
 $Y = C_0 + C_1 \cdot V$
where $Y(t)$ = Force (N),
 $V(t)$ = measured value (volts),
 $C_0 = -32.399$ N,
 $C_1 = 70.604$ N/volt,



JSS
Calibration of Yaw Velocity
Calibrated 2012-06-12 12:57Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: towdas:50001 Channel 33	Programmable Gain: 1	Excitation: 10
Sensor Model:	Plug-In Gain: 1	

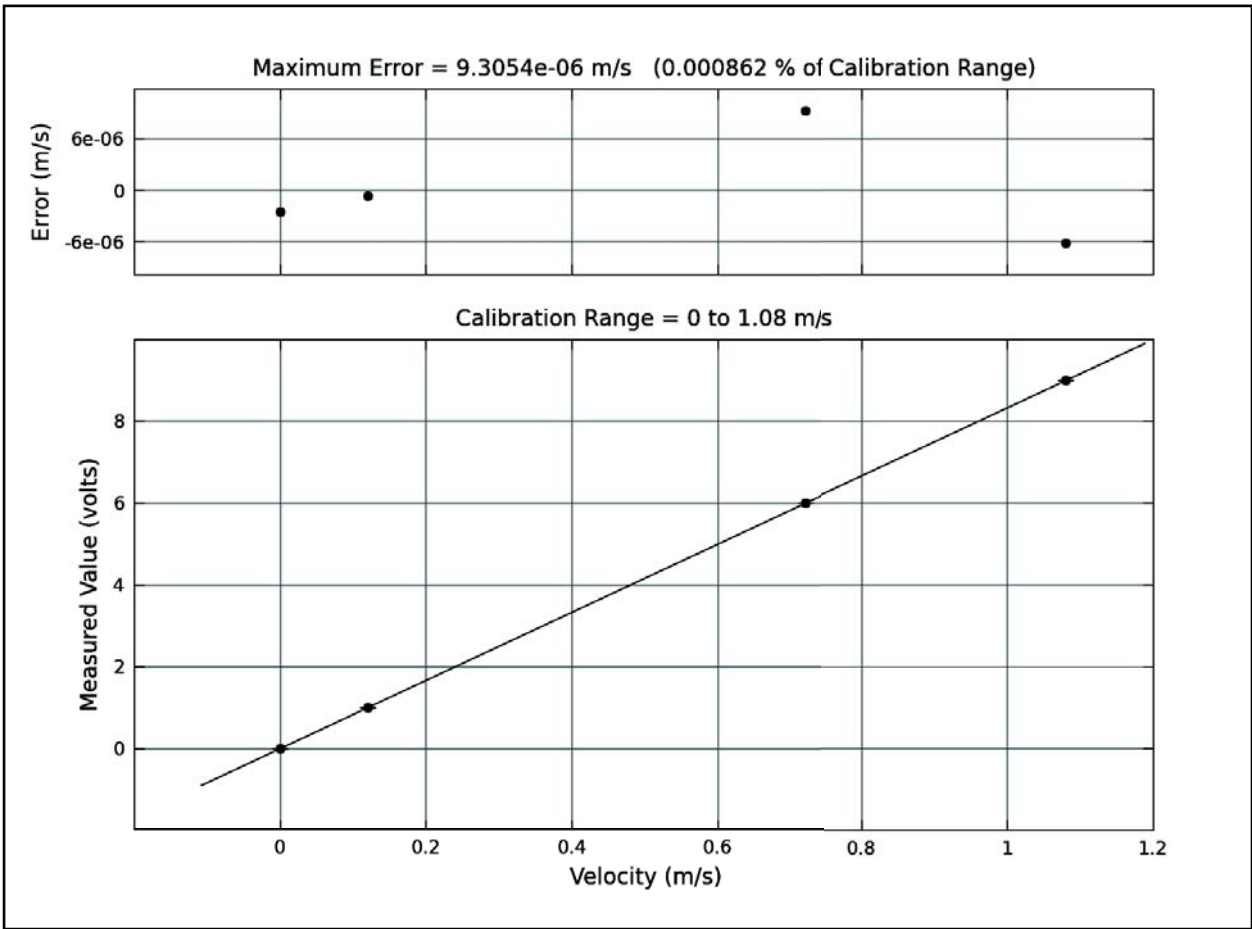
Data Point #	Physical Value (deg/s)	Measured Value (volts)	Fitted Curve Value (deg/s)	Error (deg/s)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Angular Velocity (deg/s), $V(t)$ = measured value (volts), $C_0 = 0.0074421$ deg/s, $C_1 = 3.0005$ deg/s/volt,
1	0.0000	-0.0023175	0.00048828	0.00048828	
2	9.0000	2.9967	8.9992	-0.00082192	
3	18.000	5.9966	18.000	0.00017910	
4	27.000	8.9960	27.000	0.00015454	



JSS
Calibration of Sway Velocity
Calibrated 2012-06-12 13:00Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: towdas:50001 Channel 34	Programmable Gain: 1	Excitation: 10v
Sensor Model:	Plug-In Gain: 1	

Data Point #	Physical Value (m/s)	Measured Value (volts)	Fitted Curve Value (m/s)	Error (m/s)	Definition of Calibration Curve Polynomial Degree = 1 (Linear Fit) $Y = C_0 + C_1 \cdot V$ where $Y(t)$ = Velocity (m/s), $V(t)$ = measured value (volts), $C_0 = 0.00029586$ m/s, $C_1 = 0.12003$ m/s/volt,
1	0.0000	-0.0024860	-2.5301e-06	-2.5301e-06	
2	0.12000	0.99729	0.12000	-6.4300e-07	
3	0.72000	5.9962	0.72001	9.3054e-06	
4	1.0800	8.9954	1.0800	-6.1323e-06	

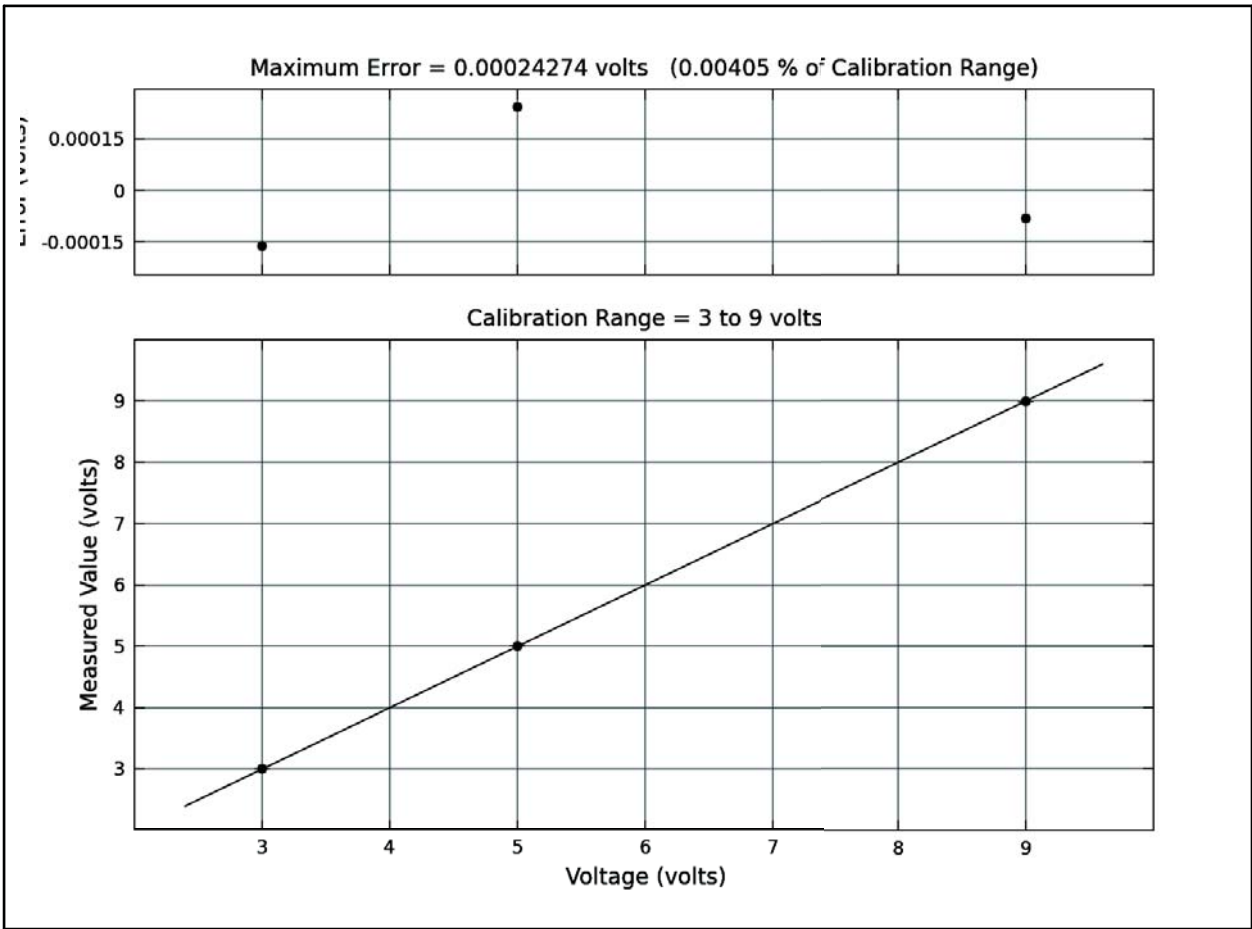


JSS
Calibration of DAS Trigger
Calibrated 2012-06-12 18:11Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: towdas:50001 Channel 35	Programmable Gain: 1	Excitation: 10v
Sensor Model:	Plug-In Gain: 1	

Data Point #	Physical Value (volts)	Measured Value (volts)	Fitted Curve Value (volts)	Error (volts)	Definition of Calibration Curve
1	3.0000	2.9964	2.9998	-0.00016181	
2	5.0000	4.9964	5.0002	0.00024274	
3	9.0000	8.9952	8.9999	-8.0927e-05	

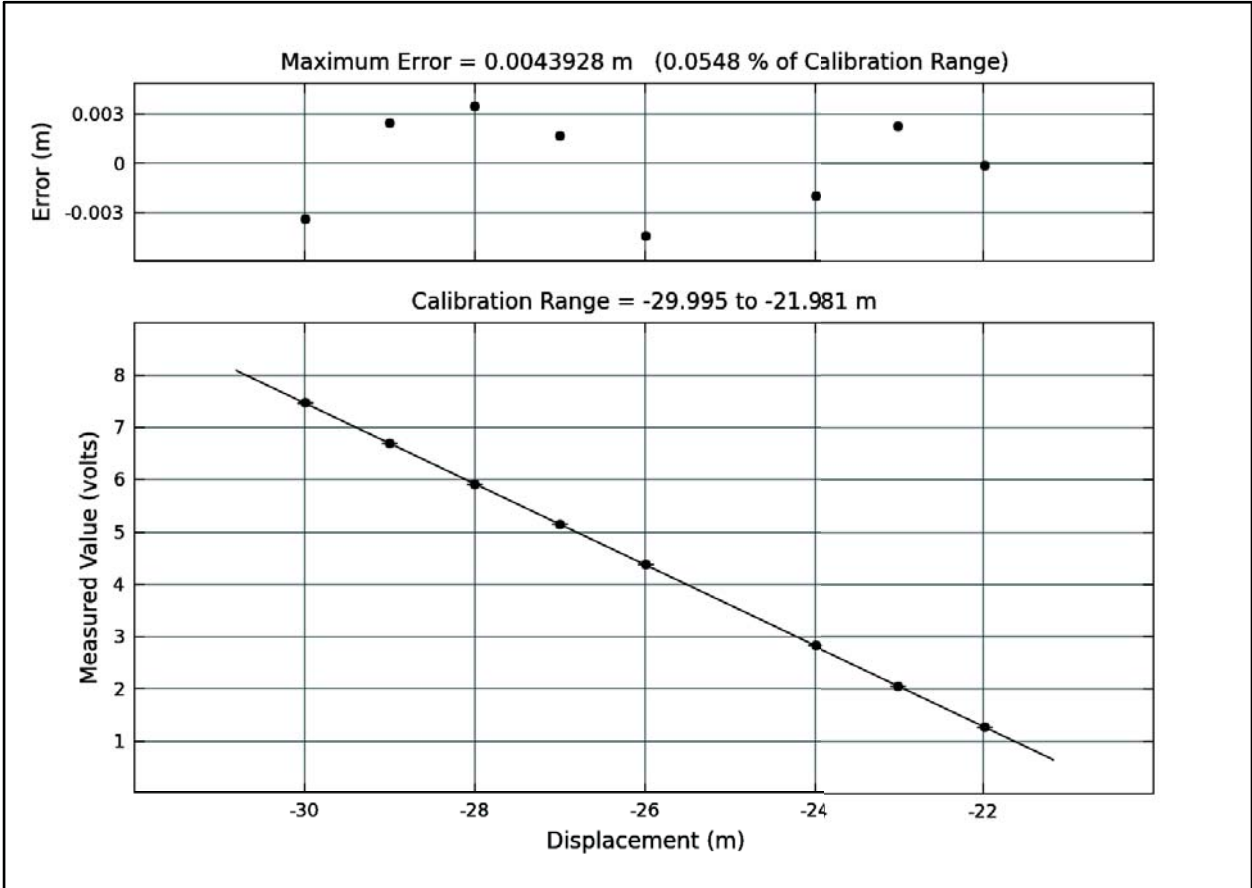
Polynomial Degree = 1 (Linear Fit)
 $Y = C_0 + C_1 \cdot V$
 where $Y(t)$ = Voltage (volts),
 $V(t)$ = measured value (volts),
 $C_0 = 0.0028737$ volts,
 $C_1 = 1.0002$ volts/volt,



JSS
Calibration of Sway Displacement
Calibrated 2012-06-11 17:08Z

Test Facility: CWT	Serial #:	Filter Frequency: 10
Data Source: towdas:50001 Channel 39	Programmable Gain: 1	Excitation: 10v
Sensor Model:	Plug-In Gain: 1	

Data Point #	Physical Value (m)	Measured Value (volts)	Fitted Curve Value (m)	Error (m)	Definition of Calibration Curve
1	-29.995	7.4662	-29.998	-0.0034051	
2	-28.996	6.6897	-28.994	0.0024796	
3	-27.996	5.9162	-27.993	0.0034695	
4	-26.997	5.1457	-26.995	0.0016671	
5	-25.995	4.3761	-25.999	-0.0043928	
6	-23.994	2.8280	-23.996	-0.0019574	
7	-22.996	2.0535	-22.994	0.0022623	
8	-21.981	1.2710	-21.981	-0.00012325	



APPENDIX B
PMM Balance: Calibration Matrix and Calculation of Forces and
Moments

The measurements of individual load cells X1, Y1, Y2, Z1, Z2, Z3 in mV/V, with the correct signs (positive forward, to starboard, and down), were multiplied by their load cell sensitivities:

X1: 296.814 N/(mV/V)
 Y1: 1070.24 N/(mV/V)
 Y2: 1031.442 N/(mV/V)
 Z1: 1089.97 N/(mV/V)
 Z2: 1098.48 N/(mV/V)
 Z3: 1107.46 N/(mV/V)

The crosstalk matrix was then applied to correct the individual load cell measurements. The crosstalk matrix represents the interferences between individual balance load cells and departures from the nominal balance geometry. The following crosstalk matrix was determined by doing a balance calibration in December 2011, using the Cussons procedure. The crosstalk matrix was derived from the force and moments measurements by reversing the exact same steps as presented in this appendix, only using the different Y1 and Y2 load cells that were in the balance at that time and their sensitivities.

	X1	Y1	Y2	Z1	Z2	Z3
X1	1.0049	0.0029	0.0030	-0.0027	0.0003	0.0000
Y1	-0.0055	0.9923	-0.0008	-0.0007	0.0003	-0.0003
Y2	-0.0012	0.0019	1.0008	0.0000	-0.0011	0.0007
Z1	-0.0104	-0.0007	-0.0028	0.9943	0.0009	-0.0001
Z2	0.0078	-0.0037	-0.0031	0.0003	0.9934	-0.0005
Z3	0.0086	0.0066	0.0037	-0.0006	-0.0010	0.9945

The longitudinal force X1 was corrected for the effect of the balance weight when the model has some trim angle, subtracting $17.245 * \text{Trim}[\text{deg}]$, as determined by performing a longitudinal inclining experiment at the start of the June 2012 test session

Then the nominal geometry matrix was applied to obtain forces and moments FX, FY, FZ, MX, MY, MZ at the balance centre P:

	X1	Y1	Y2	Z1	Z2	Z3
FX	1	0	0	0	0	0
FY	0	1	1	0	0	0
FZ	0	0	0	1	1	1
MX	0	0.067	0.067	-0.1	-0.1	0.15
MY	-0.067	0	0	0.44	-0.44	0
MZ	0	-0.5	0.5	0	0	0

Finally, the moments were transferred to model origin O.

APPENDIX C
Test Log

DATE	TIME	WAIT TIME ACTUAL	Speed (m/s)	FILENAME(DAQ)	PMMI DRIVE SIGNAL (VORG007?) MDF	RUN DESCRIPTION	RPS	Video track #	Yaw Angle	COMMENTS
08-Jun-12	8:00 to 16:00									Decommission model and start PMM install
11-Jun-12	8:00 to 16:00									PMM install and calibrations
12-Jun-12	12:00 to 14:00									Received model form model prep shop around noon. Begin ballasting of model connect model to pmm
13-Jun-12	8:20 to 9:54									Check excitations of dyno channels @model
	8:43									
	9:07									
	9:26									
	9:54									
	10:56									
	11:09									
	11:12									
	11:22									
	11:57									
	12:05									
	12:17									
	12:33									
	12:46									
	12:59									
	13:09									
	13:19									
	13:30									
	13:40									
	13:50									
	14:00									
	14:11									
	14:23									
	14:33									
	14:43									
	14:54									
	15:05									
	15:16									
	15:27									
	15:37									
	15:47									
	15:57									
	16:07									
14-Jun-12	8:23									

Test data saved on "Testdata on Knarr Y:\Test_PJ2517\CWT\June_2012"

Rudder command at 0.75 means rudder on CL
Rudder command at -0.75 means aligned flow with props on (zero yaw moment)

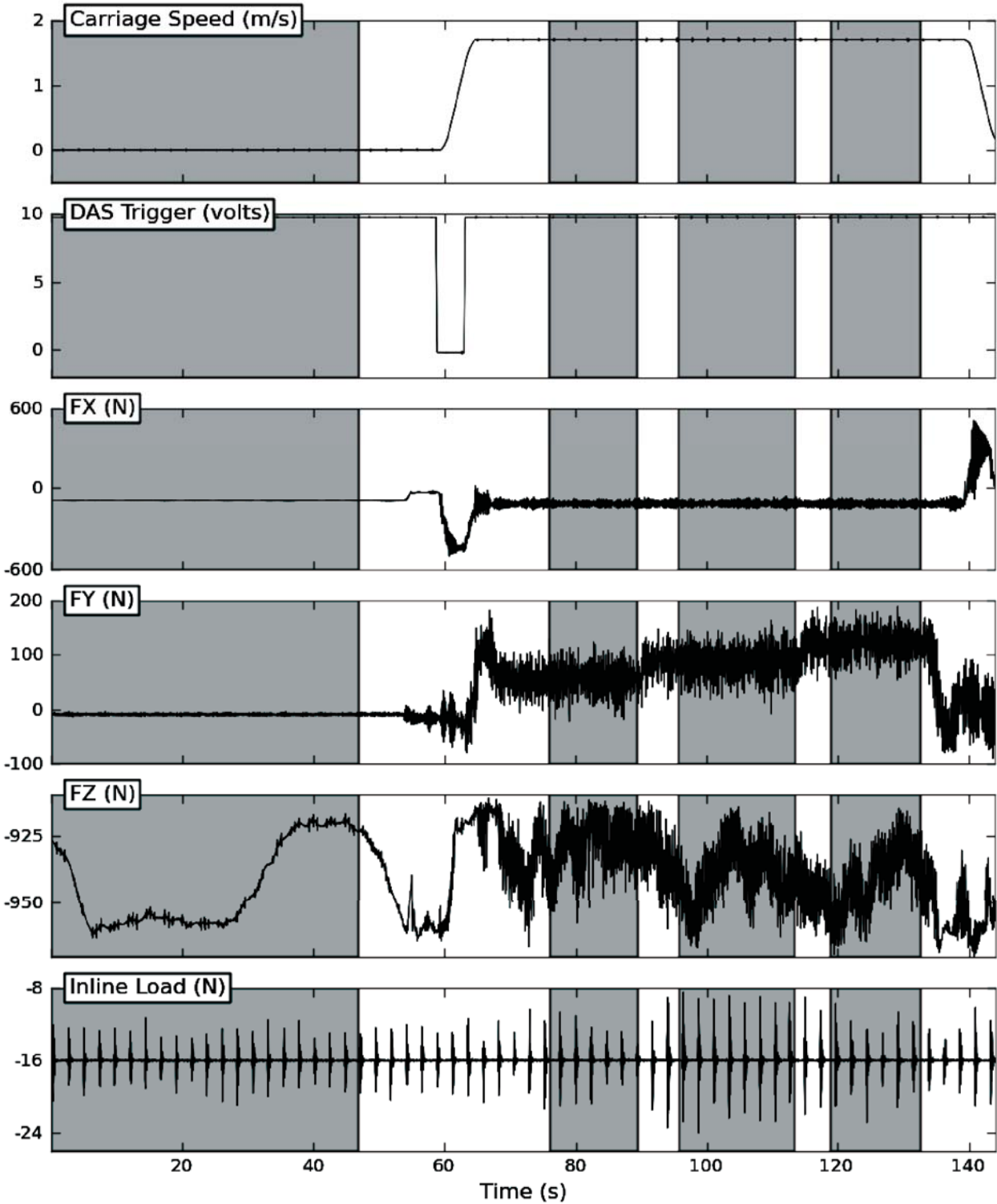
DATE	TIME	WAIT TIME ACTUAL	Speed (m/s)	FILENAME(DAQ)	PMMDRIVE SIGNAL (VORG007?)MDF	RUN DESCRIPTION	RFS	Video track #	Yaw Angle	COMMENTS
*	8:50	0:14	0.00							
*	9:04	0:11	1.697	Insitu_002 yaw sweep_003	46	Bollard, carriage at 90m yaw sweep @0.10, -20deg	6.00	N/A		rezero rudder angle and pmmd yaw
*	9:15	0:10	1.697	yaw sweep_004	47	yaw sweep @0.10, -20deg	6.00	N/A		rezero sinkage and pmmd sway
*	9:25	0:16	1.697	Run_020	N/A	Rudder angles = 35, 30, 20 deg	9.96	N/A	4	rudder commanded to +0.75deg offset
*	9:41	0:10	1.697	Run_021	4	Rudder angles = 10, -10, -20 deg	9.96	N/A	4	repeat for check
*	9:51	0:10	1.697	Run_022	4	Rudder angles = 25, 30, 35 deg	9.96	20	4	video missed
*	10:01	0:11	1.697	Run_023	4	Rudder angles = 0, -10, -20 deg	9.96	21	4	
*	10:12	0:10	1.697	Run_024	5	Rudder angles = -35, -30, -20 deg	9.96	22	8	
*	10:22	0:10	1.697	Run_025	5	Rudder angles = -10, 0, 10 deg	9.96	23	8	
*	10:32	0:10	1.697	Run_026	5	Rudder angles = 20, 30, 35 deg	9.96	24	8	
*	10:42	0:14	1.697	Run_027	6	Rudder angles = -35, -30, -20 deg	9.96	25	12	wrong angles used, repeat with new angles, will be Run_030
*	10:56	0:09	1.697	Run_028	6	Rudder angles = -10, 0, 10 deg	9.96	26	12	
*	11:05	0:10	1.697	Run_029	6	Rudder angles = 20, 30, 35 deg	9.96	27	12	
*	11:15	0:13	1.697	Run_030	5	Rudder angles = 25, 30, 35 deg	9.96	28	8	This is a repeat run / fill in run for Run_026
*	11:28	0:19	1.697	Run_031	4	Rudder angles = 25, 30, 35 deg	9.96	29	4	Fill ins for three signal 4
*	11:37	0:10	1.697	Run_032	4	Rudder angles = -25, -30, -35 deg	9.96	30	4	Fill ins for drive signal 4
*	11:47	0:10	1.697	Run_033	7	Rudder angles = -35, -30, -20 deg	9.96	31	16	
*	11:57	0:10	1.697	Run_034	7	Rudder angles = -10, 0, 10 deg	9.96	32	16	
*	12:07	0:10	1.697	Run_035	7	Rudder angles = 20, 30, 35 deg	9.96	33	16	
*	12:17	0:10	1.697	Run_036	8	Rudder angles = -35, -30, -20 deg	9.96	34	20	
*	12:27	0:11	1.697	Run_037	8	Rudder angles = -10, 0, 10 deg	9.96	35	20	
*	12:38	0:11	1.697	Run_038	8	Rudder angles = 20, 30, 35 deg	9.96	36	20	
*	12:49	0:12	1.697	Run_039	12	Rudder angles = -35, -30, -20 deg	9.96	37	4	
*	13:01	0:11	1.697	Run_040	12	Rudder angles = -10, 0, 10 deg	9.96	38	4	
*	13:12	0:10	1.697	Run_041	12	Rudder angles = 20, 30, 35 deg	9.96	39	4	
*	13:22	0:10	1.697	Run_042	11	Rudder angles = -35, -30, -20 deg	9.96	40	8	
*	13:32	0:10	1.697	Run_043	11	Rudder angles = -10, 0, 10 deg	9.96	41	-8	
*	13:42	0:11	1.697	Run_044	11	Rudder angles = 20, 30, 35 deg	9.96	42	-8	wrong rudder angle set for first angle(35deg), repeat run
*	13:53	0:10	1.697	Run_045	11	Rudder angles = -25, -20, 25 deg	9.96	43	-8	2 fill in angles included
*	14:03	0:10	1.697	Run_046	10	Rudder angles = -35, -30, -20 deg	9.96	44	-12	
*	14:13	0:10	1.697	Run_047	10	Rudder angles = -10, 0, 10 deg	9.96	45	-12	
*	14:23	0:10	1.697	Run_048	10	Rudder angles = 20, 30, 35 deg	9.96	46	-12	
*	14:33	0:10	1.697	Run_049	9	Rudder angles = -35, -30, -20 deg	9.96	47	-16	
*	14:43	0:30	1.697	Run_050	9	Rudder angles = -10, 0, 10 deg	9.96	48	-16	OCC using tank in between runs, wait times may be a little longer than 10 min
*	15:13	0:22	1.697	Run_051	9	Rudder angles = 20, 30, 35 deg	9.96	49	-16	
*	15:35	0:09	1.697	Run_052	13	Rudder angles = -35, -30, -20 deg	9.96	50	-20	
*	15:44	0:10	1.697	Run_053	13	Rudder angles = -10, 0, 10 deg	9.96	51	-20	
*	15:54	0:12	1.697	Run_054	13	Rudder angles = 20, 30, 35 deg	9.96	52	-20	
*	16:06	#####	1.697	Run_055	13	Rudder angles = 20, 30, 35 deg	9.96	53	-20	Repeat run with Optical Isolation box installed on the PMM Das Trigger Model on charge
15-Jun-12	8:23			xpull_PMM_003						rezero rudder angle and pmmd yaw
*	8:51		0.00	Insitu_003		Bollard, carriage at 90m	6.00	N/A	N/A	rezero sinkage and pmmd sway
*	9:09		1.697	yaw sweep_005	46	yaw sweep @0.10, 20deg	6.00	N/A	N/A	rudder commanded to +0.75deg offset
*	9:28		1.358	Run_056	N/A	Self propulsion determination runs, rudder programmed to 0.75 deg	various	53	0	8.96, 9.16, 9.36, 9.56, 9.76 m/s
*	9:41		1.018	Run_057	N/A	Self propulsion determination runs, rudder programmed to 0.75 deg	various	54	0	8.52, 8.62, 8.67, 8.72, 8.81, 8.91 m/s
*	10:00		0.584	Run_058	N/A	Self propulsion determination runs, rudder programmed to 0.75 deg	various	55	0	8.09, 8.12, 8.17, 8.22, 8.27, 8.34 m/s

DATE	TIME	WAIT TIME ACTUAL	Speed (m/s)	FILENAME(DAQ)	PMI DRIVE SIGNAL (VORG007?)J.MDF	RUN DESCRIPTION	RPS	Video Track #	Yaw Angle	COMMENTS
*	10:24	0:12	0.584	Run_059	N/A	Reduced speed runs	9.96	56	0	
*	10:36	0:11	1.018	Run_060	N/A	Reduced speed runs	9.96	57	0	-10, 0, 10, 20, 30, 35 deg. labeled run_059 on annotator
*	10:47	0:11	1.358	Run_061	N/A	Reduced speed runs	9.96	58	0	
*	10:58	0:11	0.594	Run_062	N/A	Reduced speed runs	8.05	59	0	
*	11:09	0:13	0.594	Run_063	N/A	Reduced speed runs	8.05	60	0	
*	11:22	0:10	1.018	Run_064	N/A	Reduced speed runs	8.71	61	0	
*	11:32	0:12	1.018	Run_065	N/A	Reduced speed runs	8.71	62	0	
*	11:44	0:10	1.358	Run_066	N/A	Reduced speed runs	9.27	63	0	
*	11:54	0:14	1.358	Run_067	N/A	Reduced speed runs	9.27	64	0	
*	12:08	0:10	1.697	Run_068	33	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	65		
*	12:18	0:11	1.697	Run_069	32	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	66		
*	12:29	0:11	1.697	Run_070	34	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	67		
*	12:40	0:20	1.697	Run_071	35	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	68		
*	13:00	0:11	1.697	Run_072	36	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	69		Shaft speed(Solist) was unplugged to see if it made a difference to the noise issue.
*	13:11	0:11	1.697	Run_073	37	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	70		Shaft speed(Solist) unplugged made no difference.
*	13:22	0:09	1.697	Run_074	37	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	71		shaft speed missed, repeat run
*	13:31	0:16	1.690	Run_075	22	Harmonic Yaw & Rudder. Rudder: 10, 20deg	9.96	72		
*	13:47	0:10	1.690	Run_076	22	Harmonic Yaw & Rudder. Rudder: -10, -20deg	9.96	73		
*	13:57	0:10	1.690	Run_077	22	Harmonic Yaw & Rudder. Rudder: 30, 35deg	9.96	74		
*	14:07	0:10	1.690	Run_078	22	Harmonic Yaw & Rudder. Rudder: -30, -35deg	9.96	75		
*	14:17	0:10	1.668	Run_079	24	Harmonic Yaw & Rudder. Rudder: 10, 20deg	9.96	76		
*	14:27	0:12	1.668	Run_080	24	Harmonic Yaw & Rudder. Rudder: -10, -20deg	9.96	77		
*	14:39	0:12	1.668	Run_081	24	Harmonic Yaw & Rudder. Rudder: 30, 35deg	9.96	78		
*	14:51	0:12	1.668	Run_082	24	Harmonic Yaw & Rudder. Rudder: -30, -35deg	9.96	79		
*	15:03	0:12	1.633	Run_083	26	Harmonic Yaw & Rudder. Rudder: 10, 20deg	9.96	80		
*	15:15	0:12	1.633	Run_084	26	Harmonic Yaw & Rudder. Rudder: -10, -20deg	9.96	81		
*	15:27	0:12	1.633	Run_085	26	Harmonic Yaw & Rudder. Rudder: 30, 35deg	9.96	82		
*	15:39	#####	1.633	Run_086	26	Harmonic Yaw & Rudder. Rudder: -30, -35deg	9.96	83		Charge model

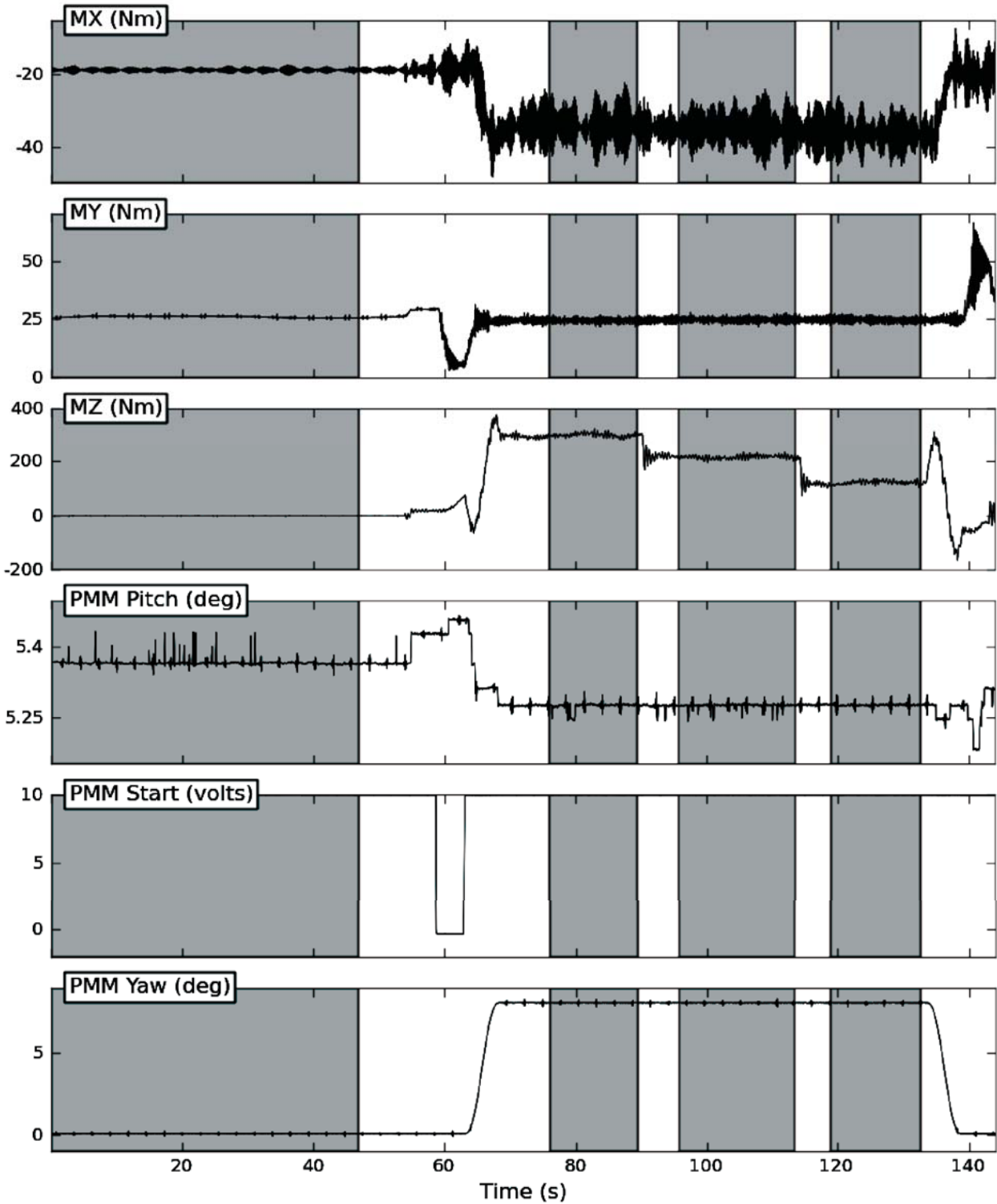
DATE	TIME	WAIT TIME ACTUAL	Speed (m/s)	FILENAME(DAQ)	PMI DRIVE SIGNAL (VORG007?)J.MDF	RUN DESCRIPTION	RPS	Video Track #	Yaw Angle	COMMENTS
18-Jun-12	8:30			xpull_PMI_004		x pull				
*	8:45									
*	8:52		0.00	Instu_004		Bollard, carriage at 90m				rezero rudder angle and pmv yaw
*	9:01		1.697	yaw_sweep_007	46	yaw sweep @0, 10, 20deg	6.00	N/A	N/A	rudder commanded to +0.75deg offset
*	9:13		1.697	yaw_sweep_008	47	yaw sweep @0, -10, -20deg	6.00	N/A	N/A	rudder commanded to +0.75deg offset
*	9:26	0:12	1.681	Run_087	31	Harmonic Yaw & Drift. Yaw amp.: 8deg/s, Period = 14, Static Yaw: 4deg	9.96	84	4	rudder commanded to +0.75deg offset
*	9:38	0:12	1.681	Run_088	30	Harmonic Yaw & Drift. Yaw amp.: 5deg/s, Period = 14, Static Yaw: 8deg	9.96	85	8	rudder commanded to +0.75deg offset
*	9:50	0:13	1.681	Run_089	38	Harmonic Yaw & Drift. Yaw amp.: 5deg/s, Period = 14, Static Yaw: -8deg	9.96	86	-8	rudder commanded to +0.75deg offset
*	10:03	0:12	1.681	Run_090	29	Harmonic Yaw & Drift. Yaw amp.: 5deg/s, Period = 14, Static Yaw: 12deg	9.96	87	12	rudder commanded to +0.75deg offset
*	10:15	0:12	1.653	Run_091	40	Harmonic Yaw & Drift. Yaw amp.: 8.3deg/s, Period = 14, Static Yaw: 4deg	9.96	88	4	rudder commanded to +0.75deg offset
*	10:27	0:12	1.653	Run_092	41	Harmonic Yaw & Drift. Yaw amp.: 8.3deg/s, Period = 14, Static Yaw: 8deg	9.96	89	8	rudder commanded to +0.75deg offset
*	10:39	0:12	1.653	Run_093	42	Harmonic Yaw & Drift. Yaw amp.: 8.3deg/s, Period = 14, Static Yaw: -8deg	9.96	90	-8	rudder commanded to +0.75deg offset
*	10:51	0:12	1.653	Run_094	43	Harmonic Yaw & Drift. Yaw amp.: 8.3deg/s, Period = 14, Static Yaw: 12deg	9.96	91	12	rudder commanded to +0.75deg offset
*	11:03	0:12	1.688	Run_095	24	yaw amp.: 6.7deg/s, period: 14s, Rudder command: -0.75deg offset	9.96	92		Repeatability check runs
*	11:15	0:12	1.697	Run_096	16	sway amp.: 0.410m/s, period: 16s, Rudder command: -0.75deg offset	9.96	93	0	
*	11:27	0:12	1.697	Run_097	36	Combined sway / yaw. Rudder command: -0.75deg offset	9.96	94	0	
*	11:39	0:12	1.653	Run_098	40	Harmonic Yaw & Drift. Yaw amp.: 8.3deg/s, Period = 14, Static Yaw: 4deg	9.96	95		rudder commanded to +0.75deg offset
*	11:51	0:12	1.653	Run_099	40	Harmonic Yaw & Drift. Yaw amp.: 8.3deg/s, Period = 14, Static Yaw: 4deg	9.96	96		rudder commanded to -0.75deg offset
*	12:03	0:12	1.668	Run_100	24	Harmonic Yaw & Rudder. Rudder: -10, -20deg	9.96	97		Rudder Sweep
*	12:15	0:12	1.697	Run_101	N/A	angles = -20, -10, 20 deg	9.96	98	0	
*	12:27	0:12	1.697	Run_102	6	Rudder angles = -10, 0, 10 deg	9.96	99	12	
*	12:39	1:00	1.697	Run_103	N/A	angles = -10, -7.5, 10 deg	9.96	100	0	
*	13:39			friction_002						

APPENDIX D
Example SWEET Output Files

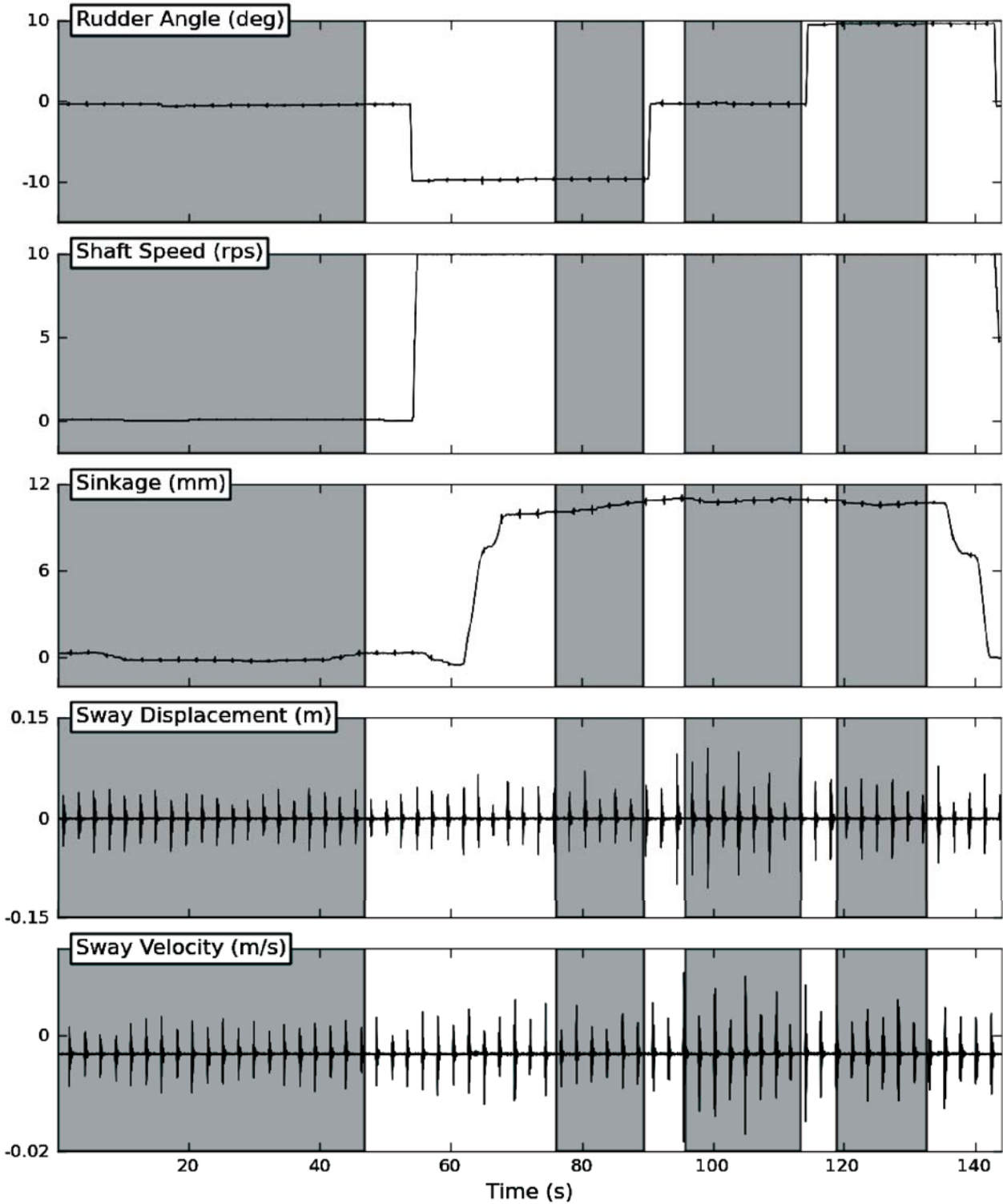
JSS
RUN_118



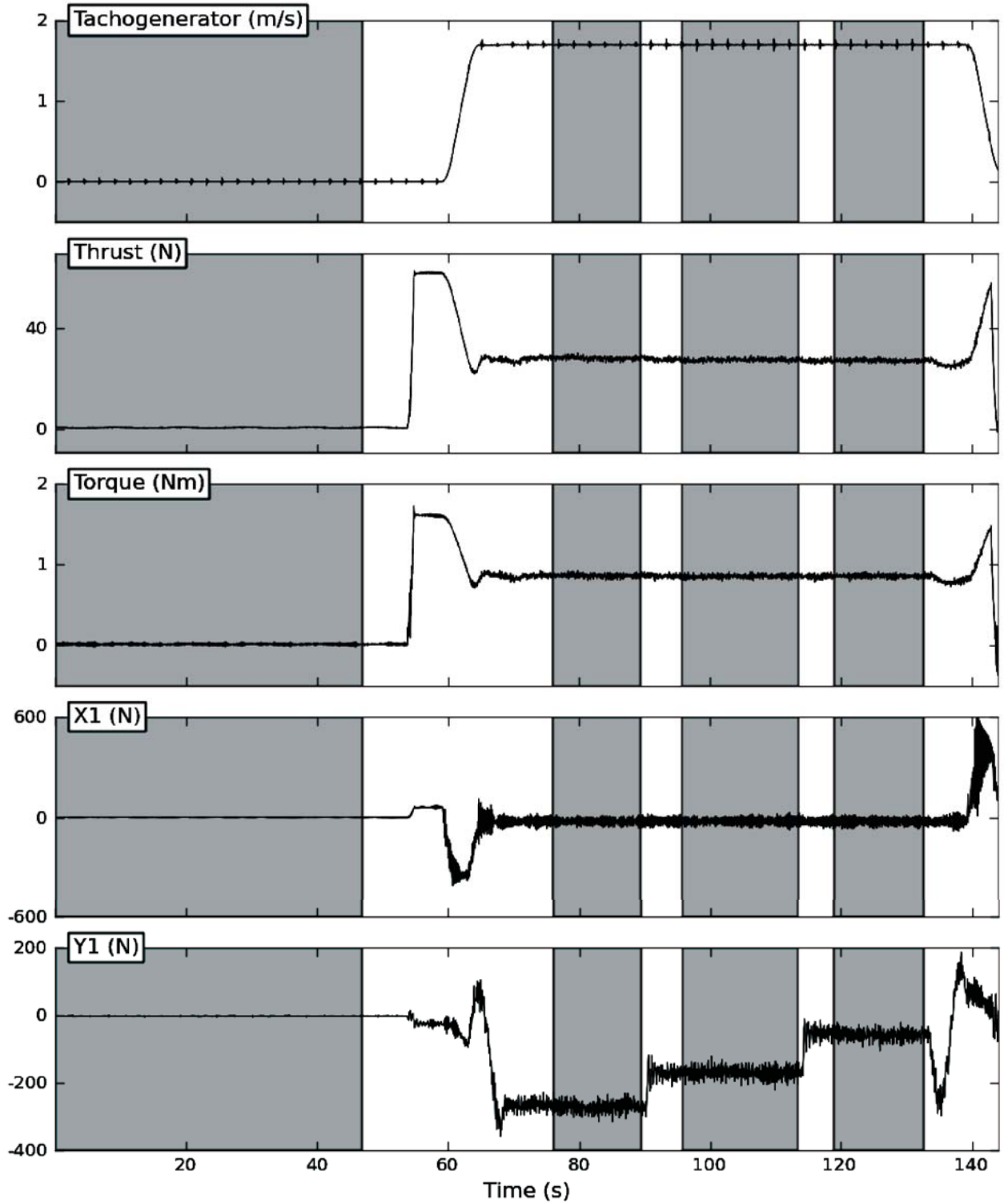
JSS
RUN_118



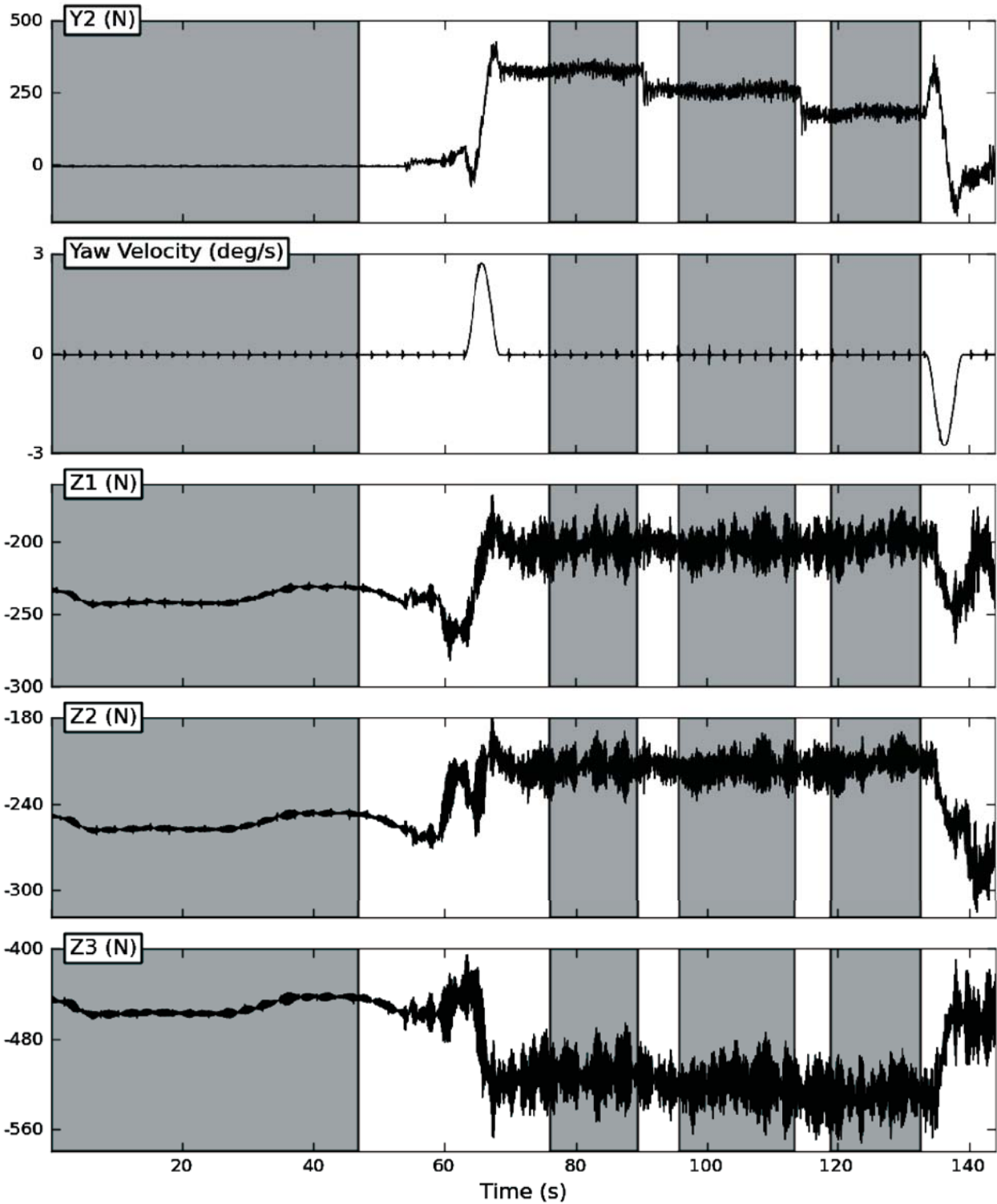
JSS
RUN_118



JSS
RUN_118



JSS
RUN_118



JSS
RUN_118
Segment 1, After Taring (0.00 to 46.87 s)

Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	-0.010207	0.026549	0.0073013	0.0027407
DAS Trigger	volts	-0.048511	0.059544	0.0000	0.0077435
FX	N	-3.8869	3.7878	0.0000	1.4227
FY	N	-5.0447	4.9655	0.0000	1.5942
FZ	N	-19.100	26.870	0.0000	15.566
Inline Load	N	-4.9593	4.6507	0.0000	0.66055
MX	Nm	-1.3948	1.3291	0.0000	0.44627
MY	Nm	-1.5399	1.5869	0.0000	0.37457
MZ	Nm	-1.9190	2.0100	0.0000	0.36270
PMM Pitch	deg	5.3395	5.4336	5.3665	0.0082734
PMM Start	volts	-0.011390	0.0098401	0.0000	0.0014548
PMM Yaw	deg	-0.095113	0.23559	0.073135	0.022332
Rudder Angle	deg	-0.83138	-0.10015	-0.50083	0.085774
Shaft Speed	rps	-0.012740	0.12269	0.075014	0.030900
Sinkage	mm	-0.35332	0.56900	0.0000	0.20118
Sway Displacement	m	-0.050236	0.044550	0.0000	0.0078285
Sway Velocity	m/s	-0.0067011	0.0064858	0.0000	0.0010471
Tachogenerator	m/s	-0.048124	0.051339	-0.00057763	0.0069949
Thrust	N	-0.30889	0.38964	0.0000	0.094562
Torque	Nm	-0.026500	0.041568	0.011034	0.010395
X1	N	-3.9109	3.7953	0.0000	1.4167
Y1	N	-3.5730	4.1674	0.0000	0.90573
Y2	N	-3.5429	3.1491	0.0000	0.84596
Yaw Velocity	deg/s	-0.13751	0.13537	0.0000	0.021444
Z1	N	-7.8274	10.579	0.0000	4.7510
Z2	N	-7.8964	10.246	0.0000	4.7806
Z3	N	-10.073	13.070	0.0000	6.5007

JSS
RUN_118
Segment 2, After Taring (76.06 to 89.46 s)

Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	1.6816	1.7253	1.7016	0.0035104
DAS Trigger	volts	-0.056142	0.055271	0.0019775	0.0085869
FX	N	-64.452	16.810	-22.366	17.320
FY	N	-12.691	137.35	66.150	25.526
FZ	N	-13.533	32.087	15.703	9.1613
Inline Load	N	-5.0239	5.2971	0.022127	0.79343
MX	Nm	-26.650	-3.4304	-15.411	4.3271
MY	Nm	-4.4211	0.90950	-1.5202	0.97478
MZ	Nm	283.13	326.09	302.68	7.4699
PMM Pitch	deg	5.2427	5.3057	5.2743	0.0084021
PMM Start	volts	-0.012974	0.012692	-0.00086561	0.0023991
PMM Yaw	deg	7.8268	8.3003	8.0696	0.033690
Rudder Angle	deg	-10.061	-9.3091	-9.7008	0.051501
Shaft Speed	rps	9.9126	9.9857	9.9487	0.0062742
Sinkage	mm	9.9687	10.899	10.454	0.25069
Sway Displacement	m	-0.048656	0.071011	0.00042825	0.0075692
Sway Velocity	m/s	-0.0059319	0.0083539	1.0447e-05	0.0011258
Tachogenerator	m/s	1.6470	1.7612	1.6964	0.0091308
Thrust	N	25.639	29.737	27.615	0.63418
Torque	Nm	0.80102	0.92302	0.85921	0.020626
X1	N	-65.956	15.226	-23.955	17.310
Y1	N	-312.56	-226.15	-268.35	14.661
Y2	N	279.61	372.98	334.50	14.890
Yaw Velocity	deg/s	-0.12285	0.16834	-0.0020982	0.024400
Z1	N	8.2885	64.199	35.748	9.8742
Z2	N	14.071	64.362	39.287	8.9136
Z3	N	-101.49	-13.754	-59.332	16.594



JSS
RUN_118
Segment 3, After Taring (95.77 to 113.52 s)

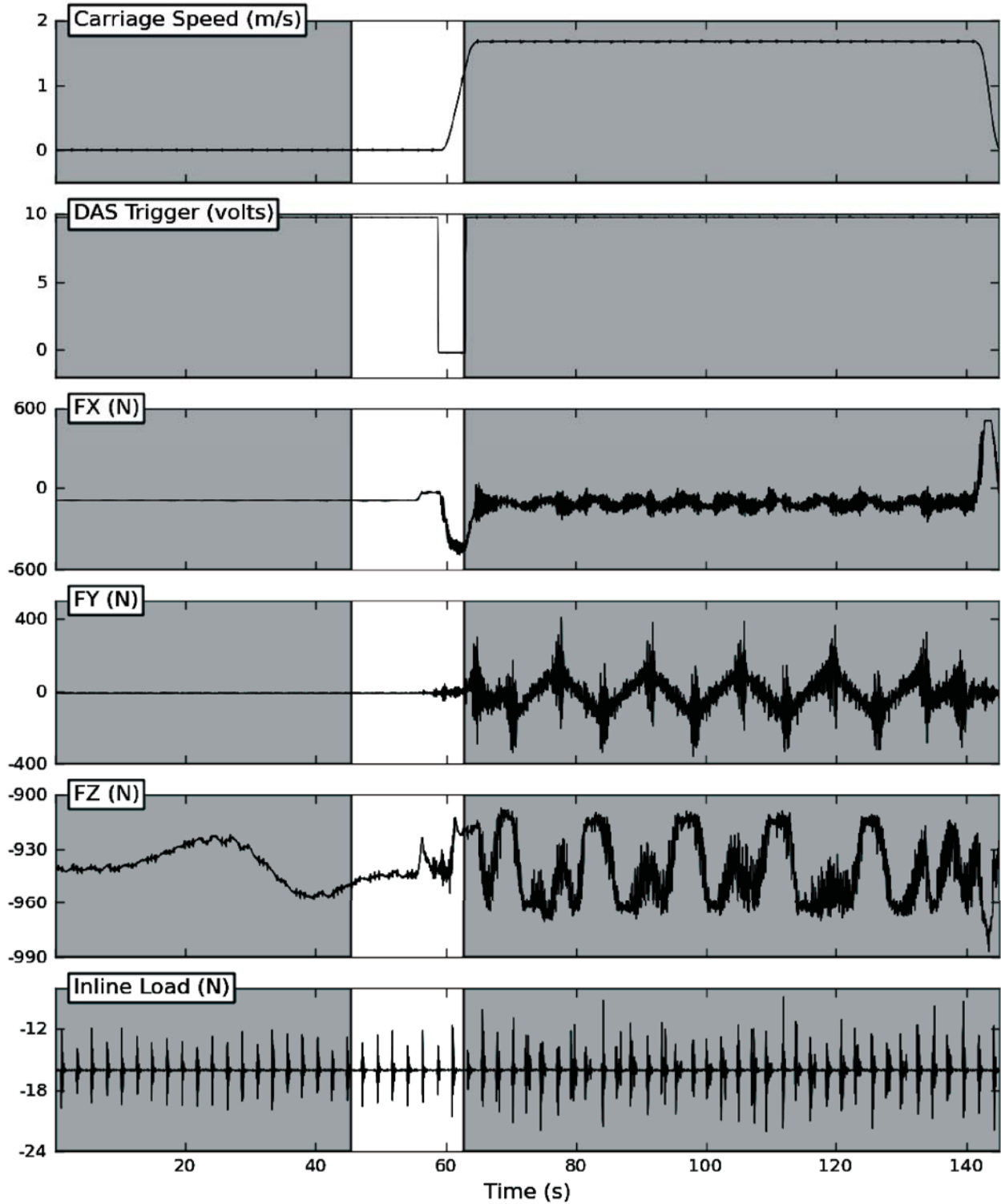
Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	1.6689	1.7344	1.7015	0.0051587
DAS Trigger	volts	-0.10986	0.097089	0.0016829	0.014029
FX	N	-73.883	30.246	-21.513	19.419
FY	N	1.3370	172.35	97.244	27.365
FZ	N	-22.888	29.508	4.5687	10.928
Inline Load	N	-8.0189	7.4949	0.0053910	1.3801
MX	Nm	-27.600	-5.2686	-16.092	4.2744
MY	Nm	-4.4099	1.8624	-1.2309	1.0868
MZ	Nm	196.87	235.84	217.01	6.7111
PMM Pitch	deg	5.2422	5.2984	5.2751	0.0066623
PMM Start	volts	-0.014875	0.0095232	-0.00090246	0.0022989
PMM Yaw	deg	7.8268	8.3228	8.0684	0.032722
Rudder Angle	deg	-0.76218	-0.080392	-0.38056	0.068516
Shaft Speed	rps	9.9086	9.9827	9.9490	0.0063045
Sinkage	mm	10.618	11.196	10.946	0.097353
Sway Displacement	m	-0.10316	0.10458	7.0476e-05	0.015144
Sway Velocity	m/s	-0.013881	0.013409	-1.8380e-05	0.0019019
Tachogenerator	m/s	1.6188	1.7708	1.6962	0.014072
Thrust	N	25.304	28.834	26.957	0.55733
Torque	Nm	0.79117	0.91147	0.85220	0.020247
X1	N	-75.458	28.694	-23.087	19.419
Y1	N	-219.10	-119.43	-166.54	15.138
Y2	N	220.44	306.95	263.78	15.316
Yaw Velocity	deg/s	-0.29501	0.28738	-0.0021410	0.040101
Z1	N	9.9426	62.829	34.806	9.7192
Z2	N	15.848	62.672	38.140	8.6796
Z3	N	-117.23	-22.024	-68.377	17.055

JSS
RUN_118
Segment 4, After Taring (119.04 to 132.65 s)

Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	1.6729	1.7242	1.7016	0.0039574
DAS Trigger	volts	-0.064994	0.069312	0.0014416	0.010473
FX	N	-67.312	20.254	-23.591	20.169
FY	N	63.395	197.97	132.23	24.295
FZ	N	-25.345	29.027	3.3574	11.808
Inline Load	N	-6.8338	6.2236	-0.0036873	0.99088
MX	Nm	-26.735	-7.1840	-17.546	3.9193
MY	Nm	-4.3758	1.4195	-1.2934	1.1320
MZ	Nm	104.66	138.12	123.38	6.3951
PMM Pitch	deg	5.2550	5.2988	5.2765	0.0040581
PMM Start	volts	-0.012340	0.010791	-0.00072439	0.0024346
PMM Yaw	deg	7.8418	8.2402	8.0674	0.030686
Rudder Angle	deg	9.2273	9.9125	9.5697	0.066668
Shaft Speed	rps	9.9155	9.9808	9.9494	0.0064313
Sinkage	mm	10.402	10.987	10.725	0.087747
Sway Displacement	m	-0.060109	0.059162	6.0293e-05	0.010415
Sway Velocity	m/s	-0.0081664	0.0093796	-1.0887e-05	0.0014507
Tachogenerator	m/s	1.6284	1.7633	1.6962	0.011984
Thrust	N	24.624	28.303	26.698	0.54889
Torque	Nm	0.78946	0.91147	0.85535	0.019110
X1	N	-68.887	18.695	-25.142	20.170
Y1	N	-102.49	-18.166	-54.758	13.501
Y2	N	146.62	219.79	186.98	13.920
Yaw Velocity	deg/s	-0.19794	0.17200	-0.0019256	0.031306
Z1	N	9.7128	62.764	38.267	9.4572
Z2	N	18.042	63.521	41.866	8.2287
Z3	N	-120.69	-36.664	-76.776	15.736



JSS
RUN_132

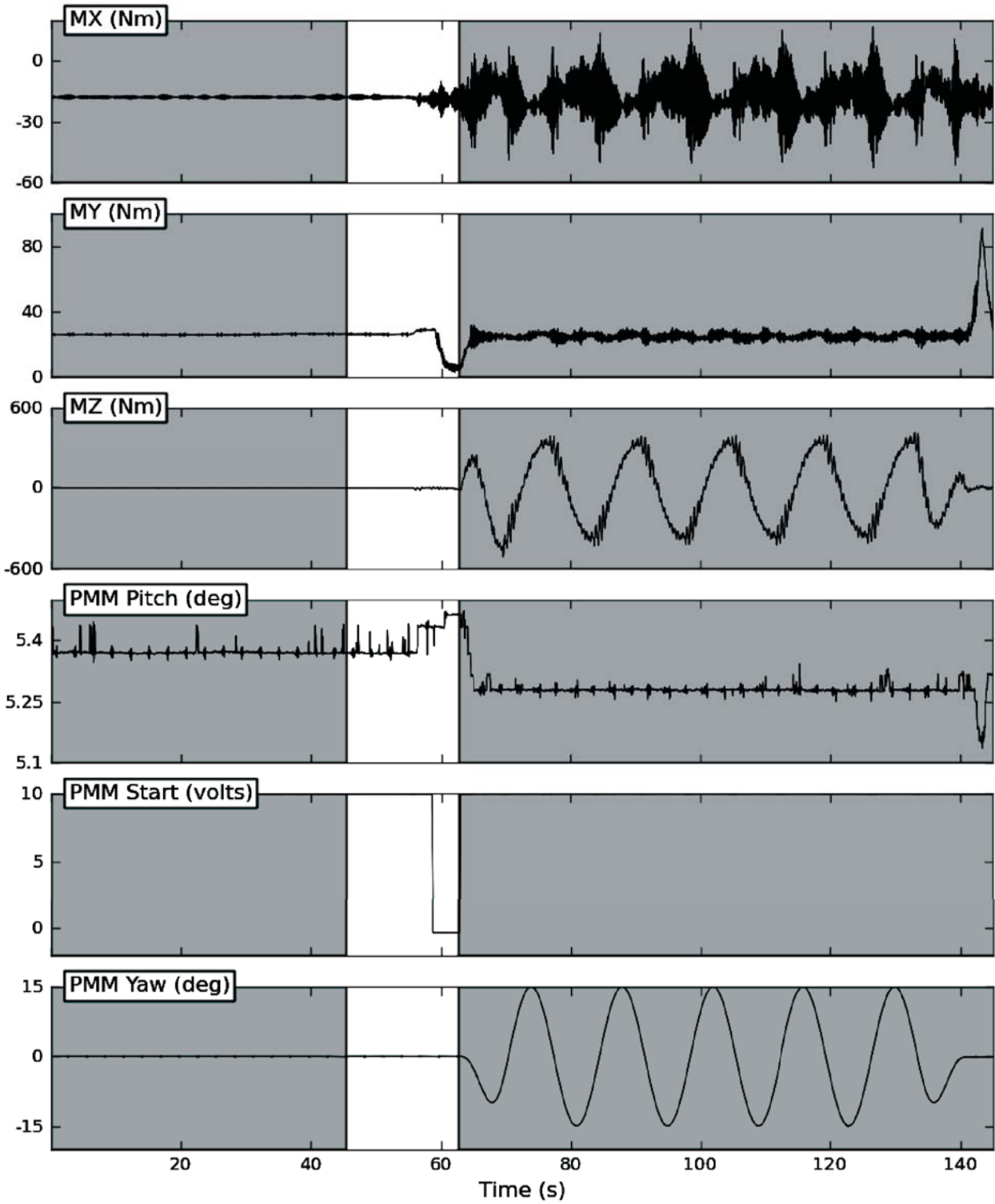


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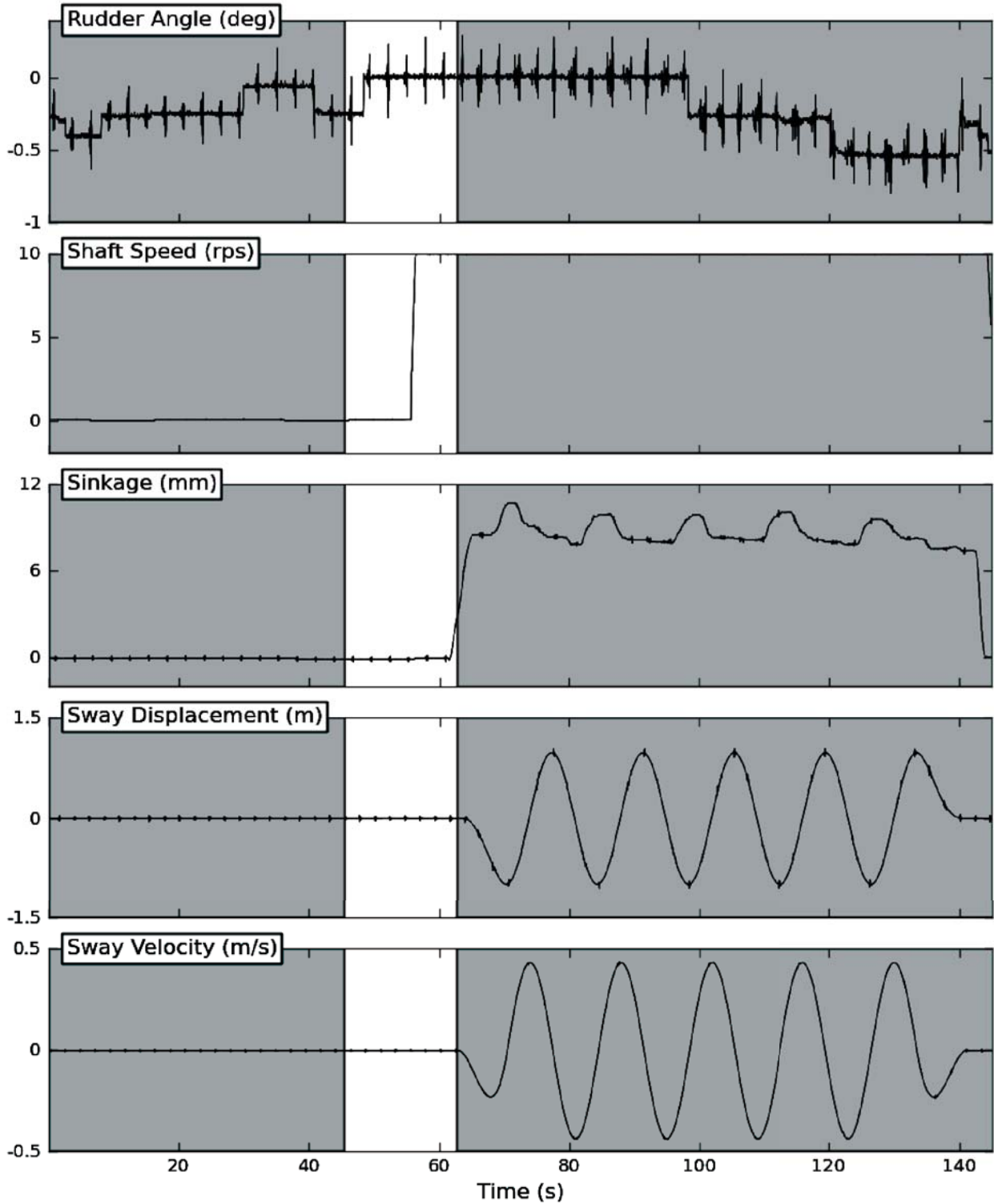
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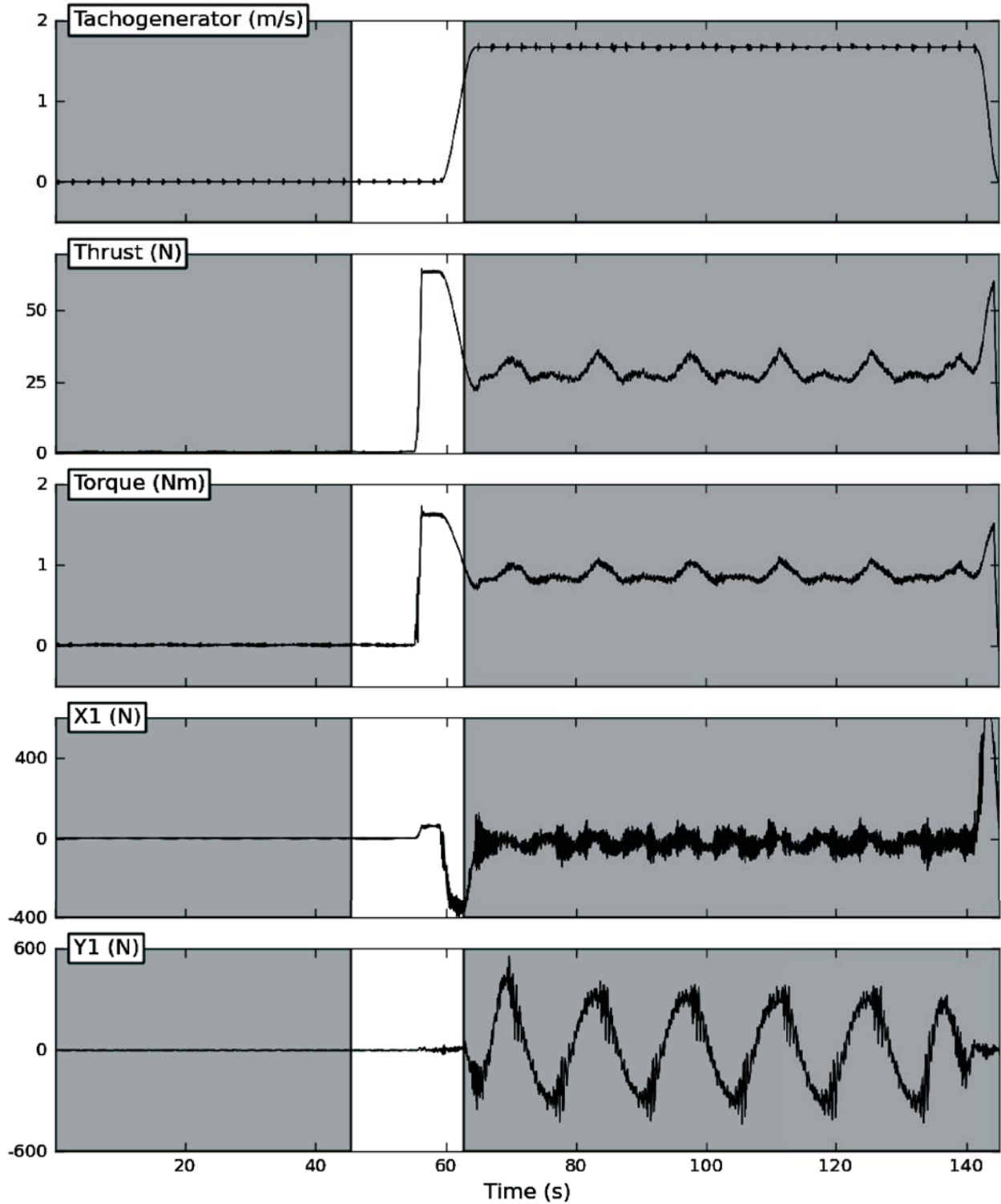


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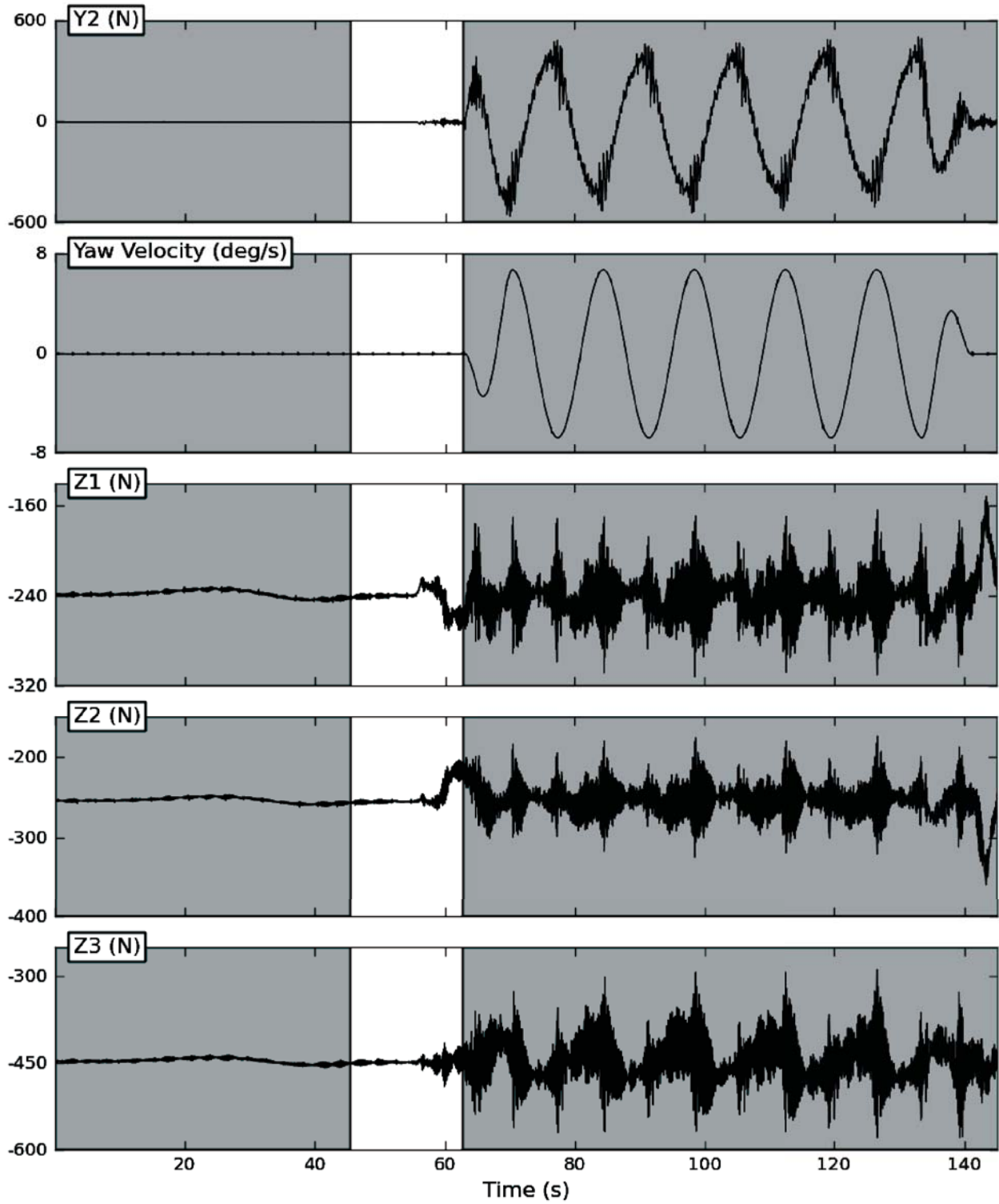


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RUN_132**

Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	-0.010527	1.7004	0.94444	0.81307
DAS Trigger	volts	-0.24391	9.8324	9.4647	1.6624
FX	N	-491.77	507.26	-99.650	91.510
FY	N	-357.96	405.47	-8.6443	64.195
FZ	N	-986.95	-907.18	-940.70	15.263
Inline Load	N	-22.064	-8.8988	-16.071	0.67565
MX	Nm	-52.374	16.743	-17.851	6.7940
MY	Nm	2.6699	91.163	25.611	6.3258
MZ	Nm	-511.84	416.43	-10.066	180.94
PMM Pitch	deg	5.1367	5.4728	5.3243	0.054431
PMM Start	volts	-0.33812	9.9842	9.6669	1.7238
PMM Yaw	deg	-15.007	14.982	-0.085603	7.2387
Rudder Angle	deg	-0.80104	0.29383	-0.20077	0.19183
Shaft Speed	rps	-0.0028543	9.9986	6.1271	4.7982
Sinkage	mm	-0.31042	10.701	4.6976	4.3223
Sway Displacement	m	-1.0460	1.0341	-0.0022409	0.48728
Sway Velocity	m/s	-0.44178	0.43724	-0.0032428	0.20913
Tachogenerator	m/s	-0.047766	1.7426	0.93781	0.81390
Thrust	N	0.13440	64.576	19.458	16.477
Torque	Nm	-0.065029	1.7296	0.57409	0.47100
X1	N	-397.54	596.15	-7.8337	91.222
Y1	N	-437.97	554.86	5.5794	162.81
Y2	N	-567.71	500.51	-14.224	201.24
Yaw Velocity	deg/s	-6.7042	6.6705	-0.022959	3.2761
Z1	N	-312.78	-151.57	-239.67	15.959
Z2	N	-358.65	-174.54	-253.86	16.688
Z3	N	-578.53	-288.43	-447.17	29.348



JSS
RUN_132
Segment 1, After Taring (0.00 to 45.38 s)

Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	-0.0087107	0.023344	0.0071393	0.0019307
DAS Trigger	volts	9.7033	9.8022	9.7506	0.0075004
FX	N	-3.4957	3.1827	0.0000	1.1545
FY	N	-4.4361	5.7407	0.0000	1.4063
FZ	N	-18.950	16.868	0.0000	9.9959
Inline Load	N	-3.9034	4.1120	0.0000	0.48021
MX	Nm	-1.3812	1.4565	0.0000	0.40593
MY	Nm	-1.3010	1.4407	0.0000	0.24004
MZ	Nm	-1.5161	1.4536	0.0000	0.38176
PMM Pitch	deg	-0.025848	0.073707	0.0000	0.010296
PMM Start	volts	9.9525	9.9731	9.9625	0.0015998
PMM Yaw	deg	-0.15524	0.10782	-0.032345	0.016341
Rudder Angle	deg	-0.63327	0.20511	-0.22607	0.10897
Shaft Speed	rps	-0.0028543	0.11577	0.059580	0.037180
Sinkage	mm	-0.22104	0.22007	0.0000	0.035718
Sway Displacement	m	-0.048864	0.043552	0.0000	0.0052570
Sway Velocity	m/s	-0.0070298	0.0066699	0.0000	0.00075040
Tachogenerator	m/s	-0.047766	0.045972	-0.00051623	0.0049455
Thrust	N	-0.35086	0.32904	0.0000	0.098277
Torque	Nm	-0.025644	0.036858	0.0089337	0.0078295
X1	N	-3.2248	3.2174	0.0000	1.1399
Y1	N	-2.8057	3.4213	0.0000	0.81067
Y2	N	-3.3287	3.4289	0.0000	0.78927
Yaw Velocity	deg/s	-0.12498	0.12684	0.0000	0.014603
Z1	N	-7.4594	6.3374	0.0000	3.1190
Z2	N	-8.1416	6.5942	0.0000	3.1232
Z3	N	-11.321	10.203	0.0000	4.3353

JSS
RUN_132
Segment 2, After Taring (62.77 to 145.13 s)

Channel	Units	Min	Max	Mean	SD
Carriage Speed	m/s	0.023985	1.7004	1.6391	0.18814
DAS Trigger	volts	-0.18592	9.8324	9.7369	0.40054
FX	N	-369.85	598.50	-5.5415	105.43
FY	N	-349.62	413.81	-0.79319	85.165
FZ	N	-48.108	31.658	-2.9616	18.375
Inline Load	N	-5.9935	7.1717	-0.0015147	0.79372
MX	Nm	-34.566	34.551	0.028990	8.9770
MY	Nm	-21.523	65.254	0.030765	7.6007
MZ	Nm	-509.22	419.04	-12.831	240.16
PMM Pitch	deg	-0.23500	0.10111	-0.089275	0.027108
PMM Start	volts	-0.33463	9.9842	9.9587	0.28501
PMM Yaw	deg	-15.007	14.982	-0.12653	9.6135
Rudder Angle	deg	-0.80104	0.29383	-0.22167	0.22295
Shaft Speed	rps	5.7408	9.9986	9.9293	0.25466
Sinkage	mm	0.043628	10.791	8.4284	1.5097
Sway Displacement	m	-1.0453	1.0348	-0.0027004	0.64713
Sway Velocity	m/s	-0.43850	0.44052	6.0847e-05	0.27775
Tachogenerator	m/s	-0.0073370	1.7426	1.6308	0.20083
Thrust	N	3.3280	59.657	28.737	4.6527
Torque	Nm	-0.065029	1.5168	0.87961	0.10831
X1	N	-368.24	594.76	-7.0811	105.16
Y1	N	-436.26	556.57	12.420	216.07
Y2	N	-561.08	507.13	-13.213	267.11
Yaw Velocity	deg/s	-6.6814	6.6933	-0.00024106	4.3510
Z1	N	-74.114	87.102	-1.0937	20.622
Z2	N	-104.75	79.364	-0.84681	21.024
Z3	N	-132.27	157.84	-1.0211	38.680

APPENDIX E
Static Tests: Table of Measured Data

Model configuration	Test Name	PMW Yaw Angle [deg]	PMW Azimuth [deg]	Acquisition Time [sec]	TEMP [Celsius]	FX	FY	FZ [N]	MX	MY	MZ	PMW Pitch Speed [rpm]	Skinkage [rpm]	Carriage Speed [Rachogenerator] [rpm]	Thrust [N]	Torque [Nm]	Time selection length [Model lengths]	$\Delta u'$	v	r	d'	$1000^\circ X$	$1000^\circ Y$	$1000^\circ K$	$1000^\circ N$	
contract design with Rudder 2	RUN_126	-20	9.6	1107/2012/1543	18	-35.3	-331.6	9.0	64.1	-2.6	-478.9	5106	9.95	25.0	1.696	21.5	0.73	1.9	-0.061	0.342	0.000	0.167	-0.774	-6.694	0.220	-2.334
contract design with Rudder 2	RUN_141	0	-10.8	1107/2012/1141	18	-17.1	-37.8	-5.8	1.2	-0.2	-0.8	3.74	9.95	7.7	1.697	31.3	0.93	2.7	0.000	0.000	0.000	-0.188	-0.345	-0.763	0.004	0.369
contract design with Rudder 2	RUN_141	0	8.6	1107/2012/1141	18	-12.9	0.7	-0.7	0.2	-0.8	-0.8	5.311	9.95	7.7	1.697	31.3	0.92	2.7	0.000	0.000	0.000	-0.101	-0.259	0.014	-0.001	-0.013
contract design with Rudder 2	RUN_141	0	-11.0	1107/2012/1141	18	-14.8	3.9	2.1	-1.4	-0.9	-10.1	5.311	9.95	7.7	1.697	31.0	0.91	2.5	0.000	0.000	0.000	-0.150	-0.289	0.684	-0.005	-0.348
contract design with Rudder 2	RUN_142	4	-0.3	1107/2012/1153	18	-20.9	3.4	8.8	-5.5	-1.4	22.1	5.311	9.95	8.4	1.696	30.4	0.89	3.0	-0.003	-0.070	0.000	-0.192	-0.422	0.068	-0.019	0.762
contract design with Rudder 2	RUN_142	4	8.6	1107/2012/1153	18	-20.9	8.3	11.6	-5.8	-1.3	-1.2	5.312	9.95	8.5	1.696	29.8	0.88	2.3	-0.003	-0.070	0.000	-0.160	-0.421	0.954	-0.026	0.361
contract design with Rudder 2	RUN_142	8	-10.7	1107/2012/1205	18	-25.9	5.7	2.8	-15.2	-1.4	32.0	5.276	9.95	10.6	1.696	29.9	0.90	2.7	-0.010	-0.138	0.000	-0.167	-0.443	1.164	-0.052	1.128
contract design with Rudder 2	RUN_143	8	-10.8	1107/2012/1205	18	-25.9	5.7	2.8	-15.2	-1.4	32.0	5.276	9.95	10.6	1.696	29.9	0.90	2.7	-0.010	-0.138	0.000	-0.167	-0.443	1.164	-0.052	1.128
contract design with Rudder 2	RUN_143	8	8.6	1107/2012/1205	18	-20.4	13.0	4.5	-18.1	-1.3	10.0	5.261	9.95	10.9	1.696	29.0	0.90	2.0	-0.010	-0.138	0.000	-0.150	-0.486	2.818	-0.062	0.347
contract design with Rudder 2	RUN_144	12	-10.9	1107/2012/1217	18	-30.6	12.6	1.1	-29.0	-1.5	40.4	5.249	9.95	15.0	1.696	26.5	0.84	2.5	-0.022	-0.208	0.000	-0.190	-0.619	2.476	-0.097	1.513
contract design with Rudder 2	RUN_144	12	8.6	1107/2012/1217	18	-31.6	20.3	-3.2	-30.3	-1.6	19.7	5.258	9.95	14.8	1.696	26.5	0.84	2.8	-0.022	-0.208	0.000	-0.150	-0.638	4.186	-0.104	0.678
contract design with Rudder 2	RUN_145	16	-11.0	1107/2012/1229	18	-33.3	22.1	8.8	-46.5	-2.0	58.6	5.187	9.95	19.9	1.696	25.2	0.82	2.5	-0.039	-0.276	0.000	-0.181	-0.673	4.471	-0.160	1.921
contract design with Rudder 2	RUN_145	16	8.6	1107/2012/1229	18	-31.2	28.8	1.7	-47.4	-1.8	42.4	5.196	9.95	20.1	1.697	24.4	0.81	2.9	-0.039	-0.276	0.000	-0.008	-0.629	5.412	-0.163	1.460
contract design with Rudder 2	RUN_146	20	-10.9	1107/2012/1241	18	-36.1	31.1	2.8	-48.9	-1.9	30.1	5.226	9.95	20.2	1.697	24.4	0.81	2.9	-0.039	-0.276	0.000	-0.150	-0.729	6.284	-0.168	1.037
contract design with Rudder 2	RUN_146	20	-0.5	1107/2012/1241	18	-35.2	38.7	6.9	-68.8	-2.3	55.1	5.150	9.95	26.0	1.697	24.2	0.79	2.6	-0.060	-0.342	0.000	-0.190	-0.744	6.794	-0.226	2.358
contract design with Rudder 2	RUN_147	24	-10.8	1107/2012/1253	18	-38.9	38.6	1.8	-65.8	-2.3	68.1	5.150	9.95	25.9	1.697	23.4	0.78	2.8	-0.060	-0.342	0.000	-0.008	-0.710	7.820	-0.230	1.908
contract design with Rudder 2	RUN_147	24	-0.8	1107/2012/1253	18	-32.3	49.3	8.5	-97.0	-1.6	83.2	5.310	9.95	33.9	1.696	28.5	0.88	2.8	-0.003	0.070	0.000	-0.189	-0.484	-1.748	0.033	0.038
contract design with Rudder 2	RUN_147	4	-0.4	1107/2012/1253	18	-18.1	-41.5	5.8	6.7	-1.2	-115.2	5.310	9.95	8.5	1.696	28.5	0.88	2.8	-0.003	0.070	0.000	-0.006	-0.366	-0.838	0.023	-0.396
contract design with Rudder 2	RUN_147	8	8.6	1107/2012/1253	18	-18.2	-8.3	3.8	5.6	-1.3	-212.5	5.310	9.95	8.4	1.696	29.6	0.88	2.2	-0.003	0.070	0.000	-0.151	-0.389	-0.168	0.019	-0.731
contract design with Rudder 2	RUN_148	-8	-10.8	1107/2012/1305	18	-26.7	-140.6	10.3	17.4	-1.8	-89.3	5.280	9.95	10.8	1.697	28.4	0.87	3.0	-0.010	0.139	0.000	-0.188	-0.539	-2.838	0.060	-0.307
contract design with Rudder 2	RUN_148	-8	8.7	1107/2012/1305	18	-19.1	-87.7	-0.9	14.5	-1.2	-213.8	5.277	9.95	10.6	1.696	28.8	0.90	3.0	-0.010	0.139	0.000	-0.005	-0.386	-1.770	0.050	-0.735
contract design with Rudder 2	RUN_148	-8	8.7	1107/2012/1305	18	-19.4	-54.3	1.5	13.1	-1.3	-308.9	5.279	9.95	10.4	1.696	30.9	0.91	1.9	-0.010	0.139	0.000	-0.151	-0.392	-1.096	0.045	-1.065
contract design with Rudder 2	RUN_149	-12	-10.7	1107/2012/1317	18	-35.8	-204.3	0.5	28.1	-2.1	-167.6	5.264	9.95	15.0	1.696	23.9	0.78	2.9	-0.022	0.208	0.000	-0.187	-0.722	-4.124	0.097	-0.576
contract design with Rudder 2	RUN_149	-12	8.6	1107/2012/1317	18	-27.8	-161.2	1.2	26.0	-1.8	-311.9	5.246	9.95	14.4	1.696	24.8	0.80	3.0	-0.022	0.208	0.000	-0.005	-0.552	-3.053	0.089	-1.072
contract design with Rudder 2	RUN_149	-12	8.6	1107/2012/1317	18	-27.8	-161.8	-2.5	25.7	-1.7	-421.5	5.246	9.95	14.2	1.696	25.6	0.81	2.0	-0.022	0.208	0.000	-0.150	-0.562	-2.387	0.088	-1.449
contract design with Rudder 2	RUN_150	-16	-10.8	1107/2012/1329	18	-31.5	-245.9	2.2	43.2	-1.6	-427.2	5.246	9.95	20.0	1.696	23.7	0.77	2.5	-0.039	0.276	0.000	-0.168	-0.694	-4.474	0.195	-0.469
contract design with Rudder 2	RUN_150	-16	8.6	1107/2012/1329	18	-32.3	-245.5	-0.7	43.1	-1.9	-536.6	5.187	9.95	19.4	1.696	23.7	0.77	2.5	-0.039	0.276	0.000	-0.150	-0.694	-4.474	0.195	-0.469
contract design with Rudder 2	RUN_150	-16	8.6	1107/2012/1329	18	-32.3	-207.6	-2.7	43.1	-1.9	-536.6	5.187	9.95	19.4	1.696	23.7	0.77	2.5	-0.039	0.276	0.000	-0.150	-0.694	-4.474	0.195	-0.469
contract design with Rudder 2	RUN_151	-20	-10.7	1107/2012/1341	18	-45.1	-417.1	6.2	65.0	-2.8	-393.6	5.173	9.95	25.0	1.697	22.9	0.76	2.7	-0.061	0.342	0.000	-0.187	-0.911	-8.420	0.223	-1.353
contract design with Rudder 2	RUN_151	-20	8.9	1107/2012/1341	18	-37.7	-370.7	6.9	64.5	-2.5	-683.4	5.151	9.95	25.6	1.696	23.6	0.77	3.0	-0.061	0.342	0.000	-0.155	-0.761	-6.699	0.222	-2.344
contract design with Rudder 3	RUN_165	0	-10.5	1107/2012/1721	18	-16.8	-32.8	12.0	1.1	-1.2	93.4	5.307	9.95	7.3	1.697	29.8	0.78	2.1	0.000	0.000	0.000	-0.184	-0.338	-0.661	0.004	0.321
contract design with Rudder 3	RUN_165	0	-0.7	1107/2012/1721	18	-14.3	3.1	10.8	-2.0	-1.1	-80.6	5.308	9.95	7.4	1.697	29.7	0.89	2.8	0.000	0.000	0.000	-0.012	-0.260	0.011	-0.002	0.034
contract design with Rudder 3	RUN_166	4	-10.4	1107/2012/1733	18	-20.0	7.6	14.2	5.3	-1.4	201.0	5.298	9.95	8.4	1.697	30.0	0.89	2.5	-0.003	0.000	0.000	-0.181	-0.403	0.154	-0.018	0.691
contract design with Rudder 3	RUN_166	4	-0.5	1107/2012/1733	18	-17.7	43.3	14.2	1.4	-1.4	112.0	5.307	9.95	8.6	1.696	28.2	0.86	2.5	-0.003	0.000	0.000	-0.009	-0.358	0.873	-0.025	0.385
contract design with Rudder 3	RUN_167	8	-10.4	1107/2012/1746	18	-30.7	62.0	1.9	-4.1	-1.4	172.0	5.277	9.95	10.9	1.697	28.5	0.87	2.6	-0.010	-0.139	0.000	-0.182	-0.470	1.254	-0.052	1.104
contract design with Rudder 3	RUN_167	8	-0.6	1107/2012/1746	18	-21.1	99.3	13.4	-16.8	-1.5	229.3	5.277	9.95	11.3	1.697	28.5	0.87	2.5	-0.010	-0.139	0.000	-0.011	-0.425	2.004	-0.058	0.798
contract design with Rudder 3	RUN_168	12	-10.3	1107/2012/1758	18	-25.5	134.1	11.8	-18.1	-1.6	120.3	5.279	9.95	11.2	1.697	27.6	0.87	2.4	-0.010	-0.139	0.000	-0.161	-0.475	2.707	-0.062	0.414
contract design with Rudder 3	RUN_168	12	-0.5	1107/2012/1758	18	-30.9	125.8	12.1	-28.1	-2.0	427.8	5.245	9.95	14.5	1.697	24.9	0.80	2.4	-0.022	-0.208	0.000	-0.180	-0.624	2.538	-0.097	1.471
contract design with Rudder 3	RUN_168	12	9.3	1107/2012/1758	18	-28.9	167.0	12.6	-30.0	-1.8	326.7	5.246	9.95	15.1	1.697	24.6	0.80	2.7	-0.022	-0.208	0.000	-0.009	-0.583	3.370	-0.103	1.123
contract design with Rudder 3	RUN_169	16	-10.3	1107/2012/1810	18	-33.1	223.2	0.6	-46.2	-1.9	215.3	5.246	9.95	19.6	1.697	24.5	0.81	1.9	-0.022	-0.208	0.000	-0.163	-0.635	4.033	-0.104	0.740
contract design with Rudder 3	RUN_169	16	-0.5	1107/2012/1810	18	-31.5	265.5	7.3	-47.8	-2.0	439.8	5.185	9.95	19.6	1.697	23.9	0.79	2.4	-0.039	-0.276	0.000	-0.008	-0.668	4.503	-0.158	1.879
contract design with Rudder 3	RUN_169	16	9.1	1107/2012/1810	18	-34.4	299.1	1.7	-47.8	-2.1	328.9	5.167	9.95	19.6	1.697	22.9	0.77	2.7	-0.039	-0.276	0.000	-0.169	-0.695	6.035	-0.164	1.512
contract design with Rudder 3	RUN_170	4	-0.6	1107/2012/1822	18	-18.1	-42.5	3.5	6.2	-1.1	-38.3	5.305	9.95	8.2	1.697	27.6	0.85	2.6	-0.002	0.070	0.000	-0.161	-0.394	-0.856	0.027	-0.338
contract design with Rudder 3	RUN_170	4	9.2	1107/2012/1822	18	-19.0	-10.2	4.5	6.2	-1.2	-162.0	5.304	9.95	8.2	1.697	27.6	0.85	2.6	-0.003	0.070	0.000	-0.161	-0.394	-0.206	0.018	-0.660
contract design with Rudder 3	RUN_171	-8	-10.4	1107/2012/1834	18	-25.6	-132.7	1.5	16.9	-1.6	-109.5	5.278	9.95	11.0	1.697	28.1	0.84	3.0	-0.010	0.139	0.000	-0.181	-0.517	-2.677	0.058	-0.376
contract design with Rudder 3	RUN_171	-8	9.4	1107/2012/1834	18	-19.8	-95.5	5.9	15.4	-1.4																

APPENDIX F
Mathematical Model Equations in Harmonic Form

The model and equations for N are of the same form as those for Y, therefore the equations are written here for Y only.

Pure harmonic sway:

Mathematical model:

$$Y = Y_0 + Y_v v + Y_{vvv} v^3 + Y_{\dot{v}} \dot{v} \quad (\text{F-1})$$

(If the model is perfectly symmetrical, Y_0 should be zero)

Motion:

$$\begin{aligned} u &= U_c = \text{constant } u_0 \\ v &= v_a \cos \omega t \\ r &= 0 \end{aligned} \quad (\text{F-2})$$

Forces and moments:

$$Y = \frac{a_{0Y}}{2} + a_{1Y} \cos(\omega t) + a_{3Y} \cos(3\omega t) + b_{1Y} \sin(\omega t) \quad (\text{F-3})$$

(a_{0Y} should be zero for reasons of symmetry, but is kept here to account for imperfections in the symmetry of the model)

Polynomial equations for Y (and N):

$$\begin{aligned} \frac{a_{0Y}}{2} &= Y_0 \\ a_{1Y} &= Y_v v_a + \frac{3}{4} Y_{vvv} v_a^3 \\ a_{3Y} &= \frac{1}{4} Y_{vvv} v_a^3 \\ b_{1Y} &= -Y_{\dot{v}} \omega v_a \end{aligned} \quad (\text{F-4})$$

Pure harmonic yaw:

The equations are the same as for pure sway, replacing all v terms by r.

Mathematical model:

$$Y = Y_0 + Y_r r + Y_{rrr} r^3 + Y_{\dot{r}} \dot{r} \quad (\text{F-5})$$

(If the model is perfectly symmetrical, Y_0 should be zero)

Motion:

$$\begin{aligned} u &= \text{constant } u_0 \\ r &= r_a \cos \omega t \\ v &= 0 \end{aligned} \quad (\text{F-6})$$

Forces and moments:

$$Y = \frac{a_{0Y}}{2} + a_{1Y} \cos(\omega t) + a_{3Y} \cos(3\omega t) + b_{1Y} \sin(\omega t) \quad (\text{F-7})$$

(a_{0Y} should be zero for reasons of symmetry, but is kept here to account for imperfections in the symmetry of the model)

Polynomial equations for Y (and N):

$$\begin{aligned} \frac{a_{0Y}}{2} &= Y_0 \\ a_{1Y} &= Y_r r_a + \frac{3}{4} Y_{rrr} r_a^3 \\ a_{3Y} &= \frac{1}{4} Y_{rrr} r_a^3 \\ b_{1Y} &= -Y_{\dot{r}} \omega r_a \end{aligned} \quad (\text{F-8})$$

APPENDIX G
Non-Dimensional Equations Written in Harmonic Form

Non-dimensional equations written in harmonic form

When working with non-dimensional motions and forces, the kinematic equations incur additional terms in their Fourier series form, due to the fact that the characteristic scale for velocities, $U(t)$, is a function of time.

Equations are written here for the general case encompassing both types of harmonic tests carried out in the JSS test program (pure harmonic sway and yaw motions).

Kinematic equations, dimensional:

$$\begin{aligned}
 u &= u_0 \\
 \dot{u} &= 0 \\
 v &= v_a \cos \omega t \\
 \dot{v} &= -v_a \omega \sin \omega t \\
 r &= r_a \cos \omega t \\
 \dot{r} &= -r_a \omega \sin \omega t
 \end{aligned} \tag{G-1}$$

Kinematic equations, non-dimensional:

$$\begin{aligned}
 U(t) &= \sqrt{u_0^2 + v_a^2} \cos^2 \omega t \\
 \Delta u' &= \frac{(u_0 - U_{ref})}{U(t)} \\
 \dot{u}' &= 0 \\
 v' &= \frac{v_a}{U(t)} \cos \omega t \\
 \dot{v}' &= \frac{-v_a \omega L \sin \omega t}{U^2(t)} \\
 r' &= \frac{r_a L}{U(t)} \cos \omega t \\
 \dot{r}' &= \frac{-r_a \omega L^2 \sin \omega t}{U^2(t)}
 \end{aligned} \tag{G-2}$$

Decomposed in Fourier series up to the third order, the non-dimensional kinematic equations take the form:

$$\begin{aligned}
 v' &= v'_1 \cos \omega t + v'_3 \cos 3\omega t \\
 r' &= r'_1 \cos \omega t + r'_3 \cos 3\omega t \\
 \Delta u' &= u'_0 + u'_2 \cos 2\omega t \\
 \dot{u}' &= 0 \\
 \dot{v}' &= \dot{v}'_1 \sin \omega t + \dot{v}'_3 \sin 3\omega t \\
 \dot{r}' &= \dot{r}'_1 \sin \omega t + \dot{r}'_3 \sin 3\omega t
 \end{aligned} \tag{G-3}$$

$$v'_3 \ll v'_1; \dot{v}'_3 \ll \dot{v}'_1; r'_3 \ll r'_1; \dot{r}'_3 \ll \dot{r}'_1; u'_2 \ll u'_0.$$

In first approximation, only the terms up to first order harmonic are retained:

$$\begin{aligned} v' &\approx v'_1 \cos \omega t \\ r' &\approx r'_1 \cos \omega t \\ \Delta u' &\approx u'_0 \\ \dot{u}' &= 0 \\ \dot{v}' &\approx \dot{v}'_1 \sin \omega t \\ \dot{r}' &\approx \dot{r}'_1 \sin \omega t \end{aligned} \tag{G-4}$$

Non-dimensional amplitudes of the motion:

$$\begin{aligned} v'_1 &= \frac{2}{3} \frac{v_a}{u_0} \left(\frac{1}{\sqrt{4 + (v_a/u_0)^2}} + \frac{1}{\sqrt{1 + (v_a/u_0)^2}} \right) \\ u'_0 &= \frac{1}{2} \left(\frac{u_0 - U_{ref}}{\sqrt{u_0^2 + v_a^2}} + \frac{u_0 - U_{ref}}{u_0} \right) \\ \dot{v}'_1 &= \frac{-2}{3} \frac{v_a \omega L}{u_0^2} \left(1 + \frac{1}{2 \left(1 + \frac{3}{4} \left(\frac{v_a}{u_0} \right)^2 \right)} \right) \\ r'_1 &= \frac{2}{3} \frac{r_a L}{u_0} \left(\frac{1}{\sqrt{4 + (v_a/u_0)^2}} + \frac{1}{\sqrt{1 + (v_a/u_0)^2}} \right) \\ \dot{r}'_1 &= \frac{-2}{3} \frac{r_a \omega L^2}{u_0^2} \left(1 + \frac{1}{2 \left(1 + \frac{3}{4} \left(\frac{v_a}{u_0} \right)^2 \right)} \right) \end{aligned} \tag{G-5}$$

We note that if the amplitude of the sway motion is small, $\frac{v_a}{u_0} \ll 1$, then:

$$\begin{aligned}
 v'_1 &\approx \frac{v_a}{u_0} \\
 u'_0 &\approx \frac{u_0 - U_{ref}}{u_0} \\
 \dot{v}'_1 &\approx \frac{-v_a \omega L}{u_0^2} \\
 r'_1 &\approx \frac{r_a L}{u_0} \\
 \dot{r}'_1 &\approx \frac{-r_a \omega L^2}{u_0^2}
 \end{aligned}
 \tag{G-6}$$

Mathematical model:

The model and equations for N are of the same form as those for Y, and the equations are written here for Y only.

Pure harmonic sway:

$$Y' = Y'_0 + Y'_v v' + Y'_{vvv} v'^3 + Y'_{\dot{v}} \dot{v}' \tag{G-7}$$

Pure harmonic yaw:

$$Y' = Y'_0 + Y'_r r' + Y'_{rrr} r'^3 + Y'_{\dot{r}} \dot{r}' \tag{G-8}$$

with the rudder angle held constant along the centerline or at neutral angle.

Forces and moments are decomposed in Fourier series:

$$Y' = \frac{a_{0Y}}{2} + a_{1Y} \cos(\omega t) + a_{2Y} \cos(2\omega t) + a_{3Y} \cos(3\omega t) + b_{1Y} \sin(\omega t) \tag{G-9}$$

Polynomial equations for Y' (and N'):

Pure harmonic sway:

$$\begin{aligned}
 \frac{a_{0Y}}{2} - a_{2Y} &= Y'_0 \\
 a_{1Y} - 3a_{3Y} &= Y'_v v'_1 \\
 a_{2Y} &= 0 \\
 a_{3Y} &= \frac{1}{4} Y'_{vvv} v'^3_1 \\
 b_{1Y} &= Y'_v \dot{v}'_1
 \end{aligned}
 \tag{G-10}$$

Pure harmonic yaw:

$$\begin{aligned}
 \frac{a_{0Y}}{2} - a_{2Y} &= Y'_0 \\
 a_{1Y} - 3a_{3Y} &= Y'_r r'_1 \\
 a_{2Y} &= 0 \\
 a_{3Y} &= \frac{1}{4} Y'_{rrr} r'^3_1 \\
 b_{1Y} &= Y'_r \dot{r}'_1
 \end{aligned}
 \tag{G-11}$$

APPENDIX H
Harmonic Runs: Data Summary

OCRE-CTR-2012-25

h1pp2 5.8715
 Uref2 1.6969
 Scale2 29.77901
JSS contract design

RUN Name	RUN_008	RUN_009	RUN_010	RUN_011	RUN_012	RUN_013	RUN_014	RUN_001	RUN_002	RUN_003	RUN_004	RUN_005	RUN_006	RUN_007
VORG file	VORG0039	VORG0014	VORG0015	VORG0016	VORG0017	VORG0018	VORG0019	VORG0021	VORG0022	VORG0022	VORG0024	VORG0025	VORG0026	VORG0027
u ₀ [m/s]	1.696	1.693	1.685	1.673	1.659	1.64	1.659	1.697	1.697	1.697	1.697	1.697	1.697	1.697
v ₀ [m/s]	0.085	0.17	0.29	0.4	0.51	0.62	0.51	0	0	0	0	0	0	0
r ₀ [deg/s]	0	0	0	0	0	0	0	1.7	3.3	5	6.7	8.3	10	6.7
T [sec]	16	16	16	16	16	16	20	14	14	14	14	14	14	17
ω _t [-]	1.36	1.36	1.36	1.36	1.36	1.36	1.09	1.55	1.55	1.55	1.55	1.55	1.55	1.28
u' ₀ [-]	-0.001	-0.002	-0.007	-0.014	-0.022	-0.034	-0.022	0	0	0	0	0	0	0
v' ₁ [-]	0.050	0.100	0.170	0.234	0.297	0.360	0.297	0	0	0	0	0	0	0
r' ₁ [-]	0	0	0	0	0	0	0	0.103	0.199	0.302	0.405	0.501	0.604	0.405
v'ddot _t [-]	-0.068	-0.136	-0.234	-0.325	-0.418	-0.514	-0.334	0	0	0	0	0	0	0
r'ddot _t [-]	0	0	0	0	0	0	0	-0.159	-0.309	-0.469	-0.628	-0.778	-0.938	-0.517
a _{0Y} [-]	0.04	0.07	0.09	0.06	0.11	0.15	0.09	0.18	0.10	0.07	0.03	0.02	0.05	0.00
a _{1Y} [-]	-0.49	-1.18	-2.24	-3.54	-5.32	-7.51	-5.33	0.29	0.56	0.78	1.07	1.45	1.89	1.17
a _{2Y} [-]	0.01	0.01	0.03	0.03	0.03	0.02	0.00	0.00	-0.01	0.01	-0.01	0.00	-0.01	-0.03
a _{3Y} [-]	-0.02	-0.05	-0.12	-0.34	-0.56	-0.82	-0.53	0.01	-0.02	-0.05	-0.08	-0.12	-0.20	-0.14
a _{0N} [-]	0.03	0.02	0.04	0.04	0.06	0.05	0.04	0.11	0.08	0.07	0.04	0.06	0.06	0.04
a _{1N} [-]	-0.24	-0.51	-0.94	-1.27	-1.65	-2.06	-1.63	-0.21	-0.42	-0.71	-0.98	-1.30	-1.71	-0.99
a _{2N} [-]	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.00	0.00	0.01	0.02	0.01	0.02	0.01
a _{3N} [-]	0.00	-0.01	-0.05	-0.03	-0.07	-0.14	-0.03	0.00	-0.01	-0.03	-0.07	-0.12	-0.17	-0.07
b _{1Y} [-]	0.66	1.29	2.27	3.33	4.49	5.65	0.04	0.06	0.13	0.24	0.29	0.44	0.60	0.30
b _{1N} [-]	0.01	0.00	-0.02	-0.01	0.00	-0.02	0.00	0.08	0.17	0.27	0.34	0.46	0.57	0.31
a _{1Y-3a_{3Y}} [-]	-0.44	-1.04	-1.88	-2.51	-3.65	-5.06	-3.75	0.27	0.60	0.92	1.31	1.80	2.49	1.58
a _{1N-3a_{3N}} [-]	-0.24	-0.49	-0.80	-1.18	-1.44	-1.64	-1.55	-0.22	-0.40	-0.62	-0.77	-0.96	-1.19	-0.78
Single run analysis														
Y _v *1000	-8.9	-10.4	-11.0	-10.7	-12.3	-14.1	-12.6	2.6	3.0	3.0	3.2	3.6	4.1	3.9
Y _v dot *1000	-9.7	-9.5	-9.7	-10.2	-10.7	-11.0	-0.1	-2.1	-2.0	-2.0	-1.9	-2.0	-2.0	-1.9
Y _r *1000								-0.5	-0.5	-0.6	-0.5	-0.6	-0.6	-0.6
N _v *1000	-4.8	-4.9	-4.7	-5.1	-4.9	-4.6	-5.2	-0.5	-0.5	-0.6	-0.5	-0.6	-0.6	-0.6
N _r *1000								-0.5	-0.5	-0.6	-0.5	-0.6	-0.6	-0.6
N _r dot *1000														

OCRE-CTR-2012-25

hipp2 5.8715
 Uref2 1.6969
 Scale2 29.77901
JSS contract design repeat

RUN Name VORG file	RUN_110 VORG0039	RUN_111 VORG0014	RUN_112 VORG0015	RUN_113 VORG0016	RUN_114 VORG0017	RUN_115 VORG0018	RUN_104 VORG0021	RUN_105 VORG0022	RUN_106 VORG0023	RUN_107 VORG0024	RUN_108 VORG0025	RUN_109 VORG0026
u ₀ [m/s]	1.696	1.693	1.685	1.673	1.659	1.64	1.697	1.697	1.697	1.697	1.697	1.697
V _a [m/s]	0.085	0.17	0.29	0.4	0.51	0.62	0	0	0	0	0	0
m [deg/s]	0	0	0	0	0	0	1.7	3.3	5	6.7	8.3	10
T [sec]	16	16	16	16	16	16	14	14	14	14	14	14
ω ₁ [°]	1.36	1.36	1.36	1.36	1.36	1.36	1.55	1.55	1.55	1.55	1.55	1.55
u' ₀ [°]	-0.001	-0.002	-0.007	-0.014	-0.022	-0.034	0	0	0	0	0	0
V ₁ [°]	0.050	0.100	0.170	0.234	0.297	0.360	0	0	0	0	0	0
r ₁ [°]	0	0	0	0	0	0	0.103	0.199	0.302	0.405	0.501	0.604
v'dot ₁ [°]	-0.068	-0.136	-0.234	-0.325	-0.418	-0.514	0	0	0	0	0	0
r'dot ₁ [°]	0	0	0	0	0	0	-0.159	-0.309	-0.469	-0.628	-0.778	-0.938
a _{0Y} [°]	0.01	0.01	-0.01	0.08	0.13	0.09	0.06	0.03	0.04	0.06	0.09	0.13
a _{1Y} [°]	-0.53	-1.18	-2.30	-3.63	-5.46	-7.76	0.29	0.56	0.84	1.14	1.52	1.94
a _{2Y} [°]	0.01	-0.01	0.01	0.03	0.03	0.03	0.00	-0.02	-0.01	-0.03	-0.02	-0.01
a _{3Y} [°]	-0.02	-0.05	-0.11	-0.33	-0.59	-0.84	0.01	-0.02	-0.04	-0.10	-0.13	-0.21
a _{0N} [°]	0.05	0.04	0.05	0.07	0.09	0.07	-0.05	0.00	-0.01	0.00	0.02	0.04
a _{1N} [°]	-0.24	-0.49	-0.92	-1.25	-1.63	-2.06	-0.22	-0.43	-0.69	-0.97	-1.29	-1.68
a _{2N} [°]	0.00	0.00	0.00	0.01	0.01	0.02	0.00	0.00	0.01	0.01	0.01	0.01
a _{3N} [°]	0.00	-0.01	-0.04	-0.02	-0.07	-0.13	0.00	-0.01	-0.03	-0.07	-0.12	-0.17
b _{1Y} [°]	0.62	1.27	2.22	3.25	4.31	5.50	0.06	0.14	0.24	0.33	0.41	0.63
b _{1N} [°]	-0.01	-0.01	-0.04	-0.04	-0.05	-0.06	0.09	0.17	0.27	0.36	0.44	0.59
a _{1Y} -3a _{3Y} [°]	-0.48	-1.03	-1.98	-2.63	-3.70	-5.24	0.26	0.61	0.97	1.43	1.90	2.56
a _{1N} -3a _{3N} [°]	-0.24	-0.47	-0.80	-1.19	-1.43	-1.66	-0.22	-0.40	-0.60	-0.76	-0.94	-1.16
Single run analysis												
YV *1000	-9.6	-10.3	-11.6	-11.2	-12.4	-14.6	2.6	3.1	3.2	3.5	3.8	4.2
Yvdot *1000	-9.0	-9.3	-9.5	-10.0	-10.3	-10.7	-2.1	-2.0	-2.0	-1.9	-1.9	-1.9
Yr *1000	-4.8	-4.7	-4.7	-5.1	-4.8	-4.6	-0.5	-0.6	-0.6	-0.6	-0.6	-0.6
NV *1000												
Nr *1000												
Nr'dot *1000												

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hipp2 5.8715
 Uref2 1.6969
 Scale2 29.77901
JSS contract design Rudder 3

RUN Name VORG file	RUN_159 VORG0039	RUN_160 VORG0014	RUN_161 VORG0015	RUN_162 VORG0016	RUN_163 VORG0017	RUN_164 VORG0018	RUN_153 VORG0021	RUN_154 VORG0022	RUN_155 VORG0023	RUN_156 VORG0024	RUN_157 VORG0025	RUN_158 VORG0026
u ₀ [m/s]	1.696	1.693	1.685	1.673	1.659	1.64	1.697	1.697	1.697	1.697	1.697	1.697
v _a [m/s]	0.085	0.17	0.29	0.4	0.51	0.62	0	0	0	0	0	0
α [deg/s]	0	0	0	0	0	0	1.7	3.3	5	6.7	8.3	10
T [sec]	16	16	16	16	16	16	14	14	14	14	14	14
ω ₁ [°]	1.36	1.36	1.36	1.36	1.36	1.36	1.55	1.55	1.55	1.55	1.55	1.55
u' ₀ [°]	-0.001	-0.002	-0.007	-0.014	-0.022	-0.034	0	0	0	0	0	0
v' ₁ [°]	0.050	0.100	0.170	0.234	0.297	0.360	0	0	0	0	0	0
r' ₁ [°]	0	0	0	0	0	0	0.103	0.199	0.302	0.405	0.501	0.604
v'dot ₁ [°]	-0.068	-0.136	-0.234	-0.325	-0.418	-0.514	0	0	0	0	0	0
r'dot ₁ [°]	0	0	0	0	0	0	-0.159	-0.309	-0.469	-0.628	-0.778	-0.938
a _{0Y} [°]	0.05	0.02	-0.09	-0.06	-0.03	0.07	-0.20	-0.05	0.12	0.11	0.15	0.19
a _{1Y} [°]	-0.51	-1.21	-2.31	-3.58	-5.36	-7.57	0.32	0.59	0.86	1.16	1.51	1.98
a _{2Y} [°]	0.00	0.01	0.01	-0.02	-0.02	0.02	0.00	-0.01	0.02	0.01	0.04	0.04
a _{3Y} [°]	-0.02	-0.06	-0.12	-0.33	-0.56	-0.81	0.01	-0.01	-0.05	-0.09	-0.14	-0.21
a _{0N} [°]	0.09	0.04	0.01	0.01	0.03	0.03	-0.01	0.05	0.13	0.11	0.12	0.13
a _{1N} [°]	-0.23	-0.49	-0.91	-1.23	-1.58	-1.99	-0.23	-0.45	-0.72	-1.00	-1.32	-1.73
a _{2N} [°]	0.00	0.00	-0.01	0.00	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01
a _{3N} [°]	0.00	-0.01	-0.04	-0.02	-0.07	-0.14	0.00	-0.01	-0.03	-0.06	-0.11	-0.17
b _{1Y} [°]	0.62	1.26	2.24	3.26	4.37	5.61	0.07	0.13	0.19	0.30	0.45	0.55
b _{1N} [°]	0.00	0.00	0.00	0.00	0.00	-0.01	0.00	0.00	-0.01	-0.01	-0.01	-0.01
a _{1Y} -3a _{3Y} [°]	-0.46	-1.03	-1.96	-2.61	-3.69	-5.15	0.28	0.62	1.01	1.44	1.94	2.61
a _{1N} -3a _{3N} [°]	-0.23	-0.47	-0.79	-1.17	-1.38	-1.57	-0.23	-0.43	-0.63	-0.81	-0.99	-1.23
Single run analysis												
Yv *1000	-9.2	-10.3	-11.5	-11.1	-12.4	-14.3	2.7	3.1	3.3	3.6	3.9	4.3
Yvdot *1000	-9.1	-9.2	-9.6	-10.0	-10.5	-10.9	-2.2	-2.1	-2.1	-2.0	-2.0	-2.0
Yr *1000	-4.5	-4.7	-4.6	-5.0	-4.6	-4.4	0.0	0.0	0.0	0.0	0.0	0.0
Nv *1000												
Nr *1000												
Nr'dot *1000												

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hipp2 5.8715
 Uref2 1.6969
 Scale2 29.77901
JSS contract design Rudder 2

RUN Name VORG file	RUN_135 VORG0039	RUN_136 VORG0014	RUN_137 VORG0015	RUN_138 VORG0016	RUN_139 VORG0017	RUN_140 VORG0018	RUN_129 VORG0021	RUN_130 VORG0022	RUN_131 VORG0023	RUN_132 VORG0024	RUN_133 VORG0025	RUN_134 VORG0026
u ₀ [m/s]	1.696	1.693	1.685	1.673	1.659	1.64	1.697	1.697	1.697	1.697	1.697	1.697
v _a [m/s]	0.085	0.17	0.29	0.4	0.51	0.62	0	0	0	0	0	0
m [deg/s]	0	0	0	0	0	0	1.7	3.3	5	6.7	8.3	10
T [sec]	16	16	16	16	16	16	14	14	14	14	14	14
ω ₁ [°]	1.36	1.36	1.36	1.36	1.36	1.36	1.55	1.55	1.55	1.55	1.55	1.55
u' ₀ [°]	-0.001	-0.002	-0.007	-0.014	-0.022	-0.034	0	0	0	0	0	0
v' ₁ [°]	0.050	0.100	0.170	0.234	0.297	0.360	0	0	0	0	0	0
r' ₁ [°]	0	0	0	0	0	0	0.103	0.199	0.302	0.405	0.501	0.604
v'dot ₁ [°]	-0.068	-0.136	-0.234	-0.325	-0.418	-0.514	0	0	0	0	0	0
r'dot ₁ [°]	0	0	0	0	0	0	-0.159	-0.309	-0.469	-0.628	-0.778	-0.938
a _{0Y} [°]	0.13	0.29	0.33	0.32	0.17	0.14	0.15	0.04	0.11	-0.01	0.03	0.12
a _{1Y} [°]	-0.55	-1.23	-2.30	-3.70	-5.46	-7.64	0.31	0.63	0.92	1.23	1.58	2.05
a _{2Y} [°]	0.01	0.01	0.02	0.04	0.01	0.00	0.00	0.00	-0.03	-0.04	-0.04	-0.01
a _{3Y} [°]	-0.03	-0.05	-0.11	-0.32	-0.55	-0.80	0.01	-0.02	-0.04	-0.08	-0.13	-0.20
a _{0N} [°]	-0.01	0.02	0.00	-0.01	-0.02	-0.07	-0.02	-0.02	-0.09	-0.09	-0.07	-0.02
a _{1N} [°]	-0.25	-0.50	-0.90	-1.22	-1.56	-1.96	-0.24	-0.46	-0.73	-1.04	-1.38	-1.79
a _{2N} [°]	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.01	0.01	0.02	0.01	0.01
a _{3N} [°]	0.00	-0.01	-0.04	-0.02	-0.06	-0.14	0.00	-0.01	-0.03	-0.06	-0.11	-0.18
b _{1Y} [°]	0.66	1.32	2.29	3.29	4.37	5.65	0.05	0.09	0.16	0.28	0.41	0.53
b _{1N} [°]	0.00	-0.01	-0.01	-0.01	-0.01	0.00	0.00	0.00	0.00	0.00	0.00	-0.01
a _{1Y} -3a _{3Y} [°]	-0.47	-1.08	-1.96	-2.72	-3.80	-5.23	0.27	0.68	1.05	1.47	1.98	2.64
a _{1N} -3a _{3N} [°]	-0.25	-0.47	-0.77	-1.15	-1.37	-1.55	-0.24	-0.44	-0.65	-0.84	-1.04	-1.27
Single run analysis												
Yv *1000	-9.3	-10.8	-11.5	-11.6	-12.8	-14.6	2.7	3.4	3.5	3.6	4.0	4.4
Yvdot *1000	-9.7	-9.6	-9.8	-10.1	-10.5	-11.0	-2.3	-2.2	-2.1	-2.1	-2.1	-2.1
Yr *1000	-4.9	-4.7	-4.5	-4.9	-4.6	-4.3	0.0	0.0	0.0	0.0	0.0	0.0
Nv *1000												
Nr *1000												
Nr'dot *1000												

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h1pp1 5.8271
 Uref1 1.6995
 Scale1 29.6891
JSS preliminary design (January 2012 test session)

RUN Name VORG file	RUN_037 VORG0039	RUN_038 VORG0014	RUN_039 VORG0015	RUN_040 VORG0016	RUN_041 VORG0017	RUN_042 VORG0018	RUN_031 VORG0021	RUN_032 VORG0022	RUN_033 VORG0023	RUN_034 VORG0024	RUN_035 VORG0025	RUN_036 VORG0026
u ₀ [m/s]	1.698	1.695	1.687	1.675	1.66	1.641	1.6995	1.6995	1.6995	1.6995	1.6995	1.6995
V _a [m/s]	0.085	0.17	0.29	0.41	0.52	0.63	0	0	0	0	0	0
r _a [deg/s]	0	0	0	0	0	0	1.7	3.3	5	6.7	8.4	10
T [sec]	15	15	15	15	15	15	14	14	14	14	14	14
ω' ₁ [°]	1.44	1.44	1.44	1.44	1.44	1.44	1.54	1.54	1.54	1.54	1.54	1.54
U' ₀ [°]	-0.001	-0.003	-0.007	-0.014	-0.023	-0.034	0	0	0	0	0	0
V' ₁ [°]	0.050	0.100	0.170	0.239	0.302	0.365	0	0	0	0	0	0
r' ₁ [°]	0	0	0	0	0	0	0.102	0.197	0.299	0.401	0.503	0.598
V'dot _t [°]	-0.072	-0.144	-0.247	-0.352	-0.450	-0.552	0	0	0	0	0	0
r'dot _t [°]	0	0	0	0	0	0	-0.157	-0.304	-0.460	-0.617	-0.774	-0.921
a _{1Y} [°]	0.08	0.15	0.16	0.21	0.25	0.29	0.08	0.08	0.12	0.13	0.15	0.14
a _{1Y} [°]	-0.48	-1.11	-2.22	-3.48	-5.14	-7.10	0.25	0.49	0.78	1.14	1.56	2.01
a _{2Y} [°]	0.01	0.00	0.01	0.03	0.05	0.06	0.00	0.00	-0.01	-0.01	0.00	0.00
a _{3Y} [°]	-0.02	-0.06	-0.13	-0.33	-0.59	-0.79	0.01	0.01	-0.02	-0.04	-0.07	-0.15
a _{4N} [°]	-0.03	0.04	-0.01	-0.01	0.00	0.00	0.00	0.00	0.04	0.02	0.00	0.02
a _{1N} [°]	-0.26	-0.49	-0.82	-1.14	-1.45	-1.78	-0.20	-0.41	-0.66	-0.92	-1.23	-1.55
a _{2N} [°]	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.01	0.01	0.00	0.00
a _{3N} [°]	0.00	0.00	-0.01	0.00	-0.03	-0.08	0.00	0.00	-0.03	-0.06	-0.09	-0.14
b _{1Y} [°]	0.62	1.26	2.21	3.39	4.53	5.80	0.06	0.13	0.19	0.31	0.42	0.58
b _{1N} [°]	-0.01	0.00	-0.02	-0.01	-0.03	-0.03	0.09	0.17	0.22	0.33	0.42	0.52
a _{1Y-3a3Y} [°]	-0.43	-0.94	-1.82	-2.50	-3.38	-4.75	0.22	0.47	0.85	1.26	1.79	2.47
a _{1N-3a3N} [°]	-0.27	-0.49	-0.79	-1.13	-1.36	-1.55	-0.20	-0.39	-0.57	-0.75	-0.95	-1.12
Single run analysis												
Y _v *1000	-8.7	-9.4	-10.7	-10.5	-11.2	-13.0	2.2	2.4	2.8	3.1	3.6	4.1
Y _v dot *1000	-8.6	-8.8	-8.9	-9.7	-10.1	-10.5	-2.0	-2.0	-1.9	-1.9	-1.9	-1.9
Y _r *1000	-5.4	-4.9	-4.6	-4.7	-4.5	-4.2	-0.6	-0.6	-0.5	-0.5	-0.5	-0.6
N _r *1000												
N _r dot *1000												

APPENDIX I
“Single-Run” Method of Harmonic Analysis

“Single-run” harmonic analysis suffers the same limitations as “multiple-run” harmonic analysis, and more: like “multiple-run” harmonic analysis it assumes pure harmonic nature of the motions; and runs of different motion amplitude yield slightly different hydrodynamic coefficients. This method was used to assess the January 2012 phase of testing, on the JSS Preliminary Design, before the analysis method was refined. It is presented here as it permits relative comparison of the stability of all vessel configurations: those tested with the JSS Preliminary Design in January 2012 together with those tested with the JSS Contract Design in this phase.

Method:

In Section 5.5, under the assumption that the motions were purely harmonic, the following equations were developed linking the Fourier coefficients of forces and moments to the hydrodynamic coefficients.

For pure harmonic sway tests:

$$\begin{aligned} \frac{a_{0Y}}{2} - a_{2Y} &= Y'_0 \\ a_{1Y} - 3a_{3Y} &= Y'_v v'_1 \\ a_{3Y} &= \frac{1}{4} Y'_{vvv} v_1^3 \\ b_{1Y} &= Y'_{\dot{v}} \dot{v}'_1 \end{aligned}$$

And for pure harmonic yaw tests:

$$\begin{aligned} \frac{a_{0Y}}{2} - a_{2Y} &= Y'_0 \\ a_{1Y} - 3a_{3Y} &= Y'_r r'_1 \\ a_{3Y} &= \frac{1}{4} Y'_{rrr} r_1^3 \\ b_{1Y} &= Y'_{\dot{r}} \dot{r}'_1 \end{aligned}$$

(and equivalent sets of equations for non-dimensional yaw moment N’).

Using the second (a₁-3a₃) and fourth (b₁) equations in the first equation set, coefficients in *v* and in *v*’ can be obtained from any single pure harmonic sway run. Using the second (a₁-3a₃) and fourth (b₁) equations in the second equation set, coefficients in *r* and in *r*’ can be obtained from any single pure harmonic yaw run.

The analysis software “pmmana” is designed to perform the “single-run” method of analysis, where hydrodynamic coefficients in *v* are assessed on the basis of one single pure sway harmonic run, and hydrodynamic coefficients in *r* are assessed on the basis of one single pure yaw harmonic run. After analysis of a pure motion run the software computes the hydrodynamic coefficients from the harmonic coefficients and outputs a table of hydrodynamic coefficients, where the newly calculated coefficients have been updated.

The hydrodynamic coefficients calculated using the “single run” analysis, vary somewhat with the amplitude of motion of the harmonic run being analyzed. The “single run” analysis is akin to determining the slope of a linear fit based on a single data point. Results from small amplitude runs could be carrying a large measurement uncertainty and be less significant, while at the largest amplitudes the mathematical model might be less valid as the physics could call for higher order terms.

Results:

Appendix H: Harmonic Runs – Data Summary shows the data and Fourier coefficients from all harmonic runs, as well as coefficients extracted for each run using the “single-run” harmonic method.

The following Figures I-1 and I-2 show that the hydrodynamic coefficients extracted with the “single-run” analysis method vary with the amplitude of the motion for that run. Yet, trends are clearly noticeable between different vessel configurations (different rudders, or compared to the JSS preliminary design).

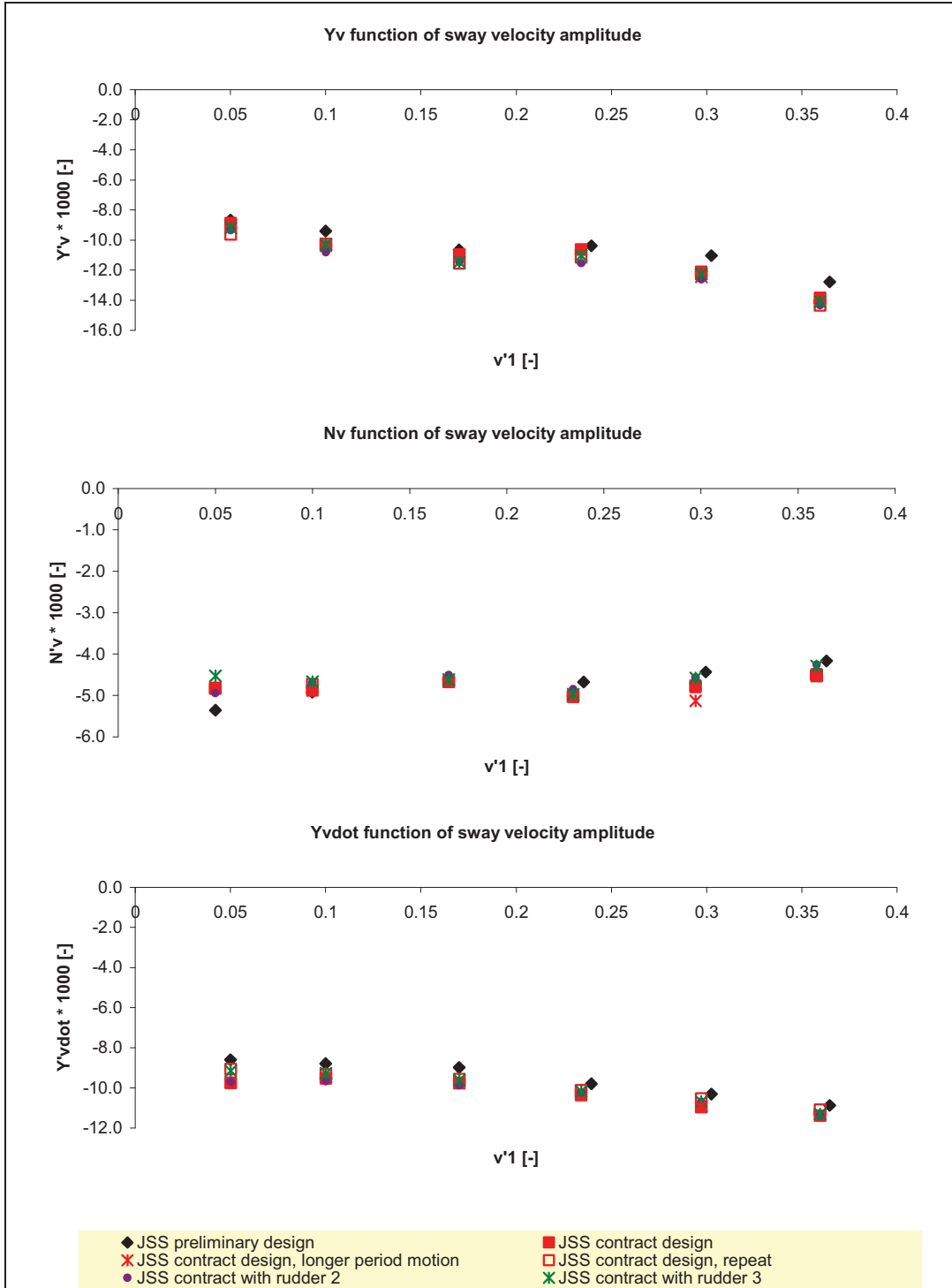


Figure I-1. Single Run Analysis: Variation with Sway Amplitude of Hydrodynamic Coefficients in v

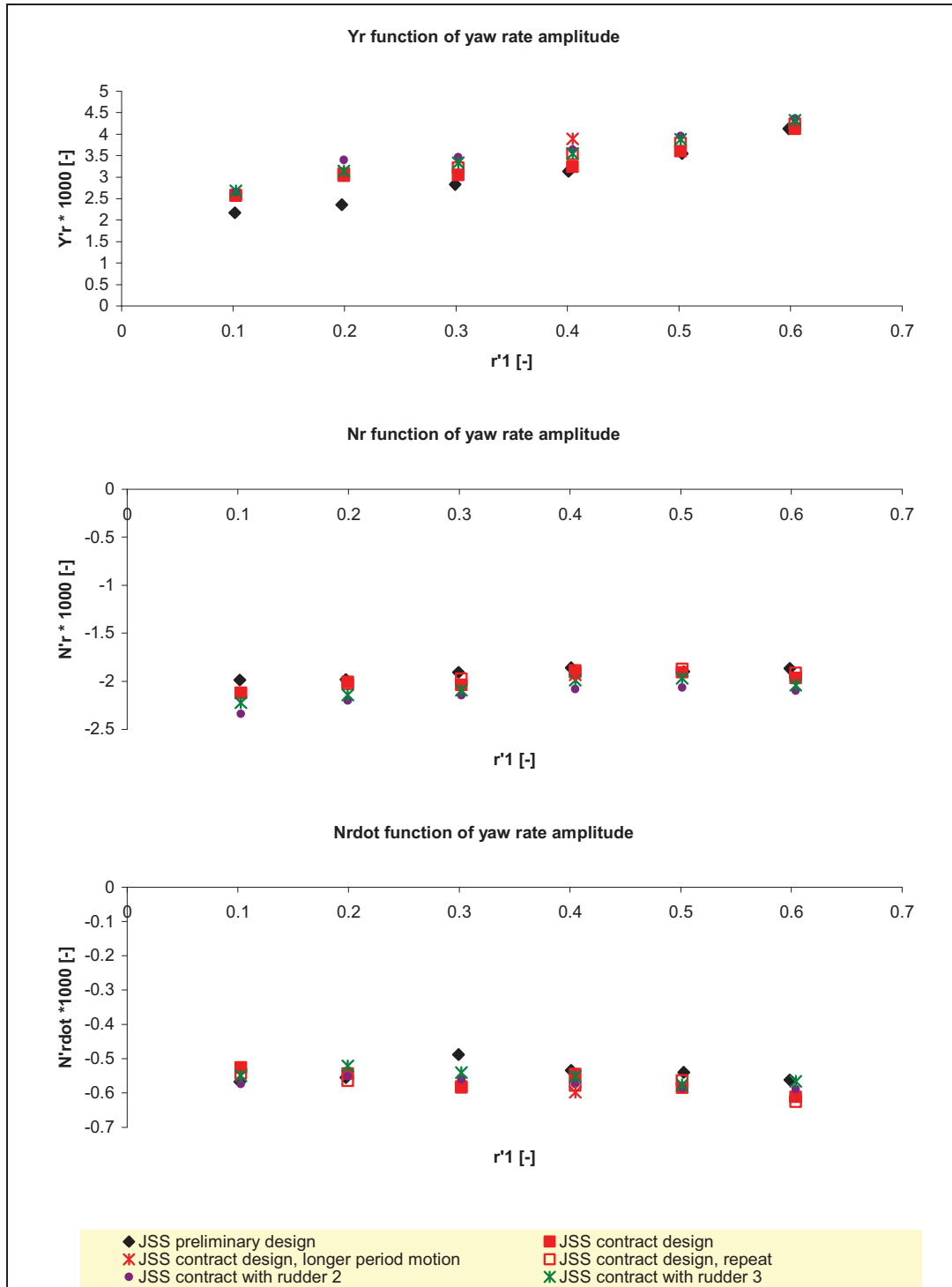


Figure I-2. Single Run Analysis: Variation with Yaw Amplitude of Hydrodynamic Coefficients in r

The hydrodynamic coefficients from the “single-run” analysis, and the resulting stability indices and criteria for all vessel configurations, are presented in Table I-1 below: for each vessel configuration, an average hydrodynamic coefficient was calculated from a selection of runs. The runs retained for calculation of each hydrodynamic coefficient, indicated to the right of the table, were chosen during the January 2012 test session, based on information available then (the choice was guided by the results of static drift tests in that session and by the observations during the pond trials done with the JSS preliminary design). Importantly, for comparing vessel configurations in a consistent manner, the same selection of runs is retained here for analysis of the contract design from the present session measurements. The corresponding results from the January session on the preliminary design (Reference [17]) are reproduced below in Table I-2 for reference.

Configuration	JSS contract design	JSS contract design, repeat	JSS contract design, with Rudder 3	JSS contract design, with Rudder 2	(Runs used)
Rudder	design rudder	design rudder	Rudder 3	Rudder 2	(runs are numbered in ascending order of amplitude) (5,6) (4,5,6) (4,5) (3,4) (3,4) (3,4)
Skeg	none	none	none	none	
shaft speed	ship self-propulsion	ship self-propulsion	ship self-propulsion	ship self-propulsion	
Y'v *1000	-12.99	-13.32	-13.18	-13.48	
N'r *1000	-1.93	-1.89	-2.00	-2.08	
Y'r *1000	3.42	3.67	3.72	3.80	
N'v *1000	-4.85	-4.86	-4.79	-4.68	
Y'vdot *1000	-10.07	-9.85	-9.89	-10.06	
N'rdot *1000	-0.56	-0.58	-0.55	-0.57	
A' *10^6	19.75	19.80	19.22	19.78	
B' *10^6	50.15	49.59	51.13	53.60	
C' *10^6	-1.8	-0.5	1.3	3.9	
sigma1	0.03	0.01	-0.02	-0.08	

A' is $(I'z - N'rdot) * (m' - Y'vdot)$
 B' is $-(I'z - N'rdot) * Y'v - (m' - Y'vdot) * N'r$
 C' is $Y'v * N'r - N'v * (Y'r - m')$

Non-dimensionalization uses the following quantities:
 distance: Lpp
 speed: instantaneous speed along track

Table I-1. Stability of JSS Contract Design, using “Single-run” analysis (and January 2011 selection of runs)

Configuration	Preliminary design	Preliminary design, with Rudder 3	Preliminary design, with Rudder 2	Preliminary design, with skeg	Preliminary design, with skeg	Preliminary design, with skeg	Preliminary design, model as tested on the pond	(Runs used) (runs are numbered in ascending order of amplitude)
Rudder	design rudder	Rudder 3	Rudder 2	design rudder	design rudder	design rudder	design rudder	
Skeg	none	none	none	0 deg	2 deg	4 deg	none	
shaft speed	ship self-propulsion	ship self-propulsion	ship self-propulsion	ship self-propulsion	ship self-propulsion	ship self-propulsion	model self-propulsion	
$Y_v * 1000$	-11.92	-11.93	-12.43	-12.82	-12.96	-13.06	-12.02	(5,6)
$N_r * 1000$	-1.88	-2.00	-2.13	-2.18	-2.20	-2.28	-1.96	(4,5,6)
$Y_r * 1000$	3.34	4.16	4.43	3.97	4.03	4.21	3.44	(4,5)
$N_v * 1000$	-4.65	-4.57	-4.48	-4.26	-4.24	-4.14	-4.53	(3,4)
$Y\dot{v}dot * 1000$	-9.40	-9.60	-9.72	-10.30	-10.35	-10.26	-9.61	(3,4)
$N\dot{r}dot * 1000$	-0.51	-0.56	-0.58	-0.58	-0.58	-0.59	-0.54	(3,4)
$A' * 10^6$	18.23	19.42	19.75	20.51	20.60	20.60	18.98	
$B' * 10^6$	46.24	49.55	52.83	55.61	56.22	57.77	48.61	
$C' * 10^6$	-3.7	2.0	6.3	6.7	7.5	10.2	-1.4	
sigma1	0.08	-0.04	-0.12	-0.13	-0.14	-0.19	0.03	

Information from analysis of earlier tests

A' is $(I_z - N_r \dot{r}dot)^2 (m' - Y_v \dot{v}dot)$
 B' is $-(I_z - N_r \dot{r}dot) Y_v \dot{v} - (m' - Y_v \dot{v}dot) N_r$
 C' is $Y_v N_r - N_v (Y_T - m')$

Non-dimensionalization uses the following quantities:

distance: L_{pp}
 speed: instantaneous speed along track

Table I-2. Stability of JSS Preliminary Design (January 2011 tests), using "Single-run" analysis

In the above results, the determination of Y_v coefficients appears too high, when compared with the drift test measurements from this session (see Table 10 of the report). In the following table, the stability criteria was recalculated using for all hydrodynamic coefficient an average of the results of the four lowest amplitude motion runs. The design configurations rank the same way, albeit now all configurations show as unstable.

Configuration	JSS2 Ship	JSS2_2	JSS2_R3	JSS2_R2	Ship (Baseline)	(Runs used)
Rudder	design rudder	design rudder	Rudder 3	Rudder 2	design rudder	(runs are numbered in ascending order of amplitude)
Skeg	none	none	none	none	none	(1-4)
shaft speed	ship self-propulsion	ship self-propulsion	ship self-propulsion	ship self-propulsion	ship self-propulsion	(1-4)
$Y_v * 1000$	-10.23	-10.66	-10.50	-10.80	-9.78	(1-4)
$N_r * 1000$	-2.02	-2.00	-2.11	-2.19	-1.93	(1-4)
$Y_r * 1000$	2.98	3.10	3.18	3.29	2.62	(1-4)
$N_v * 1000$	-4.85	-4.82	-4.69	-4.75	-4.89	(1-4)
$Y_{vdot} * 1000$	-9.86	-9.53	-9.56	-9.88	-9.05	(1-4)
$N_{rdot} * 1000$	-0.55	-0.57	-0.54	-0.56	-0.54	(1-4)
$A' * 10^6 =$	19.25	19.23	18.78	19.55	18.33	
$B' * 10^6 =$	48.46	48.10	49.77	52.49	44.76	
$C' * 10^6 =$	-8.3	-6.9	-4.9	-3.2	-12.0	
$\sigma_{mat} =$	0.16	0.14	0.10	0.06	0.24	

$$A' \text{ is } (I'z - N'rdot) * (m' - Y'vdot)$$

$$B' \text{ is } -(I'z - N'rdot) * Y'v - (m' - Y'vdot) * N'r$$

$$C' \text{ is } Y'v * N'r - N'v * (Y'r - m')$$

Non-dimensionalization uses the following quantities:
 distance: Lpp
 speed: instantaneous speed along track

Table I-3. Stability of JSS Contract Design (and Preliminary Design), using “Single-run” analysis and harmonic runs 1 to 4.

As can be expected, these results are close to those obtained with the “Multiple-Run” harmonic analysis using the four lower amplitude motion runs (Table 11 of the report, bottom part).

APPENDIX J
Comparison of Repeat Runs

Uref=	1.6969 m/s			
	RUN_011 VORG0016	RUN_096 VORG0016	RUN_096 VORG0024	RUN_095 VORG0024
u ₀	1.673	1.673	1.697	1.697
v _a	0.4	0.4	0	0
r _a	0	0	6.7	6.7
T	16	16	14	14
u'0	-0.014	-0.014	0	0
v'0	0	0	0	0
v'1	0.234	0.234	0	0
r'1	0	0	0.405	0.405
v'dot1	-0.325	-0.325	0	0
r'dot1	0	0	-0.628	-0.628
a0Y	0.06	-0.02	0.053	0.013
a1Y	-3.54	-3.51	0.020	1.12
a2Y	0.03	-0.01	0.026	-0.02
a3Y	-0.34	-0.33	0.012	-0.07
a0N	0.04	-0.01	0.034	0.03
a1N	-1.27	-1.25	0.012	-0.97
a2N	0.01	0.00	0.006	0.01
a3N	-0.03	-0.02	0.006	-0.06
b1Y	3.33	3.33	0.007	0.34
b1N	-0.01	-0.01	0.001	0.37
a1Y-3a3Y	-2.51	-2.54	0.018	1.31
a1N-3a3N	-1.18	-1.19	0.005	-0.77
Single run analysis				
Y'v	*1000	-10.7	-10.8	0.08
Y'vdot	*1000	-10.2	-10.3	0.02
Y'r	*1000			3.2
N'v	*1000	-5.1	-5.1	0.02
N'r	*1000			-1.9
N'rdot	*1000			0.0

Table J2 Comparison of Repeat Harmonic Runs