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**COMPUTER
PROGRAMS FOR
INFRARED
SPECTROPHOTOMETRY**

ANALYZED

**PROGRAMMES
D'ORDINATEURS
POUR LA
SPECTROPHOTOMÉTRIE
INFRAROUGE**

X-XV

R.N. Jones
J. Pitha

N.R.C.C. Bulletin No. 12 (1968) Bulletin du C.N.R.C.

Second Edition 1976 Deuxième édition

COMPUTER PROGRAMS FOR
INFRARED SPECTROPHOTOMETRY*

VOLUME II

ANALYZED

J. Pitha⁺ and R.N. Jones

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INTRODUCTION TO THE SECOND EDITION

The six programs in this volume were first published in 1968. Their republication here is part of our project to augment and update our total collection of computer programs for infrared spectrophotometry as described in the introduction to the Second Edition of Bulletin 11 which forms Volume I of this series of seven volumes issued as N.R.C.C. Bulletins 11-17.

These programs have been applied by a variety of users to the fitting of band envelopes based on Cauchy and Gauss functions and their sum or product combinations. Though most of the applications have been in the spectroscopic field they have also found application in other areas of science. The versions presented here do not differ significantly from those published previously. In our N.R.C.C. Bulletin 13 we supply three additional variants of the basic program. Two of these versions deal with the system in which all five parameters are free to adjust independently (the "unrestricted Cauchy-Gauss sum function"); another version in Bulletin 13 is arranged for the simplified algorithm for a set of pure Cauchy curves with only three adjustable parameters. This may have advantages where the computer storage facilities and the run time are critical. For most users the basic version given in Program X in this volume is recommended. The subsequent paragraphs of this introduction are reproduced unchanged from the First Edition.

This Bulletin supplements earlier publications from this laboratory dealing with methods of fitting analytical functions to infrared absorption bands of condensed phase systems (1-3). Seven methods of optimization with non-linear least squares approximations were examined, and two have been found to be significantly more effective than the other five (2). These preferred methods were developed by Meiron (4), and by Marquardt (5) for other purposes; they are basically similar and both are modifications of an earlier method of Levenberg (6) which Papoušek and Plivá have also used for fitting infrared band envelopes (7). The programs described in this Bulletin use Method V of our earlier publication; they combine features of both the Meiron and the Marquardt algorithms and use an automated search routine to determine the optimal value of the damping constant.

Three versions of Method V will be presented. All utilize the Cauchy-Gauss product function, while two also permit the alternative use of the Cauchy-Gauss sum function; a floating horizontal baseline is employed. Pure Cauchy or pure Gauss functions can also be fitted by all three programs, but, from the computational point of view, this is not an efficient way of operating with these simpler functions. The development of these programs was initiated on a small S.D.S. Model 920 computer and

several memory conserving procedures were introduced. These have been retained, though the larger storage capacity of the I.B.M. 360(67) computer we are now using diminishes their importance, and their replacement could increase the speed of computation on large computers. In other respects also these programs reflect their piecemeal evolution, and no claim is made for high computational efficiency. The input and output formats interface with the set of modular programs that have been developed in our laboratory to perform the common numerical transformations of absorption spectrophotometry (8).

A. The Basic Version (Program X)

As written, this program will handle a maximum of twenty component bands simultaneously optimizing up to 81 band indices.* It can be expanded by changing the dimensional statement, but the execution time increases rapidly with the number of bands, as also does the demand on the storage capacity.

B. The Moving Subspace Version (Program XI)

This is Method VIII of reference (2). The initial guessed indices are introduced at the beginning of the computation, but the indices of only a limited number of consecutive bands are adjusted at one time. In principle this "moving subspace" program can cope with envelopes containing a very large number of constituent bands. As written the moving subspace can deal with from two to five consecutive bands and twenty bands in all. The total number of bands can be increased by altering the dimension statement with no change in the body of the program. This program operates on the Cauchy-Gauss product function only; a version operating on the unrestrained Cauchy-Gauss sum function is provided by Program XVIII in Bulletin 13.

C. Version with Correction for Spectral Slit Distortion (Program XII)

This version resembles Program X in that it operates on all indices simultaneously and will handle both the product and sum

* We use the term "band indices" to designate the values of the variables defining the composite band envelope. All three programs described in this Bulletin require $4M+1$ indices to define an envelope derived from M overlapping bands.

functions. The slit function ordinates are introduced (or computed) and the curve generated from the calculated indices is convoluted with the spectral slit function before optimization with the experimental data. In this way a band envelope is generated that conforms with the contour of the "true" spectrum adjusted for the finite spectral slit distortion (9,10).

D. Other Programs

(i) Program XIII. This program evaluates the areas, half-band widths and the Cauchy-Gauss proportionality of the calculated component bands from the band indices.

(ii) Program XIV. This program calculates and lists the individual computed abscissal values of the calculated band envelope from the band indices. It also provides a set of punched cards (or a card image output data set) in the standard 8(I5, I4,IX) format.

(iii) Program XV. When provided with the card decks from the experimental spectrum and the computed spectrum from Program XIV this program first passes a five point quadratic convoluting smoothing function through each and evaluates the following quantities as described in reference (2).

(a) The total error spectrum.

(b) The high frequency component of the error spectrum which is attributed to the misfit arising from the noise component of the experimental curve.

(c) The low frequency component of the error spectrum which is attributed to the mathematical misfit of the computed curve, corrected for noise.

This program also serves as a general purpose program for subtracting one spectrum from another. It will operate on both transmission and absorbance ordinate data and yields a punched card output in our standard formats (8) as well as the printed listing.

For all three band fitting programs the experimental data points are read from Hollerith cards each of which carries eight data points in 8(I5,I4,IX) format. The abscissal units are wavenumber in $\text{cm}^{-1} \times 10$, recorded at constant wavenumber intervals in diminishing sequence. The ordinate units are transmittance $\times 1000$; these conditions were dictated by the standardized digital encoding conditions used in our laboratory (11,12). The input and output indices for peak height (x_1) and band center (x_2) are in units of absorbance and cm^{-1} respectively. A subroutine SORT

checks the sequence of the experimental data cards and will make a limited number of corrections for misplaced cards; all such corrections are noted in the print-out.

The programs are written in FORTRAN IV.* They are listed and described in the main section of this Bulletin with interpretive detail and comment. A set of numerical test data based on a simulated four band spectrum is included. A more critical appraisal with some discussion of the physical significance of the band fits obtained is given on pp. 64-65 of reference (13).

* IBM System/360 Basic Programming Support FORTRAN IV.
(Version 8.1).

ALGEBRAIC STATEMENT OF THE PROBLEM OF
SPECTRAL BAND FIT OPTIMIZATION

A. The Cauchy-Gauss Product Function

The experimental band envelope is approximated by the function

$$\begin{aligned} (T/T_0)_{\text{vcalc}} = \exp - 2.30258 \left\{ \alpha + \sum_{P=1}^M x_1(P) (1+x_3^2(P) (\nu-x_2(P))^2)^{-1} \right. \\ \left. \cdot \exp \left[- x_4^2(P) (\nu-x_2(P))^2 \right] \right\} \end{aligned} \quad [1]$$

where $(T/T_0)_{\text{vcalc}}$ is the computed ordinate at the wavenumber ν in transmittance units; α , x_1 , x_2 , x_3 , x_4 , are the adjustable indices and M is the number of constituent bands; x_1 is the peak height in absorbance units, x_2 is the wavenumber position of the band center in cm.^{-1} ; x_3 and x_4 jointly define the half-band width and the Cauchy-Gauss ratio; α is the baseline displacement in absorbance units.

The values of $(x_1 \dots x_4)_p$ and α are varied to minimize ϕ where

$$\phi = \sum f_i^2 \quad [2]$$

with

$$f_i = (T/T_0)_{\text{vobs}} - (T/T_0)_{\text{vcalc}} \quad [3]$$

The iteration step is expressed most succinctly in the form developed by Meiron (5)

$$\underline{x}_{m+1} = \underline{x}_m - (\underline{B}_m + p\underline{C}_m)^{-1} \cdot \underline{G}_m \quad [4]$$

where \underline{x}_m is the vector of indices after m iterations and \underline{B} is a matrix equal to $\underline{A}^T \underline{A}$ where \underline{A} is a matrix of the partial derivatives $\partial f_i / \partial x_j$. The diagonal matrix \underline{C} is formed from \underline{B} by setting the off-diagonal terms to zero; p is a scalar damping factor, the value of which is adjusted to minimize ϕ during each iteration cycle; \underline{G} is the gradient vector ($\text{grad } \phi$).

Equation [4] can be rewritten

$$\underline{x}_{m+1} C_{-m}^{\frac{1}{2}} = \underline{x}_{-m} C_{-m}^{\frac{1}{2}} - (C_{-m}^{-\frac{1}{2}} B_{-m} C_{-m}^{-\frac{1}{2}} + pI)^{-1} G_{-m} C_{-m}^{-\frac{1}{2}} \quad [5]$$

This is the form of the algorithm developed by Marquardt (5). Our programs compute on this basis, since, from the numerical point of view, it has the advantage that all the diagonal terms are equal to unity. In consequence, no round off difficulties are to be expected, even when the simple Gauss-Jordan procedure is used to solve the system of linear equations (14).

The symbolism used in the above equations conforms with that of our previous publications. Within the computer program it is convenient to handle all the indices in a single array corresponding to the vector \underline{x} and to convert the ordinate scale from decadic to Napierian absorbance. It will simplify the subsequent discussion if we rewrite equation [5] in the form

$$TC_{(W)} = EXP - \left\{ X_{(N)} + \sum_{I=1}^{I=M} X_{(I)} (1 + X_{(I+2M)}^2 (W - X_{(I+M)})^2)^{-1} \right. \\ \left. \cdot EXP \left[- (X_{(I+3M)}^2 (W - X_{(I+M)})^2) \right] \right\} \quad [6]$$

where the symbolism conforms more closely with that used in the FORTRAN program.

Equation [2] similarly transposes to

$$FS = \sum_1^{NP} F^2 \quad [7]$$

$$= \sum_1^{NP} (Y_{(W)} - TC_{(W)})^2 \quad [8]$$

B. The Cauchy-Gauss Sum Function

In the symbolism of reference (2) this equation is written

$$(T/T_0)_{vcalc} = \exp - 2.30258 \left\{ \alpha + \sum_{P=1}^M \left[x_1(P) (1 + x_3^2(P) (v - x_2^2(P))^2)^{-1} \right. \right. \\ \left. \left. + x_5(P) \cdot \exp - (x_4^2(P) (v - x_2^2(P))^2) \right] \right\} \quad [9]$$

Whereas the product function requires the adjustment of $4M+1$ indices, the sum function, as written above, has $5M+1$ adjustable parameters, where M is the number of constituent bands. It is used in these programs with the restraint that $x_4 = kx_3$, where k is a constant that is selected by an input card. In this form the sum function has proved superior to the product function in some instances (e.g. for fitting single bands generated by convoluting a Cauchy band with a triangular slit function (3)). Subsequent experience has shown that the sum function will often yield solutions in which x_1 or x_5 assumes negative values, and such solutions can have doubtful physical significance, though they may be acceptable analytically. Provision is included in these programs to restrict x_1 and x_5 to positive values if desired. Values of k in the range 0.4-0.8 are usually satisfactory. An alternative version of the program in which the restraint on x_4/x_3 has been removed is given by Program XVI in Bulletin 13.

In the quasi-FORTRAN symbolism* equation [9] becomes

$$TC_{(W)} = EXP - \left\{ X_{(N)} + \sum_{I=1}^{I=M} \left[X_{(I)} (1 + X_{(I+2M)}^2 (W - X_{(I+M)})^2 \right)^{-1} + X_{(I+3M)} EXP \left(- X_{(I+2M)}^2 \text{CAY}^2 (W - X_{(I+M)})^2 \right) \right] \right\} \quad [10]$$

 * We apologize for introducing this bastardized mathematical symbolism at several places in this Bulletin, but it is convenient for promoting cross-communication between the FORTRAN programs and the basic mathematical logic. We further admit to inconsistency in the symbolism for the band indices. We have chosen to use the following sets of symbols interchangeably for the band indices, whichever the context would indicate as being the more convenient: $(x_1, x_2, x_3, x_4, x_5, \alpha)$; $(X(1), X(2), X(3), X(4), X(5), \text{ALPHA})$; $(X(I), X(J), X(K), X(L), X(L), X(N))$: $(X(I), X(I+M), X(I+2M), X(I+3M), X(I+3M), X(N))$ where $\text{CAY} = x_4/x_3$, and $X(N), X(I)$ and $X(I+3M)$ have been transposed from decadic absorption to Napierian absorption.

The procedure for introducing the perturbation is as follows. We consider a system of particles in a box of volume V . The unperturbed Hamiltonian is H_0 and the perturbation is H_1 . The total Hamiltonian is $H = H_0 + H_1$. The energy levels of H_0 are $E_n^{(0)}$ and the eigenfunctions are $\psi_n^{(0)}$. The energy levels of H are E_n and the eigenfunctions are ψ_n . The perturbation theory is applied to the energy levels and eigenfunctions of H . The first-order correction to the energy level E_n is given by $E_n^{(1)} = \langle \psi_n^{(0)} | H_1 | \psi_n^{(0)} \rangle$. The first-order correction to the eigenfunction ψ_n is given by $\psi_n^{(1)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}} \psi_m^{(0)}$. The second-order correction to the energy level E_n is given by $E_n^{(2)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle \langle \psi_n^{(0)} | H_1 | \psi_m^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}}$. The second-order correction to the eigenfunction ψ_n is given by $\psi_n^{(2)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle \langle \psi_n^{(0)} | H_1 | \psi_m^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}} \psi_m^{(0)}$.

$$E_n = E_n^{(0)} + E_n^{(1)} + E_n^{(2)} + \dots$$

It is shown that this classic case is a special case of the more general case of a system of particles in a box of volume V . The energy levels of H_0 are $E_n^{(0)}$ and the eigenfunctions are $\psi_n^{(0)}$. The energy levels of H are E_n and the eigenfunctions are ψ_n . The perturbation theory is applied to the energy levels and eigenfunctions of H . The first-order correction to the energy level E_n is given by $E_n^{(1)} = \langle \psi_n^{(0)} | H_1 | \psi_n^{(0)} \rangle$. The first-order correction to the eigenfunction ψ_n is given by $\psi_n^{(1)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}} \psi_m^{(0)}$. The second-order correction to the energy level E_n is given by $E_n^{(2)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle \langle \psi_n^{(0)} | H_1 | \psi_m^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}}$. The second-order correction to the eigenfunction ψ_n is given by $\psi_n^{(2)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle \langle \psi_n^{(0)} | H_1 | \psi_m^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}}$.

or equivalent volume V is given by

$$E_n = E_n^{(0)} + E_n^{(1)} + E_n^{(2)} + \dots$$

The procedure for introducing the perturbation is as follows. We consider a system of particles in a box of volume V . The unperturbed Hamiltonian is H_0 and the perturbation is H_1 . The total Hamiltonian is $H = H_0 + H_1$. The energy levels of H_0 are $E_n^{(0)}$ and the eigenfunctions are $\psi_n^{(0)}$. The energy levels of H are E_n and the eigenfunctions are ψ_n . The perturbation theory is applied to the energy levels and eigenfunctions of H . The first-order correction to the energy level E_n is given by $E_n^{(1)} = \langle \psi_n^{(0)} | H_1 | \psi_n^{(0)} \rangle$. The first-order correction to the eigenfunction ψ_n is given by $\psi_n^{(1)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}} \psi_m^{(0)}$. The second-order correction to the energy level E_n is given by $E_n^{(2)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle \langle \psi_n^{(0)} | H_1 | \psi_m^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}}$. The second-order correction to the eigenfunction ψ_n is given by $\psi_n^{(2)} = \sum_{m \neq n} \frac{\langle \psi_m^{(0)} | H_1 | \psi_n^{(0)} \rangle \langle \psi_n^{(0)} | H_1 | \psi_m^{(0)} \rangle}{E_n^{(0)} - E_m^{(0)}}$.

$$E_n = E_n^{(0)} + E_n^{(1)} + E_n^{(2)} + \dots$$

PROGRAM X

PROGRAM X

The Basic Band Fit Optimization Program

(PC-116)

The Input Data

Cards 1 and 2 are heading cards and can carry any desired alphameric indexing, or identification statements (HEAD1, HEAD2). These cards must be included though they may be blank.

Card 3 carries ten fixed point instructions, NDATA, IDECK, NP, M, KURVE, NSEC, NI, MLIST, LIMIT, NONEG, in format 10I5.

NDATA

Use NDATA = 1 to process a single data set or the terminal data set of a series.

Use NDATA = 2 for an initial or intermediate set of a series. After completing the computation, the program will proceed automatically to execute the next computation of the series.

IDECK

Use IDECK = 1 to list the output on the printer only.

Use IDECK = 2 to punch an additional output card deck carrying the optimized indices (one band per card) in the format for input to Programs XIII and XIV. The terminal card of the deck carries the baseline constant ALPHA.

NP

is the number of experimental data points (maximum 2000).

M

is the number of component bands (maximum 20).

KURVE

Use KURVE = 1 for the product function, and for pure Cauchy and pure Gauss functions.

Use KURVE = 2 for the sum function.

NSEC

is the maximum permitted computation time in seconds. This is the time within the iterative cycling routine. If exceeded the program will print the last set of indices obtained and either terminate or proceed to the next data set according to the value of IDECK.

NI is the maximum permitted number of iteration cycles, a recommended value is 10.

MLIST Use MLIST=1 to print the input and output data and a minimal report on the progress of the optimization convergence, as is shown in the numerical examples on pp. 99 and 103. This will normally suffice unless difficulties are encountered.

Use MLIST=2 to print additional information about the extreme values of the B and $\underline{C}^{-\frac{1}{2}}\underline{BC}^{-\frac{1}{2}}$ matrix elements (see p. 6).

Use MLIST=3 to record the restraints applied by LIMIT and NONEG (see below).

Use MLIST=4 for a combination of MLIST=2 and MLIST=3.

LIMIT Use LIMIT=1 to restrict the half-widths of the component bands within the range 1 cm.^{-1} to 50 cm.^{-1} .
If LIMIT=2 no restriction is applied.

NONEG Use NONEG=1 with the sum function to restrict both the Cauchy and Gauss bands to zero or positive values.
If NONEG=2 no restriction is applied.
Always use NONEG=2 with the product function.

Card 4 carries two floating point instructions for the product function and three for the sum function in formats 2F15.5 or 3F15.5 respectively.

WB is the highest (starting) wavenumber of the experimental data deck in cm.^{-1} .

WI is the constant wavenumber interval in cm.^{-1} . By convention this interval is taken as positive for a diminishing wavenumber sequence.

CAY is the ratio x_4/x_3 and is required only for the sum function. Suggested trial values are 0.5 or 0.8.

Card 5 carries the instructions DOWN, UP and CHANGE in format 3F15.5 for varying the damping factor (see p. 18).

Recommended values are 0.01 1000.0 0.5

Card Deck 6 is the main data deck carrying the NP experimental data points. These must be sequenced in diminishing order of wavenumber. Subroutine SORT will check this sequence and make a limited number of corrections. It is discussed more fully in Bulletin 11. It is important to make sure that the starting wavenumber of the deck corresponds with WB.

These cards must be punched in format 8(I5, I4, 1X) with the wavenumber in units of $\text{cm}^{-1} \times 10$ followed by the intensity in transmittance $\times 1000$ (i.e. a transmittance of 0.500 at 1000.0 cm^{-1} followed by a transmittance of 0.499 at 999.5 cm^{-1} is encoded as 1000 500 9995 499).

Card Deck 7

This is a deck of M cards, each of which carries four input indices for one band in format 4F15.5. For the product function these are x_1, x_2, x_3 and x_4 which appear in the FORTRAN symbolism as X(I), X(J), X(K) and X(L). The units of x_1 are absorbance and of $x_2 \text{ cm}^{-1}$. For the sum functions x_1, x_2, x_3 and x_5 are listed and they also appear in the FORTRAN symbolism as X(I), X(J), X(K) and X(L). It is important to observe that X(L) has a different connotation for the sum function than for the product function. The units of both x_1 and x_5 are absorbance.

Card 8

This is the terminating card and carries the input value of the baseline constant α in F15.5 format. It is X(N) in the FORTRAN notation. The units of α are absorbance. The program requires that this card be included, even if $\alpha = 0.0$.

Note that this program calls the library subroutines SETCLK and RDCLK which are discussed in Bulletin 11. If these are not available appropriate alterations have to be made in the program.

B. Description of the Basic Program

The Initial Section, ending at statement 31, accepts the input data, checks the sequence of the abscissal data points by subroutine SORT and transposes the input ordinate data from the fixed point array IY(I) on a scale of transmittance $\times 1000$ to a floating point array Y(I) on a scale of transmittance.

This is followed by the Input Section which continues to statement 154. Here the initial values of several quantities are set. These include the number of completed iterations (NIT), the total number of band indices (N), the starting value of the damping factor (P1), the number of entries (NAL) in the array AQ(IM), and TERM which is needed later for a convergence check. The values of the input indices are then accepted in the DO loop ending at statement 153; they are stored in the array X(I). By this stage the output headings have been printed, including a list of the input indices; the ordinate indices have been converted from a decadic to a Napierian logarithmic scale, as also has the baseline constant X(N). The timing subroutine SETCLK is activated at the beginning of this section.

The central core of the program is the (G,AQ,F) Section, which runs from statement 200 to statement 233. Here, initial values are first set for several quantities; FS is the value of the minimization function within a given iteration cycle (cf. equation [7]). FM is the maximal difference between the observed and computed ordinates, and WFM is the wavenumber position of FM.

The values of FS, the matrix \underline{B} and the vector G are next calculated. The main computation occurs in the double DO loop between statements 203 and 218. For each experimental data point SUBROUTINE POINT determines the ordinate value of the computed curve (cf. equations [6] and [10]). This is compared with the experimental ordinate value to determine F, FM, and FS. The partial differentials are computed in the DO loops beginning at statement 207 for the product function and at statement 210 for the sum function (see p. 17). These comprise one row of the \underline{A} matrix for each data point and are stored for one row at a time in the array AM(I). The matrix \underline{B} and the vector G are generated by a storage saving technique which avoids the need to accumulate the complete \underline{A} matrix; the algebra involved is discussed on p. 19. Since \underline{B} is symmetric, only the matrix elements that lie above the diagonal need be calculated. These are stored in the array AQ(IM) at statement 218, and transferred serially to the array A(I,IJ) as required for the subsequent calculations in the DO loop beginning at statement 219.

The diagonal elements of \underline{B} comprise the non-zero terms of \underline{C} . The matrix $\underline{C}^{-\frac{1}{2}}$ is formed at statement 226 and stored in the array DIA(I). The upper half of \underline{B} is converted to $\underline{C}^{-\frac{1}{2}}\underline{B}\underline{C}^{-\frac{1}{2}}$ and stored in the array AQ(IM). The vector GAST(I) is formed at the same time at statement 227.

The diagonal terms of $\underline{C}^{-\frac{1}{2}}\underline{B}\underline{C}^{-\frac{1}{2}}$ are unity and the off diagonal terms are correlation coefficients between the indices. If numerical difficulties occur, it is helpful to have a record of the extreme values of these coefficients, and also of the minimal and maximal values of the diagonal elements of \underline{B} . When the program is operated with MLIST=2 or 4, these are located and recorded, using the following terminology:

ADMIN	Value of minimal diagonal element of \underline{B}
MINAD	Location of ADMIN
ADMAX	Value of maximal diagonal element of \underline{B}
MAXAD	Location of ADMAX
AMIN	Value of minimal off-diagonal element of $\underline{C}^{-\frac{1}{2}}\underline{B}\underline{C}^{-\frac{1}{2}}$
MINA1	Row location of AMIN
MINA2	Column location of AMIN
AMAX	Value of maximal off-diagonal element of $\underline{C}^{-\frac{1}{2}}\underline{B}\underline{C}^{-\frac{1}{2}}$
MAXA1	Row location of AMAX
MAXA2	Column location of AMAX

The absolute values of AMIN and AMAX must be less than unity; an approach to this limiting value implies a strong interaction between the indices involved and may help to locate a source of difficulty in optimization.

This major computational section ends with the evaluation of the gradient length (GL) at statement 233. The time is read (RDCLK) and the accumulated computation time evaluated (ISECS). The values of FS, GI, WFM, FM, NIT, and ISECS are printed. These appear in tabular form and, under normal conditions with MLIST = 1 or 3, they provide all the information needed to demonstrate satisfactory convergence to the m^{th} iteration cycle of equation [5].

The values of FS, B, G, and C having been evaluated above, it is still necessary to select the optimal value of p to complete the $m+1^{\text{th}}$ iteration.* The optimal value of FS can be extremely sensitive to the choice of P. For the first approximation $P=0.1$ is used, but in subsequent cycles the best value of P is sought by an automated, though essentially empirical method which is described in the Appendix to reference (2) and is discussed further on p. 18 of this Bulletin. Four values of P are obtained for each iteration cycle, and the corresponding values of X(I) and FS are calculated; they are designated XP(I) and FSP; if MLIST = 2 or 4 all four values of P and FSP are printed. The value of P associated with the minimal value of FSP is chosen and the corresponding indices in XP(I) are transferred to XB(I), at statement 305, as starting values for the next iteration.

These operations take place in the (P,INVERT,XP) Section, and in the (FSP) Section. Both sections are traversed four times in each iteration cycle; the logical path is controlled by the computed GO TO statement 252. In the first three traversals the

* Note that p of equation [5] is transposed to P in the FORTRAN notation.

change in P is controlled by the values of UP, DOWN, and CHANGE. The fourth P value is interpolated by the method discussed in the Appendix to reference (2); this occurs between statements 263 and 270.

The damping factor is added to $C^{-\frac{1}{2}}BC^{-\frac{1}{2}}$ at statement 267 and the linear system of equations is solved by the Gauss-Jordan elimination method in which the diagonal members are used as a pivot (14).

Messages indicating numerical difficulties may be printed at statements 271 and 284. The former will draw attention to difficulty in interpolating a fourth value for P, but the execution of the program will continue. The latter indicates that there are difficulties with the Gauss-Jordan procedure. In that event the computation will output at the end of the current iteration cycle. This is a safety check and is not likely to occur.

The decision whether to continue to the next iteration, or to terminate, is made following statement 312 in the Terminal Section. The number of completed iterations (NIT) is compared with the permitted number (NI), and the elapsed computation time is compared with the permitted time (NSEC). Two checks for slow convergence are also supplied. One is the fractional change in the minimization function (TERM/FSM). The computation terminates if this ratio falls below 1.002. The program will also terminate should GL be reduced below 0.0001. This is also an indication of slow convergence, though normally the TERM/FSM ratio test will terminate the program first. The program will also terminate should FM be reduced below 0.001, which indicates that a maximal significant fit has been achieved; under normal circumstances, the accuracy of the experimental ordinate measurement will not be better than 0.001 transmittance units.

At the end of the computation, the program tabulates the optimized values of the indices, the corresponding values of the error function (FSM), the root-mean-square of the residuals (DIS), the maximal ordinate error (FM), and the wavenumber of FM (WFM).* A check is made against NDATA; if NDATA = 2 the program proceeds to process the next data deck, otherwise it calls the EXIT routine and the calculations are completed.

If LIMIT = 1 or NONEG = 1, restraints are applied to the permitted values of the indices. These boundary conditions are

* If WFM remains constant throughout the iteration series, it most probably indicates that there is a punch error in the corresponding experimental ordinate, or suggests the need to introduce an additional component band.

monitored and controlled in the section Boundary Conditions to Limit the Ranges of X(1), X(2), X(4), and X(5). It has been observed that occasionally a band may be virtually eliminated by making the half-width excessively wide, or, more commonly, reducing it to a spike so that it falls almost wholly between two consecutive abscissal data points.* Limits can be set to X(3) and X(4), for the product function, or to X(3) for the sum function which will restrict the half-width within the spectroscopically significant ranges of 1 cm.^{-1} to 50 cm.^{-1} . These limiting conditions are summarized in Table I and discussed further in connection with Program XIII on p. 95.

TABLE I

Limiting Values for X(3) and X(4) to Restrain the Half-Band Width in the Approximate Range 1 to 50 cm.^{-1}

Product Function

Half-band width $< 1 \text{ cm.}^{-1}$ if $[X(3)] > 2.0$ or $[X(4)] > 1.0$
Half-band width $< 50 \text{ cm.}^{-1}$ if:
 either $[X(3)] > 0.03$
 or $[X(3)] \leq 0.03$ but $[X(4)] > 0.0333$

Sum Function with CAY in the Range 0.4-0.8

Half-band width $< 1 \text{ cm.}^{-1}$ if $[X(3)] > 2.0$
Half-band width $> 50 \text{ cm.}^{-1}$ if $[X(3)] < 0.042$

Negative values of X(3) and X(4) not infrequently occur for the product function and of X(3) for the sum function. Since these quantities only enter the band shape calculations as squared terms the sign is not significant, and it is the absolute values of these quantities that determine the boundary conditions listed in Table I.

For the sum function, negative values of X(1) and X(5) are also frequently encountered, and indicate that the optimized solution involves a subtraction of a Gauss component from a Cauchy

* It is also possible for a band to be "lost" by a large abscissal displacement of X(2) out of the computed wavenumber range. We have only rarely encountered this difficulty with this program, though it occurred more frequently with the Method I optimization technique when highly inaccurate starting values were employed (2).

component, or vice versa. This can be restricted by setting NONEG=1 which causes a negative X(1) or X(5) ordinate index to be replaced by a positive one, one-tenth of the intensity of that of the preceding iteration. This tends progressively to yield a pure Gauss or Cauchy curve. Generally this gives a solution that converges less efficiently; it can sometimes be circumvented by altering CAY.

C. Subroutine POINT

This small subroutine computes the values of $\ln(T_0/T)_v$ for a given set of variables X(I), at a given wavenumber W. It also computes the quantities PC(I) and PG(I) which correspond to

$$x_1 (1 + x_3^2 (v - x_2)^2)^{-1}$$

and

$$x_4^2 (v - x_2)^2$$

of equations [1] and [6]; these are needed in the evaluation of the arrays of partial derivatives AM(I) at statements 207-209 and 210-212.

D. The Method for Selecting the Damping Factor P

The evaluation of P is crucial to the efficient functioning of the program and some further comment is pertinent.

The technique we use to obtain an optimal P is distinctly an arbitrary one. During the initial development of the program we used an S.D.S. 920 computer with direct access, permitting selected values of P to be introduced on demand from a typewriter. We later used a one-dimensional search by Fibonacci numbers (15), also under the operator's direct control. This would still appear to be the best approach when direct access to the computer is possible. In attempting to achieve a fully automated procedure we first developed a method whereby a succession of preselected damping factors was tested. This was successful in several cases, but often the conditions for rapid convergence were extremely sensitive, and so limited that they might be completely missed. Later we tested the method described by Marquardt (5), but tests on practical examples showed that some efficiency is lost by always accepting the lowest value of P. The method we finally adopted has proved acceptable in most cases: nevertheless it can only be regarded as a compromise solution.

Our method is sensitive to the preselected values of UP, DOWN and CHANGE. In cases where difficulty is encountered, the

values of these quantities should be adjusted. A drawback to the current automatic procedure is that no provision is made to deal with cases where the damping factors must be greatly increased to achieve convergence (i.e. by 10^4 or more). The danger of this situation has been indicated by Marquardt and his article should be consulted (5). We have rarely encountered this difficulty; a more common problem arises with very small damping constants, but here successful convergence can usually be achieved if sufficient iterations are allowed.

E. The Evaluation of the B Matrix

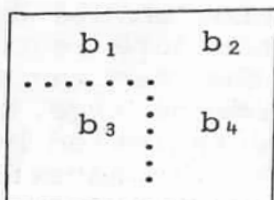
The B matrix is constructed from a vector of binary product terms of A, which is stored in the array AQ(IM). Advantage is taken of the symmetry of B; only the terms above the diagonal need to be evaluated since $A_{ji} = A_{ij}$. The lower half of B can therefore be obtained by interchange of the indices in the A(I,IJ) array; this reduces the number of B elements to be computed from N^2 to $N(N+1)/2$.

The binary products of the A matrix are computed in a sequence that permits all the elements in a single row of B to be evaluated simultaneously by a summation procedure which can be illustrated with reference to a 2×3 A matrix as follows:

<u>A</u> ^T	<u>A</u>
a ₁₁ a ₂₁ a ₃₁	a ₁₁ a ₁₂
a ₁₂ a ₂₂ a ₃₂	a ₂₁ a ₂₂
	a ₃₁ a ₃₂

<u>B</u>
(a ₁₁ a ₁₁ + a ₂₁ a ₂₁ + a ₃₁ a ₃₁) (a ₁₁ a ₁₂ + a ₂₁ a ₂₂ + a ₃₁ a ₃₂)
(-----) (a ₁₂ a ₁₂ + a ₂₂ a ₂₂ + a ₃₂ a ₃₂)

On the first passage through the DO loop beginning at statement 203, the three product terms $a_{11}a_{11}$, $a_{11}a_{12}$, and $a_{12}a_{12}$ are evaluated and stored in AQ(1), AQ(2), and AQ(3) at statement 218. The second passage yields $a_{21}a_{21}$, $a_{21}a_{22}$, and $a_{22}a_{22}$ which are added respectively to AQ(1), AQ(2), and AQ(3). The third and final cycle adds $a_{31}a_{31}$ to AQ(1), $a_{31}a_{32}$ to AQ(2) and $a_{32}a_{32}$ to AQ(3), to complete the first, second and fourth elements of B. The b_3 element, below the diagonal is equal to b_2 .



F. The Partial Derivatives

The differential equations $\partial f_i / \partial x_k$ are computed for the product and sum functions in the DO loops beginning at statements 207 and 210 respectively.

From equation [3],

$$\begin{aligned} f_i &= T_{\text{vobs}} - T_{\nu} \\ &= T_{\text{vobs}} - e^{-A_{\nu}} \end{aligned} \quad [11]$$

where T_{ν} and A_{ν} are the transmittance and Napierian absorbance ordinates for the calculated curve at wavenumber ν .

It follows that

$$\begin{aligned} \partial f_i / \partial x_k &= \partial f_i / \partial A \cdot \partial A / \partial x_k \\ &= -e^{-A_{\nu}} \cdot \partial A / \partial x_k \\ &= -T_{\nu} \cdot \partial A / \partial x_k \end{aligned} \quad [12]$$

For the product function we may write

$$T = \exp - [x_1' P_C P_g + \alpha'] \quad [13]$$

where

$$P_C = 1 / (1 + R^2 x_3^2) \quad [14]$$

$$P_g = \exp - [R^2 x_4^2] \quad [15]$$

$$R = (\nu - x_2) \quad [16]$$

in which x_2, x_3, x_4 have their usual connotation from equation [1],
 $x_1' = 2.30258x_1$ and $\alpha' = 2.30258\alpha$.

Differentiation yields the expressions

$$\partial f_i / \partial x_1' = TP_C P_g \quad [17]$$

$$\partial f_i / \partial x_2 = 2x_1' TP_C P_g (x_4^2 + P_C x_3^2) R \quad [18]$$

$$\partial f_i / \partial x_3 = -2x_1' x_3 TP_C^2 P_g R^2 \quad [19]$$

$$\partial f_i / \partial x_4 = -2x_1' x_4 TP_C P_g R^2 \quad [20]$$

$$\partial f_i / \partial \alpha' = T \quad [21]$$

Setting

$$\begin{aligned} S_p &= 2x_1' TP_C P_g R \\ &= 2x_1' R \cdot \partial f_i / \partial x_1' \end{aligned} \quad [22]$$

equations [18 to 20] reduce to

$$\partial f_i / \partial x_2 = S_p (x_4^2 + P_C x_3^2) \quad [23]$$

$$\partial f_i / \partial x_3 = -S_p x_3 P_C R \quad [24]$$

$$\partial f_i / \partial x_4 = -S_p x_4 R$$

Likewise, we have for the sum function with $x_5' = 2.30258x_5$

$$A_v = x_1' P_C + x_5' P_g + \alpha' \quad [25]$$

and with the restraint that $x_4 = kx_3$

$$P_g = \exp - [R^2 k^2 x_3^2] \quad [26]$$

The expressions for the derivatives are

$$\partial f_i / \partial x_1' = TP_C \quad [27]$$

$$\partial f_i / \partial x_2 = S_s x_3 \quad [28]$$

$$\partial f_i / \partial x_3 = -S_S R \quad [29]$$

$$\partial f_i / \partial x_5' = TP_g \quad [30]$$

$$\partial f_i / \partial \alpha' = T \quad [31]$$

where

$$S_S = 2x_3 TR(x_1' P_C^2 + x_5 k^2 P_g) \quad [32]$$

$$T = \exp[-(x_1' P_C + x_5' P_g + \alpha')] \quad [32A]$$

THE TEST DATA

As test data for the band fit programs, curves generated from overlapping systems of four bands are used. These are described in connection with Program XIV and are illustrated in Figs. 1 and 2.

Four Band Test Curve for Product Function

X(1)	X(2)	X(3)	X(4)
0.300	970.0	0.200	0.100
0.600	955.0	0.200	0.200
0.300	940.0	0.100	0.100
0.400	920.0	0.200	0.100

Alpha = 0.05

NP = 200 WB = 1000.0 WI = 0.5

Four Band Test Curve for Sum Function

X(1)	X(2)	X(3)	X(5)
0.200	970.0	0.200	0.100
0.400	955.0	0.200	0.200
0.100	940.0	0.100	0.200
0.250	920.0	0.200	0.150

Alpha = 0.05

NP = 200 WB = 100.0 WI = 0.5 CAY = 0.8

FOUR BAND TEST CURVE (PRODUCT)

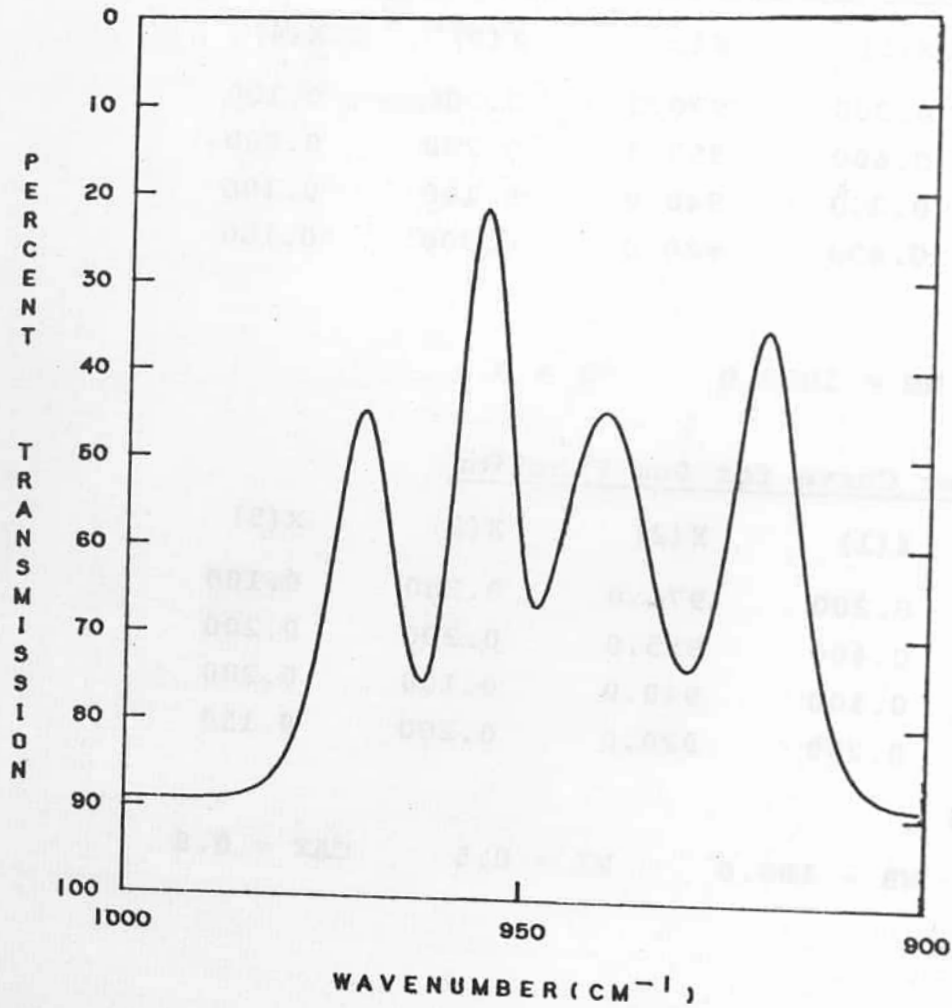


Fig. 1 Four band test curve for the Cauchy-Gauss product function.

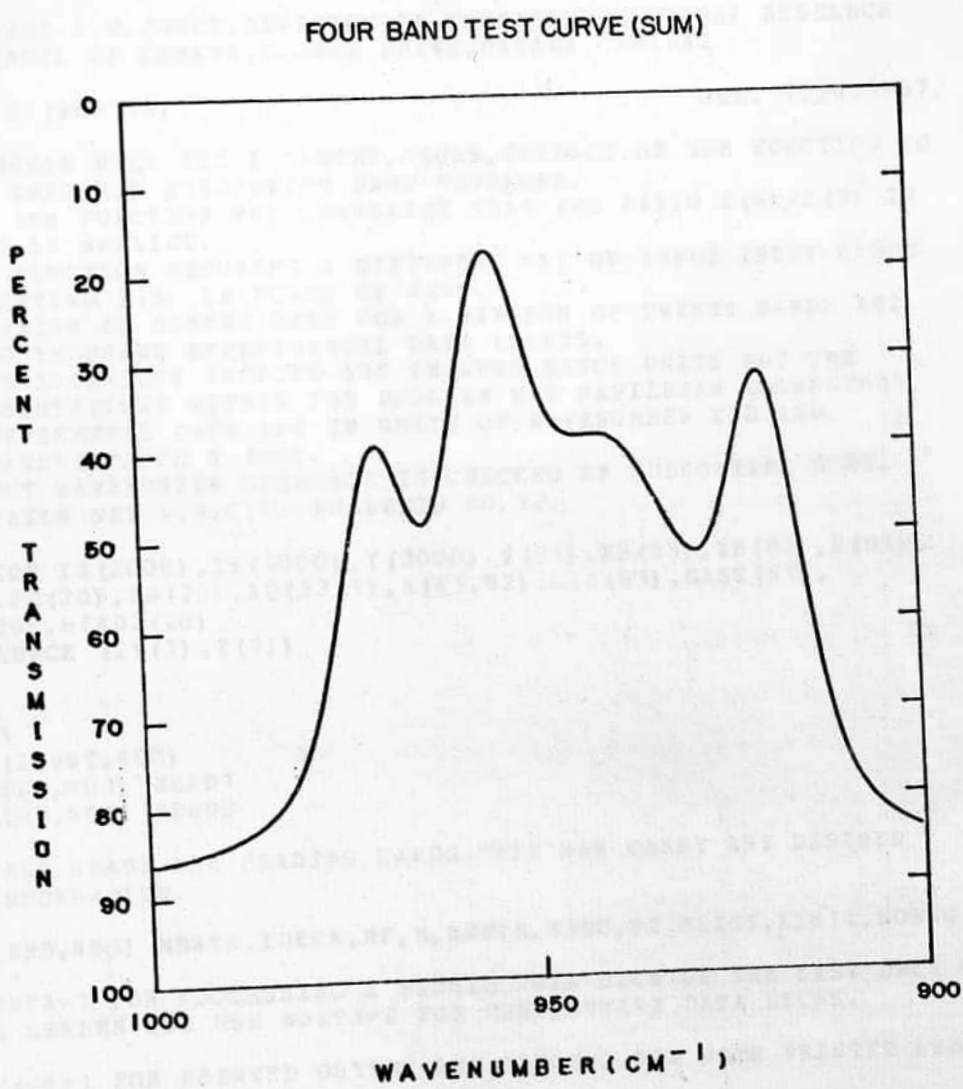


Fig. 2 Four band test curve for the Cauchy-Gauss sum function.

C		10
C	*****	20
C	*	30
C	* SPECTRAL BAND FIT OPTIMIZATION PROGRAM *	40
C	*	50
C	* BASIC VERSION. *	60
C	*	70
C	*****	80
C		90
C	J. PITHA AND R. N. JONES, DIVISION OF CHEMISTRY, NATIONAL RESEARCH	100
C	COUNCIL OF CANADA, SUSSEX DRIVE, OTTAWA, CANADA.	110
C		120
C	PROGRAM X (PC-116) .	130
C		140
C	JULY 12TH. 1967.	150
C	THIS PROGRAM WILL FIT A CAUCHY, GAUSS, PRODUCT, OR SUM FUNCTION TO	160
C	AN INFRARED ABSORPTION BAND ENVELOPE.	170
C	FOR THE SUM FUNCTION THE RESTRAINT THAT THE RATIO X(4)/X(3) IS	180
C	CONSTANT IS APPLIED.	190
C	THE SUM FUNCTION REQUIRES A DIFFERENT SET OF INPUT INDEX CARDS	200
C	CARRYING X(5) IN PLACE OF X(4).	210
C	THIS VERSION IS DIMENSIONED FOR A MAXIMUM OF TWENTY BANDS AND	220
C	TWO THOUSAND EXPERIMENTAL DATA POINTS.	230
C	THE BAND INTENSITY INDICES ARE IN ABSORBANCE UNITS BUT THE	240
C	COMPUTATIONS WITHIN THE PROGRAM USE NAPIERIAN LOGARITHMS.	250
C	THE EXPERIMENTAL DATA ARE IN UNITS OF WAVENUMBER X10 AND	260
C	TRANSMITTANCE X 1000.	270
C	THE INPUT WAVENUMBER SEQUENCE IS CHECKED BY SUBROUTINE SORT.	280
C	FOR DETAILS SEE N. R. C. C. BULLETIN NO. 12.	290
C		300
C	DIMENSION IX(2000), IY(2000), Y(2000), X(81), XP(81), XB(81), G(81),	310
C	1AM(81), PC(20), PG(20), AQ(3321), A(81,82), DIA(81), GAST(81),	320
C	2HEAD1(20), HEAD2(20)	330
C	EQUIVALENCE (IY(1), Y(1))	340
C	IRD=1	350
C	IPCH=2	360
C	IPRNT=3	370
C	11 WRITE (IPRNT,400)	380
C	READ (IRD,401) HEAD1	390
C	READ (IRD,401) HEAD2	400
C		410
C	HEAD1 AND HEAD2 ARE HEADING CARDS. THEY MAY CARRY ANY DESIRED	420
C	INFORMATION.	430
C		440
C	READ (IRD,403) NDATA, IDECK, NP, M, KURVE, NSEC, NI, MLIST, LIMIT, NONEG	450
C		460
C	USE NDATA=1 FOR PROCESSING A SINGLE DATA DECK OR THE LAST DECK OF	470
C	A SERIES AND USE NDATA=2 FOR CONSECUTIVE DATA DECKS.	480
C		490
C	USE IDECK=1 FOR PRINTED OUTPUT AND IDECK=2 FOR BOTH PRINTED AND	500
C	CARD OUTPUT.	510
C		520
C	NP IS THE NUMBER OF DATA POINTS.	530
C		540
C	M IS THE NUMBER OF CALCULATED BANDS.	

C		550
C	USE KURVE=1 FOR PRODUCT FUNCTION AND KURVE=2 FOR SUM FUNCTION.	560
C		570
C	NSEC IS THE MAXIMUM PERMITTED COMPUTATION TIME IN SECONDS.	580
C		590
C	NI IS THE MAXIMUM NUMBER OF PERMITTED ITERATIONS.	600
C		610
C	MLIST CONTROLS THE AMOUNT OF INFORMATION REPORTED ABOUT THE	620
C	PROGRESS OF THE COMPUTATION.	630
C		640
C	USE MLIST=1 FOR MINIMUM PROGRESS REPORT AND FINAL OUTPUT	650
C	ONLY.	655
C	USE MLIST=2 FOR ADDITIONAL INFORMATION ON THE EXTREME VALUES	660
C	OF THE B MATRIX ELEMENTS DURING EACH ITERATION.	670
C	USE MLIST=3 TO PRINT RESTRAINTS APPLIED BY LIMIT AND NONEG.	680
C	USE MLIST=4 FOR COMBINATION OF MLIST=2 + MLIST=3.	690
C		700
C	CALL SETCLK	710
C	SETCLK IS A TIMING SUBROUTINE.	720
C		730
C	USE LIMIT=1 TO RESTRICT THE HALF-WIDTHS OF THE COMPONENT BANDS	740
C	WITHIN THE RANGE 1-50 CM.-1	750
C	IF LIMIT=2 NO RESTRICTION TO THE HALF-BAND WIDTH IS APPLIED.	760
C		770
C	USE NONEG=1 WITH THE SUM FUNCTION TO RESTRICT X1 AND X5 TO ZERO	780
C	OR POSITIVE VALUES.	790
C	IF NONEG=2 NO RESTRICTION IS APPLIED ----- ALWAYS USE	800
C	NONEG=2 WITH THE PRODUCT FUNCTION.	810
C		820
C	IF (KURVE.EQ.2) GO TO 13	830
C	READ (IRD,404) WB,WI	840
C	GO TO 16	850
C	13 READ (IRD,404) WB,WI,CAY	860
C		870
C	CAY DEFINES THE X(4)/X(3) RATIO IN THE SUM FUNCTION CALCULATIONS.	880
C	FOR CHOICE OF VALUE SEE CAN.J.CHEM. VOL.45 PAGE 2347 (1967)	890
C	VALUES OF CAY IN THE RANGE 0.6 - 0.8 ARE SUGGESTED.	900
C		910
C	WB AND WI ARE THE STARTING WAVENUMBER AND THE WAVENUMBER ENCODING	920
C	INTERVAL IN CM.-1 BY CONVENTION WI IS POSITIVE FOR A	930
C	DIMINISHING WAVENUMBER SEQUENCE.	940
C		950
C	16 IF (IDECK.EQ.1) GO TO 12	960
C	WRITE (IPCH,401) HEAD1	970
C	WRITE (IPCH,401) HEAD2	980
C	12 WRITE (IPRNT,402) HEAD1	990
C	WRITE (IPRNT,402) HEAD2	1000
C	WRITE (IPRNT,408)	1010
C	READ (IRD,404) DOWN,UP,CHANGE	1020
C		1030
C	DOWN,UP AND CHANGE REGULATE THE SEARCH FOR OPTIMAL DAMPING FACTOR.	1040
C	RECOMMENDED TRIAL VALUES ARE DOWN=0.01 UP=1000.0 CHANGE=0.5	1050
C		1060
C	WRITE (IPRNT,409) DOWN,UP,CHANGE	1070

```
WRITE (IPRNT,423) NP,WB,WI
IF (NONEQ.EQ.2) GO TO 14
IF (MLIST.LT.3) WRITE (IPRNT,432)
14 IF (LIMIT.EQ.2) GO TO 15
IF (MLIST.LT.3) WRITE (IPRNT,433)
15 READ (IRD,405) (IX(I),IY(I),I=1, NP)
IWB=WB*10.0+0.5
IWI=WI*10.0+0.5
CALL SORT1 (IX,IY,WB,WI, NP, IPRNT, KLENUP, IWB, IWI)
IF (KLENUP.EQ.1) GO TO 30
20 UP=0.0
DOWN=0.0
CHANGE=0.0
IF (NDATA.EQ.2) GO TO 11
STOP
30 DO 31 I=1, NP
31 Y(I)=IY(I)*0.001

C ***** INPUT SECTION *****
C
N=4*M+1
N1=N+1
NAL=N*N1/2
NIT=0
TERM=1000.0
P1=0.1
IF (KURVE.EQ.2) GO TO 151
WRITE (IPRNT,416)
GO TO 152
151 WRITE (IPRNT,417)
152 DO 153 I=1, M
J=I+M
K=J+M
L=K+M
READ (IRD,404) X(I),X(J),X(K),X(L)
X(I),X(J),X(K) AND X(L) ARE THE SPECTRAL INDICES FOR EACH BAND.
IF (KURVE.EQ.2) GO TO 155
WRITE (IPRNT,410) X(I),X(J),X(K),X(L)
GO TO 157
155 XG=X(K)*CAY
WRITE (IPRNT,406) X(I),X(J),X(K),XG,X(L)
X(L)=2.30258*X(L)
157 X(I)=2.30258*X(I)
153 CONTINUE
READ (IRD,404) X(N)
WRITE (IPRNT,418) X(N)
X(N)=2.30258*X(N)
DO 154 I=1, N
154 XB(I)=X(I)

C ***** (G,AQ,F) SECTION *****
C
200 DO 201 I=1, N
201 G(I)=0.0
```

DO 202 I=1,NAL	1620
202 AQ(I)=0.0	1630
FS=0.0	1640
FM=0.0	1650
FS1=1.0E10	1660
FS2=1.0E10	1670
P1L=P1	1680
IT=1	1690
203 DO 218 II=1,NP	1700
W=IX(II)*0.1	1710
CALL POINT1 (X,PC,PG,W,AC,M,N,CAY,KURVE)	1720
TC=EXP(-AC)	1730
F=Y(II)-TC	1740
FA=ABS(F)	1750
IF (FM.GE.FA) GO TO 206	1760
FM=FA	1770
WFM=W	1780
206 FS=FS+F*F	1790
IF (KURVE.EQ.2) GO TO 210	1800
207 DO 209 I=1,M	1810
J=I+M	1820
K=J+M	1830
L=K+M	1840
AM(I)=TC*PG(I)*PC(I)	1850
R=W-X(J)	1860
SP=2.0*AM(I)*X(I)*R	1870
AM(J)=SP*(X(L)*X(L)+X(K)*X(K))*PC(I)	1880
AM(K)=-SP*R*X(K)*PC(I)	1890
209 AM(L)=-SP*R*X(L)	1900
GO TO 211	1910
210 DO 212 I=1,M	1920
J=I+M	1930
K=J+M	1940
L=K+M	1950
R=W-X(J)	1960
AM(I)=TC*PC(I)	1970
SS=2.0*TC*(X(I)*PC(I)*PC(I)+CAY*CAY*X(L)*PG(I))*R*X(K)	1980
AM(J)=SS*X(K)	1990
AM(K)=-SS*R	2000
212 AM(L)=TC*PG(I)	2010
211 AM(N)=TC	2020
IM=0	2030
DO 218 I=1,N	2040
AMI=AM(I)	2050
G(I)=G(I)+AMI*F	2060
DO 218 IJ=I,N	2070
IM=IM+1	2080
218 AQ(IM)=AQ(IM)+AMI*AM(IJ)	2090
FSM=FS	2100
IM=0	2110
DO 219 I=1,N	2120
DO 219 IJ=I,N	2130
IM=IM+1	2140
219 A(I,IJ)=AQ(IM)	2150

	ADMIN=1.0E+10	2160
	ADMAX=-1.0E+10	2170
	DO 227 I=1,N	2180
	GO TO (224,220,224,220),MLIST	2190
220	IF (A(I,I).GE.ADMIN) GO TO 221	2200
	ADMIN=A(I,I)	2210
	MINAD=I	2220
221	IF (ADMAX.GE.A(I,I)) GO TO 224	2230
	ADMAX=A(I,I)	2240
	MAXAD=I	2250
224	IF (A(I,I).GT.1.0E-10) GO TO 226	2260
	DIA(I)=0.0	2270
	GO TO 227	2280
226	DIA(I)=1.0/SQRT(A(I,I))	2290
227	GAST(I)=G(I)*DIA(I)	2300
	IM=0	2310
	AMIN=1.0E+10	2320
	AMAX=-1.0E-10	2330
	DO 228 I=1,N	2340
	DIAI=DIA(I)	2350
	DO 228 IJ=I,N	2360
	IM=IM+1	2370
	AQ(IM)=A(I,IJ)*DIAI*DIA(IJ)	2380
	GO TO (228,229,228,229),MLIST	2390
229	IF (I.EQ.IJ) GO TO 228	2400
	IF(AQ(IM).GE.AMIN) GO TO 231	2410
	AMIN=AQ(IM)	2420
	MINA1=I	2430
	MINA2=IJ	2440
231	IF (AMAX.GE.AQ(IM)) GO TO 228	2450
	AMAX=AQ(IM)	2460
	MAXA1=I	2470
	MAXA2=IJ	2480
228	CONTINUE	2490
	GL=0.0	2500
	DO 233 I=1,N	2510
	GI=G(I)	2520
233	GL=GL+GI*GI	2530
	SM=-2.0*GL	2540
	GL=SQRT(GL)	2550
C		2560
C	THERE IS AN APPROXIMATION IN THE EVALUATION OF SM BUT WE FIND NO	2570
C	SIGNIFICANT IMPROVEMENT IN ACCURACY OR CONVERGENCE RATE WHEN	2580
C	THE EXACT FORMULA IS USED. IT HAS NOT BEEN GENERALLY	2590
C	INTRODUCED AS IT OCCASIONALLY CAUSES NUMERICAL DIFFICULTIES.	2600
C		2610
C	CALL RDCLK (TIME)	2620
C		2630
C	RDCLK IS A TIMING SUBROUTINE.	2640
C		2650
C	ISECS=TIME+0.5	2660
C	WRITE (IPRNT,407) FS,GL,WFM,FM,NIT,ISECS	2670
C		2680
C	***** MATRIX DATA OUTPUT SECTION *****	2690

C	GO TO (250,249,250,249),MLIST	2700
	249 WRITE (IPRNT,424) MINAD,MAXAD,ADMIN,ADMAX,MINA1,MINA2,AMIN,MAXA1,	2710
	1MAXA2,AMAX	2720
C	***** (P,INVERT,XP) SECTION *****	2730
C		2740
	250 IM=0	2750
	DO 251 I=1,N	2760
	DO 251 IJ=I,N	2770
	IM=IM+1	2780
	AQIM=AQ(IM)	2790
	A(I,IJ)=AQIM	2800
	251 A(IJ,I)=AQIM	2810
	252 GO TO (260,261,262,263,311),IT	2820
	260 P=P1L	2830
	GO TO 265	2840
	261 IF (FS.LE.FS1) GO TO 266	2850
	P=P1L*DOWN	2860
	GO TO 265	2870
	266 P=P1L*UP	2880
	GO TO 265	2890
	262 P=P1*CHANGE	2900
	GO TO 265	2910
	263 X3=1.0/P1	2920
	X4=1.0/P2	2930
	DET=X3*X3*X4*X4*X4-X3*X3*X3*X4*X4	2940
	IF (DET.EQ.0.0) GO TO 269	2950
	AP1=X3*X3*(FS2-FS-SM*X4)	2960
	AP2=X4*X4*(FS1-FS-SM*X3)	2970
	AI=6.0*(AP1-AP2)/DET	2980
	BI=2.0*(X4*AP2-X3*AP1)/DET	2990
	DET=BI*BI-2.0*AI*SM	3000
	IF (DET) 269,279,270	3010
	270 DET=SQRT(DET)	3020
	279 IF (AI.EQ.0.0) GO TO 269	3030
	X3=(-BI+DET)/AI	3040
	X4=(-BI-DET)/AI	3050
	IF (X3.LE.0.0) GO TO 272	3060
	IF (X4.LE.0.0) GO TO 275	3070
	IF (X4.LE.X3) GO TO 274	3080
	275 P=1.0/X3	3090
	GO TO 265	3100
	272 IF (X4.LE.0.0) GO TO 269	3110
	274 P=1.0/X4	3120
	GO TO 265	3130
	269 P=10000.0	3140
	271 WRITE (IPRNT,411)	3150
	265 IT=IT+1	3160
	267 DO 278 I=1,N	3170
	A(I,I)=A(I,I)+P	3180
	278 A(I,N1)=-GAST(I)	3190
	DO 282 I=1,N	3200
	AII=A(I,I)	3210
		3220
		3230

	IF (ALL.EQ.0.0) GO TO 284	3240
	PIV=1.0/ALL	3250
	DO 281 J=I,N1	3260
281	A(I,J)=PIV*A(I,J)	3270
	DO 282 K=1,N	3280
	IF (I.EQ.K) GO TO 282	3290
	Q=A(K,I)	3300
	DO 285 J=I,N1	3310
285	A(K,J)=A(K,J)-Q*A(I,J)	3320
282	CONTINUE	3330
	GO TO 286	3340
284	WRITE (IPRNT,412)	3350
	GO TO 314	3360
286	DO 288 I=1,N	3370
288	XP(I)=X(I)+A(I,N1)*DIA(I)	3380
		3390
	* BOUNDARY CONDITIONS TO LIMIT THE RANGES OF X(1),X(3),X(4),X(5) *	3400
		3410
	IF (KURVE.EQ.2) GO TO 540	3420
		3430
	THE PRODUCT FUNCTION.	3440
		3450
	IF (LIMIT.EQ.2) GO TO 299	3460
	DO 505 I=1,M	3470
	J=I+M	3480
	K=J+M	3490
	L=K+M	3500
	XPK=ABS(XP(K))	3510
	XPL=ABS(XP(L))	3520
	IF (XPL.LE.1.0) GO TO 500	3530
	XPL=1.0	3540
	IF (MLIST.LT.3) GO TO 500	3550
	WRITE (IPRNT,427) XP(J)	3560
500	IF (XPK.LE.2.0) GO TO 501	3570
	XPK=2.0	3580
	IF (MLIST.LT.3) GO TO 506	3590
	WRITE (IPRNT,427) XP(J)	3600
	GO TO 506	3610
501	IF (XPK.GT.0.03) GO TO 506	3620
	IF (XPL.GT.0.0333) GO TO 506	3630
	XPL=0.0333	3640
	IF (MLIST.LT.3) GO TO 506	3650
	WRITE (IPRNT,428) XP(J)	3660
506	IF (XP(K).LT.0.0) GO TO 503	3670
	XP(K)=XPK	3680
	GO TO 507	3690
503	XP(K)=-XPK	3700
507	IF (XP(L).LT.0.0) GO TO 504	3710
	XP(L)=XPL	3720
	GO TO 505	3730
504	XP(L)=-XPL	3740
505	CONTINUE	3750
	GO TO 299	3760
		3770

```

C THE SUM FUNCTION.
C
540 IF (LIMIT.EQ.1) GO TO 550
    IF (NONEG.EQ.2) GO TO 299
550 DO 556 I=1,M
    J=I+M
    K=J+M
    L=K+M
    XPI=XP(I)
    XPK=ABS(XP(K))
    XPL=ABS(XP(L))
    IF (LIMIT.EQ.2) GO TO 559
    IF (XPK.LT.2.0) GO TO 551
    XPK=2.0
    IF (MLIST.LT.3) GO TO 552
    WRITE (IPRNT,427) XP(J)
    GO TO 552
551 IF (XPK.GE.0.042) GO TO 552
    XPK=0.042
    IF (MLIST.LT.3) GO TO 552
    WRITE (IPRNT,428) XP(J)
552 IF (XP(K).LT.0.0) GO TO 553
    XP(K)=XPK
    GO TO 557
553 XP(K)=-XPK
557 IF (XP(L).LT.0.0) GO TO 554
    XP(L)=XPL
    GO TO 558
554 XP(L)=-XPL
C
558 IF (NONEG.EQ.2) GO TO 556
559 IF (XPI.GE.0.0) GO TO 555
    XP(I)=XB(I)*0.1
    IF (MLIST.LT.3) GO TO 555
    WRITE (IPRNT,429) XP(J)
555 IF (XP(L).GE.0.0) GO TO 556
    XP(L)=XB(L)*0.1
C
C NOTE THAT IF X1 OR X5 GOES NEGATIVE WE REDUCE IT TO ONE TENTH OF
C THE VALUE FOUND IN THE PREVIOUS ITERATION.
C
    IF (MLIST.LT.3) GO TO 556
    WRITE (IPRNT,430) XP(J)
556 CONTINUE
C
C ***** (FSP) SECTION *****
C
299 FSP=0.0
    JSKIP=1
    KSKIP=1
    DO 301 II=1,NP
    W=IX(II)*0.1
    CALL POINT1 (XP,PC,PG,W,AC,M,N,CAY,KURVE)
    IF (AC.GT.-2.0) GO TO 304

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```
IF (JSKIP.EQ.2) GO TO 300 4320
WRITE (IPRNT,425) 4330
JSKIP=2 4340
300 TC=7.3891 4350
GO TO 310 4360
304 IF (AC.LT.10.0) GO TO 307 4370
IF (KSKIP.EQ.2) GO TO 302 4380
KSKIP=2 4390
WRITE (IPRNT,426) 4400
302 TC=0.000045 4410
GO TO 310 4420
307 TC=EXP(-AC) 4430
310 F=Y(II)-TC 4440
301 FSP=FSP+F*F 4450
IF (FSM.LE.FSP) GO TO 303 4460
C 4470
C NOTE IF RESTRAINTS ARE APPLIED,THE PROGRAM CAN BRANCH BACK HERE ON 4480
C THE FIRST CYCLE TO REPETITIVELY OUTPUT THE ORIGINAL GUESSED 4490
C INDICES.THIS INDICATES THAT THE GUESSED INDICES (WITHOUT 4500
C RESTRAINTS) FIT BETTER THAN THE COMPUTED INDICES (WITH 4510
C RESTRAINTS). IF IT HAPPENS RERUN WITH MLIST=2 AND CHANGE THE 4520
C INPUT INDICES. 4530
C 4540
FSM=FSP 4550
DO 305 I=1,N 4560
305 XB(I)=XP(I) 4570
303 IF (FS1.LE.FSP) GO TO 306 4580
FS2=FS1 4590
P2=P1 4600
FS1=FSP 4610
P1=P 4620
GO TO 308 4630
306 IF (FS2.LE.FSP) GO TO 308 4640
P2=P 4650
FS2=FSP 4660
308 GO TO (250,309,250,309),MLIST 4670
309 WRITE (IPRNT,414) P,FSP 4680
GO TO 250 4690
311 DO 312 I=1,N 4700
C ***** TERMINAL SECTION ***** 4710
312 X(I)=XB(I) 4720
NIT=NIT+1 4730
TEST=TERM/FSM 4740
TERM=FSM 4750
IF (TEST.GE.1.002) GO TO 315 4760
WRITE (IPRNT,436) 4770
GO TO 314 4780
315 IF (NIT.LE.NI) GO TO 316 4790
WRITE (IPRNT,437) 4800
GO TO 314 4810
316 IF (GL.GE.0.0001) GO TO 317 4820
WRITE (IPRNT,438) 4830
GO TO 314 4840
317 IF (ISECS.LE.NSEC) GO TO 320 4850
```

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WRITE (IPRNT,439)
GO TO 314
320 IF (FM.GT.0.001) GO TO 200
WRITE (IPRNT,440)
314 DIS=SQRT(FSM/NP)
WRITE (IPPNT,415)
WRITE (IPRNT,419) FSM,DIS,FM,WFM
IF (KURVE.EQ.2) GO TO 318
WRITE (IPRNT,416)
DO 319 I=1,M
J=I+M
K=J+M
L=K+M
X(I)=0.43429*X(I)
IF (IDECK.EQ.1) GO TO 319
WRITE (IPCH,420) X(I),X(J),X(K),X(L)
319 WRITE (IPRNT,410) X(I),X(J),X(K),X(L)
X(N)=0.43429*X(N)
IF (IDECK.EQ.1) GO TO 322
WRITE (IPCH,434) X(N)
322 WRITE (IPRNT,413) X(N)
GO TO 328
318 WRITE (IPRNT,417)
DO 325 I=1,M
J=I+M
K=J+M
L=K+M
X(I)=0.43429*X(I)
X(L)=0.43429*X(L)
XG=X(K)*CAY
IF (IDECK.EQ.1) GO TO 325
WRITE (IPCH,421) X(I),X(J),X(K),X(L)
325 WRITE (IPRNT,406) X(I),X(J),X(K),XG,X(L)
X(N)=0.43429*X(N)
IF (IDECK.EQ.1) GO TO 327
WRITE (IPCH,435) X(N)
327 WRITE (IPRNT,422) X(N),CAY
328 WRITE (IPRNT,431)
GO TO 20

```

C
C

```

400 FORMAT ('1PITHA AND JONES. PROGRAM X (PC-116) SPECTRAL BAND FIT
1 OPTIMIZATION PROGRAM BASIC VERSION.')
```

401 FORMAT (20A4) 5280
402 FORMAT (1X,20A4) 5290
403 FORMAT (10I5) 5300
404 FORMAT (4F15.5) 5310
405 FORMAT (8(I5,I4,1X)) 5320
406 FORMAT (1X,5(6X,F15.5)) 5330
407 FORMAT (5X,2HFS,E12.4,8X,2HGL,E12.4,7X,3HWFM,F7.1,7X,2HFM,E12.4,7X 5340
1,3HNIT,I3,4X,5HISECS,I5) 5350
408 FORMAT ('0INPUT PARAMETERS.')

409 FORMAT (20X,4HDOWN,E14.6,7X,2HUP,E14.6,7X,6HCHANGE,E14.6) 5370
410 FORMAT (1X,4(6X,F15.5)) 5380
5390

411	FORMAT (1X, 'TFOUBLE WITH EVALUATION OF P,CHECK MATRIX DATA OUTPUT. 1')	5400
412	FORMAT (1X, 'TERMINATED BY TROUBLE WITH SOLUTION OF EQUATIONS.')	5410
413	FORMAT (4X, 7HALPHA =F8.5/, 'OSOLVED FOR PRODUCT, CAUCHY OF GAUSS FUN 1CTION. '/' (PUFE CAUCHY IF X(4)=0 OR PURE GAUSS IF X(3)=0)')	5420 5430
414	FORMAT (64X, 1HP, E14.6, 8X, 3HFSP, E14.6)	5440
415	FORMAT (11X, '----- 1-----'/1X, 17HOUTPUT PARAMETERS)	5450 5460
416	FORMAT ('0', 15X, 4HX (1), 17X, 4HX (2), 17X, 4HX (3), 17X, 4HX (4))	5470
417	FORMAT ('0', 15X, 4HX (1), 17X, 4HX (2), 17X, 4HX (3), 17X, 4HX (4), 17X, 4HX (5) 1)	5480 5490
418	FORMAT (4X, 7HALPHA =, F8.5, /11X, '----- 1-----')	5500 5510
419	FORMAT (18X, 3HFSP, E14.6, 7X, 3HDIS, E14.6, 7X, 2HFM, E14.6, 7X, 3HWFM, F7.1 1)	5520 5530
420	FORMAT (4F15.5, 5X, 7HPRODUCT)	5540
421	FORMAT (4F15.5, 9X, 3HSUM)	5550
422	FORMAT (4X, 7HALPHA =, F8.5/'OSOLVED FOR SUM FUNCTION WITH X4 =', F5. 12, 4H X3.)	5560 5570
423	FORMAT ('0', 19X, 2HNP, I6, 17X, 2HWB, F8.1, 13X, 2HWI, F5.1)	5580
424	FORMAT (/4X, 5HMINAD, I4, 13X, 5HMAXAD, I4, 12X, 5HADMIN, E14.6, 5X, 5HADMAX 1, E14.6/4X, 5HMINA1, I4, 1X, 5HMINA2, I4, 3X, 4HAMIN, E14.6, 3X, 5HMAXA1, I4, 23X, 5HMAXA2, I4, 3X, 4HAMAX, E14.6)	5590 5600 5610
425	FORMAT ('0THE MAXIMAL ALLOWED TRANSMITTANCE HAS BEEN EXCEEDED.')	5620
426	FORMAT ('0THE MINIMAL ALLOWED TRANSMITTANCE HAS BEEN EXCEEDED.')	5630
427	FORMAT ('0MINIMAL HALF-WIDTH FOR BAND AT', F7.1, 6H CM.-1)	5640
428	FORMAT ('0MAXIMAL HALF-WIDTH FOR BAND AT', F7.1, 6H CM.-1)	5650
429	FORMAT ('CX1 HELD POSITIVE AT', F6.1, 6H CM.-1)	5660
430	FORMAT ('OX5 HELD POSITIVE AT', F6.1, 6H CM.-1)	5670
431	FORMAT ('0FSM IS THE VALUE OF THE MINIMIZATION FUNCTION. '/' 1'ODIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEA 2N SQUARE OF THE RESIDUALS). '/' 'OPM IS THE MAXIMUM ORDINATE DIFFERE 3NCE. '/' 'OWFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE. 4')	5680 5690 5700 5710 5720 5730
432	FORMAT ('0RESTRAINTS TO HOLD X(1) AND X(5) POSITIVE HAVE BEEN APPL 1IED.')	5740 5750
433	FORMAT ('0RESTRAINTS TO HOLD THE HALF-WIDTHS BETWEEN 1 AND 50 CM.- 1-1 HAVE BEEN APPLIED.')	5760 5770
434	FORMAT (F15.5, 50X, 7HPRODUCT)	5780
435	FORMAT (F15.5, 54X, 3HSUM)	5790
436	FORMAT ('0TERMINATED BECAUSE OF SLOW CONVERGENCE. '/'	5800
437	FORMAT ('0TERMINATED BY ITERATION LIMIT. '/'	5810
438	FORMAT ('0TERMINATED BY LOW VALUE OF GL. '/'	5820
439	FORMAT ('0TERMINATED BY TIME LIMITATION. '/'	5830
440	FORMAT ('0TERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VA 1LUE. '/'	5840 5850
	END	5860

```
C
C
C *****
C
C SUBROUTINE SOPT1 (IX,IY,WB,WI,NP,IPRNT,KLENUP,IWB,IWI)
C
C SUBROUTINE SOPT CHECKS FOR ERRORS IN THE INPUT WAVENUMBER DATA.
C A LIMITED NUMBER OF WAVENUMBER SEQUENCE ERRORS ARE CORRECTED
C BUT SEQUENCE ERRORS IN EXCESS OF 160 DATA POINTS (20 CARDS)
C OR ANY OTHER TYPE OF WAVENUMBER ERROR WILL TERMINATE THE
C COMPUTATION, AS ALSO WILL A DISCREPANCY BETWEEN IWB AND THE
C STARTING WAVENUMBER.
C THE WAVENUMBER POSITIONS OF THE CORRECTIONS AND OF A TERMINATING
C ERROR ARE RECORDED.
C IF CORRECTIONS ARE MADE, CORRECTED INPUT DATA ARE LISTED IN FULL.
C IF A TERMINATING ERROR IS FOUND THE UNCORRECTED INPUT DATA ARE
C LISTED IN FULL.
C
C DIMENSION IX(2000), IY(2000), ITEMPX(160), X1(160), ITEMPY(160)
C IF (IX(1).EQ.IWB) GO TO 10
C WRITE (IPRNT,456)
C KLENUP=2
C RETURN
10 MM=1
C DO 11 I=2,NP
C IW=IWB-IWI*(I-1)
C IF (IW.EQ.IX(I)) GO TO 11
C XX=IX(I)
C TEST=(WB-0.1*XX)/WI
C NTEST=TEST+0.005
C IF (ABS(TEST-NTEST).GT.0.005) GO TO 12
C ITEMPX(MM)=IX(I)
C ITEMPY(MM)=IY(I)
C MM=MM+1
C IF (MM.GT.160) GO TO 13
11 CONTINUE
C IF (MM.GT.1) GO TO 14
C WRITE (IPRNT,451)
15 KLENUP=1
C RETURN
12 XX1=IX(I-1)*0.1-WI
C WRITE (IPRNT,452) XX1
16 KLENUP=2
C RETURN
13 WRITE (IPRNT,453)
C WRITE (IPRNT,455) (IX(I),IY(I), I=1,NP)
C GO TO 16
14 NN=MM-1
C DO 17 MM=1,NN
C K1=1+(IWB-ITEMPX(MM))/IWI
C IX(K1)=ITEMPX(MM)
C IY(K1)=ITEMPY(MM)
17 X1(MM)=IX(K1)*0.1
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6400

WRITE (IPRNT,450) (X1(MM),MM=1,NN)	6410
WRITE (IPRNT,454) (IX(I),IY(I),I=1,NP)	6420
GO TO 15	6430
450 FORMAT ('0WAVENUMBER CORRECTIONS AT',/ ,12(2X,F6.1,2X))	6440
451 FORMAT ('0WAVENUMBER SEQUENCE IS CORRECT.')	6450
452 FORMAT ('0TERMINATED BY ERROR AT',F6.1,6H CM.-1)	6460
453 FORMAT ('0TERMINATED BY MULTIPLE WAVENUMBER SEQUENCE EPRORS.')	6470
454 FORMAT ('0REARRANGED INPUT.',/ ,9(4X,2I5))	6480
455 FORMAT ('0UNCORRECTED INPUT.',/ ,9(4X,2I5))	6490
456 FORMAT ('0TERMINATED BY AN ERROR IN THE STARTING WAVENUMBER.')	6500
END	6510

C		6520
C		6530
C	*****	6540
C		6550
	SUBROUTINE POINT1 (X,PC,PG,W,AC,M,N,CAY,KURVE)	6560
C		6570
C	SUBROUTINE POINT CALCULATES THE ORDINATES OF THE COMPUTED BAND	6580
C	ENVELOPE.	6590
	DIMENSION X(81),PC(20),PG(20)	6600
	AC=0.0	6610
	DO 10 I=1,M	6620
	J=I+M	6630
	K=J+M	6640
	L=K+M	6650
	R=W-X(J)	6660
	RSQ=R*R	6670
	PC(I)=1.0/(1.0+X(K)*X(K)*RSQ)	6680
	IF (KURVE.EQ.2) GO TO 12	6690
	PG(I)=X(L)*X(L)*RSQ	6700
	GO TO 13	6710
12	PG(I)=CAY*CAY*X(K)*X(K)*RSQ	6720
13	IF (PG(I).LT.10.0) GO TO 14	6730
	PG(I)=0.0	6740
	GO TO 16	6750
14	PG(I)=EXP(-PG(I))	6760
16	IF (KURVE.EQ.2) GO TO 17	6770
	AC= X(I)*PC(I)*PG(I)+AC	6780
	GO TO 10	6790
17	AC=X(I)*PC(I)+X(L)*PG(I)+AC	6800
10	CONTINUE	6810
	AC=AC+X(N)	6820
	RETURN	6830
	END	6840

PITHA AND JONES. PROGRAM X (PC-116) SPECTRAL BAND FIT OPTIMIZATION PROGRAM BASIC VERSION.
FEBRUARY 2ND.1968 PROGRAM X (PC-116)
FOUR BAND TEST DECK. PRODUCT FUNCTION.

INPUT PARAMETERS.

DOWN 0.100000E-01 UP 0.100000E 04 CHANGE 0.500000E 00
MP 200 WB 1000.0 WI 0.5

WAVENUMBER SEQUENCE IS CORRECT.

X(1)	X(2)	X(3)	X(4)
0.27000	968.50000	0.18000	0.12000
0.62000	957.00000	0.22000	0.18000
0.32000	941.00000	0.12000	0.12000
0.37000	918.00000	0.22000	0.12000

ALPHA = 0.02000

FS 0.2960E 01	GL 0.1623E 02	WFM 952.5	FM 0.2766E 00	NIT 0	ISECS 2
FS 0.1804E 00	GL 0.1174E 01	WFM 953.5	FM 0.9665E-01	NIT 1	ISECS 6
FS 0.8375E-02	GL 0.2064E 00	WFM 957.5	FM 0.2904E-01	NIT 2	ISECS 9
FS 0.3347E-04	GL 0.1325E-01	WFM 952.0	FM 0.1428E-02	NIT 3	ISECS 13
FS 0.1748E-04	GL 0.2013E-03	WFM 969.5	FM 0.7316E-03	NIT 4	ISECS 17

TERMINATED BECAUSE OF SLOW CONVERGENCE.

OUTPUT PARAMETERS

FSM 0.174846E-04 DIS 0.295674E-03 FM 0.731587E-03 WFM 969.5

X(1)	X(2)	X(3)	X(4)
0.29972	969.99951	0.19925	0.10054
0.59947	954.99902	0.20020	0.19981
0.29993	939.99756	0.09980	0.10013
0.39994	920.00098	0.20006	0.09998

ALPHA = 0.05004

SOLVED FOR PRODUCT, CAUCHY OF GAUSS FUNCTION.
(PURE CAUCHY IF X(4)=0 OR PURE GAUSS IF X(3)=0)

FSM IS THE VALUE OF THE MINIMIZATION FUNCTION.

DIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEAN SQUARE OF THE RESIDUALS).

FM IS THE MAXIMUM ORDINATE DIFFERENCE.

WFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE.

PITHA AND JONES. PROGRAM X (PC-116) SPECTRAL BAND FIT OPTIMIZATION PROGRAM BASIC VERSION.

FEBRUARY 2ND. 1968 PROGRAM X (PC-116) SUM FUNCTION CAY = 0.8
FOUR BAND TEST DECK.

INPUT PARAMETERS. DOWN 0.100000E-01 UP 0.100000E 04 CHANGE 0.500000E 00
NP 200 WB 1000.0 WI 0.5

WAVENUMBER SEQUENCE IS CORRECT.

X(1)	X(2)	X(3)	X(4)	X(5)
0.18000	968.00000	0.18000	0.14400	0.11000
0.37000	953.00000	0.22000	0.17600	0.22000
0.10000	942.00000	0.11000	0.08800	0.18000
0.26000	919.00000	0.21000	0.16800	0.16000

ALPHA = 0.02000

FS 0.1341E 01	GL 0.1568E 02	WFM 927.5	FM 0.1469E 00	NIT 0	ISECS 2
FS 0.3667E-01	GL 0.6070E 00	WFM 956.5	FM 0.3637E-01	NIT 1	ISECS 6
FS 0.2021E-02	GL 0.1412E 00	WFM 968.0	FM 0.8336E-02	NIT 2	ISECS 10
FS 0.2904E-04	GL 0.3383E-01	WFM 985.5	FM 0.1129E-02	NIT 3	ISECS 13
FS 0.1548E-04	GL 0.3633E-02	WFM 985.5	FM 0.8870E-03	NIT 4	ISECS 17

TERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VALUE.

OUTPUT PARAMETERS

FSM 0.153626E-04 DIS 0.277151E-03 FM 0.887036E-03 WFM 985.5

X(1)	X(2)	X(3)	X(4)	X(5)
0.20042	970.00488	0.20018	0.16015	0.09910
0.40776	954.95878	0.19969	0.15975	0.19399
0.09552	939.97925	0.10035	0.08028	0.20338
0.25119	920.00195	0.19965	0.15972	0.14941

ALPHA = 0.04997

SOLVED FOR SUM FUNCTION WITH X4 = 0.80 X3.

FSM IS THE VALUE OF THE MINIMIZATION FUNCTION.

DIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEAN SQUARE OF THE RESIDUALS).

FM IS THE MAXIMUM ORDINATE DIFFERENCE.

WFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE.

PROGRAM XI

PROGRAM XI

Band Fit Optimization Program with Moving Subspace

(PC-117)

This program was developed to deal with long sections of spectra. It will probably prove more efficient and economic in computer time than the Basic Version if the number of bands exceeds about twelve, but this has not been systematically examined. When fitting long sections of spectra it is our current practice to break the curve into units of 8 to 12 bands and optimize the sections separately using the Basic Version. The complete curve is then processed through the Multiplet Version using the output indices from the sectionally optimized computations as input indices. Such a "trimmer run" effectively smooths the break points. The program described here is dimensioned for a maximum of 20 bands and 2000 data points.

Equation [6] may be rewritten

$$TC_{(W)} = EXP - \left[\sum_{I=1}^{I=K} \psi_I(\underline{X}, W) + \left\{ X_{(N)} + \sum_{I=K+1}^{I=K+MULT} \psi_I(\underline{X}, W) \right\} + \sum_{I=K+MULT+1}^{I=M} \psi_I(\underline{X}, W) \right] \quad [33]$$

where

$$\psi_I(\underline{X}, W) = X_{(I)} (1 + X_{(I+2M)}^2 (W - X_{(I+M)})^2)^{-1} \cdot EXP - \left[X_{(I+3M)}^2 (W - X_{(I+M)})^2 \right] \quad [34]$$

Only the "active subspace" section of the X vector within the braces is optimized. As the program is written, this consists of the indices of from two to five consecutive bands together with the baseline variable α . The number of bands in the variable subspace is defined by MULT. The program allows for two iterations within each defined subspace. This number is controlled by the computed GO TO statement following statement 312; it can easily be changed within the program. Having completed the required number of cycles, the subspace shifts by MULT-1 bands so that the terminal band of one subject is carried

as the leading band of the next subset. This process continues until all the bands have been adjusted and the cycle then recommences.

The version of the program published here operates only on the product function; the facility to restrict the half-band widths within the range $1-50 \text{ cm.}^{-1}$ under the control of $\text{LIMIT}=1$ is retained, but the NONEG restraint on negative peak heights is not needed.

A multiplet version of the unrestrained sum function is provided in Program XVIII in Bulletin 13.

A. The Input Data

- Cards 1 and 2 are the same as for the Basic Version (p. 11).
- Card 3 carries nine fixed point instructions in format 9I5; these are consecutively NDATA , IDECK , NP , M , NSEC , NI , MLIST , MULT , LIMIT . The number of bands in the active subspace (range 2-5) is MULT and the other instructions are the same as for the Basic Version (p. 11).
- Card 4 carries the two floating point instructions WB and WI in format 2F15.5 (p. 12).
- Card 5 carries the floating point instructions for DOWN , UP and CHANGE in format 3F15.5 (p. 12).
- Card Deck 6 is the main input data deck carrying the NP experimental data points.
- Card Deck 7 is the deck of M cards carrying the 4M input band indices (p. 13).
- Card 8 is the input value of the baseline constant α (p. 13).

B. Description of the Multiplet Program

The number of variables in the active subspace, NMULT , is evaluated in the Input Section. The complete set of input indices is read into the array $\text{XS}(\text{I})$. N2 and N3 are the index numbers of the initial and terminal bands of the active subspace and ICY is the number of the iteration within the given operational subspace. This may be zero, one or two, under the control of the computed GO TO statement following statement 312.

The major modification from the Basic Version occurs in the Activation Section. This provides for the selection and exchange of the bands in the active subspace. In the first part, ending at statement 180, the values of N2 and N3 are set; N3 is checked against M to determine when a complete cycle has been completed, and in the terminating sequence of the cycle N3 is adjusted to equal M, retaining an increased overlap with the preceding subspace, should this be necessary.

In the DO loop following statement 181, the arrays X(I) and XB(I) of the active subspace are filled from XS(I), and the background index α is added, all ordinate indices have previously been transposed to Napierian absorbance units. In the large DO loop which begins shortly after statement 184, the ordinate contributions from the bands lying outside the active subspace are computed and stored in the array YS(II). They are introduced as needed in Subroutine POINT (X). It should be noted that within the wavenumber range of the active subspace these comprise a wing correction.

The remainder of the program follows that of the Basic Version closely. In the (G,AQ,F) Section, the G vector is calculated along with the elements of the B matrix and of the values of FS for the region within the active subspace. FM and WFM are evaluated over the complete spectrum; a small change in the FORTRAN notation is the replacement of G(I) by PRD(I) for the gradient vector. After the first optimization in a given subspace, the improved values for the indices are transferred to the XB(I) array at statement 312 and the next iteration is initiated. After the second optimization the improved values are transferred to the main array of indices (XS(I)) in the DO loop beginning at statement 330.

The same tests for termination are applied as for the Basic Version, with the exception of the TERM/FSM convergence test which is omitted. The printout lists the active subspace ranges for each iteration cycle so that the regions of the spectrum most sensitive to the optimization process are readily identified. When setting up the program it should be noted that the number of permitted iterations (NI) relates to the total number of iterations, calculated as two for each active subspace for each cycle through the spectrum.

This program calls the library subroutines SETCLK and RDCLK which are discussed in Bulletin 11. If these are not available appropriate alterations have to be made to the program.

The four band test data set (Figure 1) is used with the bands taken two at a time (MULT=2).

C		520
C	NSEC IS THE MAXIMUM PERMITTED COMPUTATION TIME IN SECONDS.	530
C		540
C	NI IS THE MAXIMUM NUMBER OF PERMITTED ITERATIONS.	550
C		560
C	MLIST CONTROLS THE AMOUNT OF INFORMATION REPORTED ABOUT THE	570
C	PROGRESS OF THE COMPUTATION.	580
C		590
C	USE MLIST=1 FOR MINIMAL PROGRESS REPORT AND FINAL OUTPUT ONLY	600
C	USE MLIST=2 FOR ADDITIONAL INFOPMATION ON THE EXTREME VALUES	610
C	OF THE B MATRIX ELEMENTS DURING EACH ITERATION.	620
C	USE MLIST=3 TO PRINT RESTRAINTS APPLIED BY LIMIT.	630
C	USE MLIST=4 FOR COMBINATION OF MLIST=2 + MLIST=3.	640
C		650
C	USE LIMIT=1 TO RESTRICT THE HALF-WIDTHS OF THE COMPONENT BANDS	660
C	WITHIN THE RANGE 1-50 CM.-1	670
C	IF LIMIT=2 NO RESTRICTION TO THE HALF-BAND WIDTH IS APPLIED.	680
C		690
C	MULT IS THE NUMBER OF BANDS IN THE VARIABLE SUBSPACE (MAXIMUM 5)	700
C		710
C	READ (IRD,404) WB,WI	720
C		730
C	WB AND WI ARE THE STARTING WAVENUMBER AND THE WAVENUMBER ENCODING	740
C	INTERVAL IN CM.-1 BY CONVENTION WI IS POSITIVE FOR A	750
C	DIMINISHING WAVENUMBER SEQUENCE.	760
C		770
C	IF (IDECK.EQ.1) GO TO 12	780
C	WRITE (IPCH,401) HEAD1	790
C	WRITE (IPCH,401) HEAD2	800
C	12 WRITE (IPRNT,402) HEAD1	810
C	WRITE (IPRNT,402) HEAD2	820
C	WRITE (IPRNT,408)	830
C	READ (IRD,404) DOWN,UP,CHANGE	840
C	WRITE (IPRNT,409) DOWN,UP,CHANGE	850
C		860
C	DOWN,UP AND CHANGE REGULATE SEARCH FOR THE OPTIMAL DAMPING FACTOR.	870
C	RECOMMENDED TRIAL VALUES ARE DOWN = 0.01 UP = 1000.0 CHANGE =0.5	880
C		890
C		900
C	IF (LIMIT.EQ.2) GO TO 15	910
C	IF (MLIST.LT.3) WRITE (IPFNT,430)	920
C	15 READ (IRD,405) (IX(I),IY(I),I=1,NP)	930
C	WRITE (IPRNT,423) NP,WB,WI	940
C	IWB=WB*10.0+0.5	950
C	IWI=WI*10.0+0.5	960
C	CALL SORT (IX,IY,WB,WI,NP,IPRNT,KLENUP,IWB,IWI)	970
C	IF (KLENUP.EQ.1) GO TO 30	980
C	20 IF (NDATA.EQ.2) GO TO 11	990
C	STOP	1000
C	30 DO 31 I=1,NP	1010
C	31 Y(I)=IY(I)*0.001	1020
C		1030
C	***** INPUT SECTION *****	1040
C		1050
C	CALL SETCLK	

	X (II) =XS (I)	1600
	XB (II) =X (II)	1610
	IPC=I+M	1620
	X (JJ) =XS (IPC)	1630
	XB (JJ) =X (JJ)	1640
	IPC=IPC+M	1650
	X (KK) =XS (IPC)	1660
	XB (KK) =X (KK)	1670
	IPC=IPC+M	1680
	X (LL) =XS (IPC)	1690
184	XB (LL) =X (LL)	1700
	X (NMULT) =XS (N)	1710
	XB (NMULT) =X (NMULT)	1720
	DO 185 II=1, NP	1730
	W=IX (II) *0.1	1740
	YS (II) =0.0	1750
	IF (IADBL.EQ.2) GO TO 187	1760
	IPO=N2-1	1770
	DO 188 I=1, IPO	1780
	IPC=I+M	1790
	R=W-XS (IPC)	1800
	RSQ=R*R	1810
	IPC=IPC+M+M	1820
	PGS=XS (IPC) *XS (IPC) *RSQ	1830
	IF (PGS.GE.10.0) GO TO 188	1840
	IPC=IPC-M	1850
	PGL=XS (IPC) *XS (IPC) *RSQ	1860
	IF (PGL.GE.10000.0) GO TO 188	1870
	YS (II) =YS (II) +XS (I) / (1.+PGL) *EXP (-PGS)	1880
188	CONTINUE	1890
	IF (IADBL.EQ.1) GO TO 185	1900
187	IPO=N3+1	1910
	DO 189 I=IPO, M	1920
	IPC=I+M	1930
	R=W-XS (IPC)	1940
	RSQ=R*R	1950
	IPC=IPC+M+M	1960
	PGS=XS (IPC) *XS (IPC) *RSQ	1970
	IF (PGS.GE.10.0) GO TO 189	1980
	IPC=IPC-M	1990
	PGL=XS (IPC) *XS (IPC) *RSQ	2000
	IF (PGL.GE.10000.0) GO TO 189	2010
	YS (II) =YS (II) +XS (I) / (1.0+PGL) *EXP (-PGS)	2020
189	CONTINUE	2030
185	CONTINUE	2040
	***** (G, AQ, F) SECTION *****	2050
		2060
200	DO 201 I=1, NMULT	2070
201	PRD (I) =0.0	2080
	DO 202 I=1, NAL	2090
202	AQ (I) =0.0	2100
	ICY=ICY+1	2110
	FS=0.0	2120
		2130

C
C
C

FM=0.0	2140
FS1=1.0E10	2150
FS2=1.0E10	2160
P1L=P1	2170
IT=1	2180
DO 218 II=1,NP	2190
W=IX(II)*0.1	2200
CALL POINT (X,MULT,NMULT,II,W,AC,PC,PG,YS)	2210
TC=EXP(-AC)	2220
F=Y(II)-TC	2230
FA=ABS(F)	2240
IF (FM.GE.FA) GO TO 206	2250
FM=FA	2260
WFM=W	2270
206 FS=FS+F*F	2280
DO 209 I=1,MULT	2290
J=I+MULT	2300
K=J+MULT	2310
L=K+MULT	2320
AM(I)=TC*PG(I)*PC(I)	2330
R=W-X(J)	2340
SP=2.0*AM(I)*X(I)*R	2350
AM(J)=SP*(X(L)*X(L)+X(K)*X(K)*PC(I))	2360
AM(K)=-SP*R*X(K)*PC(I)	2370
209 AM(L)=-SP*R*X(L)	2380
AM(NMULT)=TC	2390
IM=0	2400
DO 218 I=1,NMULT	2410
AMI=AM(I)	2420
PRD(I)=PRD(I)+AMI*F	2430
DO 218 IJ=I,NMULT	2440
IM=IM+1	2450
218 AQ(IM)=AQ(IM)+AMI*AM(IJ)	2460
FSM=FS	2470
IM=0	2480
DO 219 I=1,NMULT	2490
DO 219 IJ=I,NMULT	2500
IM=IM+1	2510
219 A(I,IJ)=AQ(IM)	2520
ADMIN=1.0E+10	2530
ADMAX=-1.0E+10	2540
DO 227 I=1,NMULT	2550
GO TO (224,220,224,220),MLIST	2560
220 IF (A(I,I).GE.ADMIN) GO TO 221	2570
ADMIN=A(I,I)	2580
MINAD=I	2590
221 IF (ADMAX.GE.A(I,I)) GO TO 224	2600
ADMAX=A(I,I)	2610
MAXAD=I	2620
224 IF (A(I,I).GT.1.0E-10) GO TO 226	2630
DIA(I)=0.0	2640
GO TO 227	2650
226 DIA(I)=1.0/(SQRT(A(I,I)))	2660
227 GAST(I)=PRD(I)*DIA(I)	2670

```

IM=0
AMIN=1.0E+10
AMAX=-1.0E-10
DO 228 I=1,NMULT
DIAI=DIA(I)
DO 228 IJ=I,NMULT
IM=IM+1
AQ(IM)=A(I,IJ)*DIAI*DIA(IJ)
GO TO (228,229,228,229),MLIST
229 IF (I.EQ.IJ) GO TO 228
IF (AQ(IM).GE.AMIN) GO TO 231
AMIN=AQ(IM)
MINA1=I
MINA2=IJ
231 IF (AMAX.GE.AQ(IM)) GO TO 228
AMAX=AQ(IM)
MAXA1=I
MAXA2=IJ
228 CONTINUE
GL=0.0
DO 233 I=1,NMULT
PRDI=PRD(I)
233 GL=GL+PRDI*PRDI
SM=-2.0*GL
GL=SQRT(GL)
C
C SM HAS BEEN APPROXIMATED. SEE COMMENT WRITTEN INTO PROGRAM X.
C
CALL RDCLK (TIME)
C
RDCLK IS A TIMING SUBROUTINE.
C
ISECS=TIME+0.5
WRITE (IPRNT,407) FS,GL,WFM,FM,NIT,N2,N3,ISECS
C
C ***** MATRIX DATA OUTPUT SECTION *****
C
GO TO (249,248,249,248),MLIST
248 WRITE (IPRNT,424) MINAD,MAXAD,ADMIN,ADMAX,MINA1,MINA2,AMIN,MAXA1,
1MAXA2,AMAX
C
C ***** (P,INVEPT,XP) SECTION *****
C
249 ISKIP=1
250 IM=0
DO 251 I=1,NMULT
DO 251 IJ=I,NMULT
IM=IM+1
AQIM=AQ(IM)
A(I,IJ)=AQIM
251 A(IJ,I)=AQIM
GO TO (260,261,262,263,311),IT
260 P=P1L
GO TO 265

```

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3200
3210

261	IF (FS.LE.FS1) GO TO 266	3220
	P=P1L*DCWN	3230
	GO TO 265	3240
266	P=P1L*UP	3250
	GO TO 265	3260
262	P=P1*CHANGE	3270
	GO TO 265	3280
263	X3=1.0/P1	3290
	X4=1.0/P2	3300
	DET=X3*X3*X4*X4-X3*X3*X3*X4*X4	3310
	IF (DET.EQ.0.0) GO TO 269	3320
	AP1=X3*X3*(FS2-FS-SM*X4)	3330
	AP2=X4*X4*(FS1-FS-SM*X3)	3340
	AI=6.0*(AP1-AP2)/DET	3350
	BI=2.0*(X4*AP2-X3*AP1)/DET	3360
	DET=BI*BI-2.0*AI*SM	3370
	IF (DET) 269,279,270	3380
270	DET=SQRT (DET)	3390
279	IF (AI.EQ.0.0) GO TO 269	3400
	X3=(-BI+DET)/AI	3410
	X4=(-BI-DET)/AI	3420
	IF (X3.LE.0.0) GO TO 272	3430
	IF (X4.LE.0.0) GO TO 275	3440
	IF (X4.LE.X3) GO TO 274	3450
275	P=1.0/X3	3460
	GO TO 265	3470
272	IF (X4.LE.0.0) GO TO 269	3480
274	P=1.0/X4	3490
	GO TO 265	3500
269	P=10000.0	3510
271	WRITE (IPRNT,411)	3520
265	IT=IT+1	3530
	DO 278 I=1,NMULT	3540
	A(I,I)=A(I,I)+P	3550
278	A(I,N1MULT)=-GAST(I)	3560
	DO 282 I=1,NMULT	3570
	AII=A(I,I)	3580
	IF (AII.EQ.0.0) GO TO 284	3590
	PIV=1.0/AII	3600
	DO 281 J=I,N1MULT	3610
281	A(I,J)=PIV*A(I,J)	3620
	DO 282 K=1,NMULT	3630
	IF (I.EQ.K) GO TO 282	3640
	Q=A(K,I)	3650
	DO 280 J=I,N1MULT	3660
280	A(K,J)=A(K,J)-Q*A(I,J)	3670
282	CONTINUE	3680
	GO TO 286	3690
284	IF (ISKIP.EQ.2) GO TO 285	3700
	ISKIP=2	3710
	PIL=100.0	3720
	IT=1	3730
	GO TO 250	3740
285	WRITE (IPENT,412)	3750

```
      ISKIP=1
      GO TO 314
286 DO 288 I=1, NMULT
288 XP(I)=X(I)+A(I, NMULT)*DIA(I)
C
C ***** BOUNDARY CONDITIONS TO LIMIT HALF-BAND WIDTH *****
C
      IF (LIMIT.EQ.2) GO TO 298
      DO 505 I=1, MULT
      J=I+MULT
      K=J+MULT
      L=K+MULT
      XPK=ABS(XP(K))
      XPL=ABS(XP(L))
      IF (XPL.LE.1.0) GO TO 500
      XPL=1.0
      IF (MLIST.LT.3) GO TO 500
      WRITE (IPRNT,427) XP(J)
500 IF (XPK.LE.2.0) GO TO 501
      XPK=2.0
      IF (MLIST.LT.3) GO TO 506
      WRITE (IPRNT,427) XP(J)
      GO TO 506
501 IF (XPK.GT.0.03) GO TO 506
      IF (XPL.GT.0.0333) GO TO 506
      XPL=0.0333
      IF (MLIST.LT.3) GO TO 506
      WRITE (IPRNT,428) XP(J)
506 IF (XP(K).LT.0.0) GO TO 503
      XP(K)=XPK
      GO TO 507
503 XP(K)=-XPK
507 IF (XP(L).LT.0.0) GO TO 504
      XP(L)=XPL
      GO TO 505
504 XP(L)=-XPL
505 CONTINUE
      GO TO 298
C
C ***** (FSP) SECTION *****
C
298 FSP=0.0
      JSKIP=1
      KSKIP=1
      DO 301 II=1, NP
      W=IX(II)*0.1
      CALL POINT (XP, MULT, NMULT, II, W, AC, PC, PG, YS)
      IF (AC.GT.-2.0) GO TO 304
      IF (JSKIP.EQ.2) GO TO 300
      WRITE (IPRNT,425)
      JSKIP=2
300 TC=7.3891
      GO TO 310
304 IF (AC.LT.10.C) GO TO 307
```

IF (KSKIP.EQ.2) GO TO 302	4300
WRITE (IPRNT,426)	4310
KSKIP=2	4320
302 TC=0.000045	4330
GO TO 310	4340
307 TC=EXP(-AC)	4350
310 F=Y(II)-TC	4360
301 FSP=FSP+F*F	4370
IF (FSM.LE.FSP) GO TO 303	4380
FSM=FSP	4390
DO 305 I=1,NMULT	4400
305 XB(I)=XP(I)	4410
303 IF (FS1.LE.FSP) GO TO 306	4420
FS2=FS1	4430
P2=P1	4440
FS1=FSP	4450
P1=P	4460
GO TO 308	4470
306 IF (FS2.LE.FSP) GO TO 308	4480
P2=P	4490
FS2=FSP	4500
308 GO TO (250,309,250,309),MLIST	4510
309 WRITE (IPRNT,414) F,FSP	4520
GO TO 250	4530
311 DO 312 I=1,NMULT	4540
312 X(I)=XB(I)	4550
GO TO (200,330),ICY	4560
C ICY CONTROLS THE NUMBER OF ITERATIONS WITHIN EACH SUBSPACE.	4570
C THE ABOVE STATEMENT FIXES THIS AT TWO.	4580
C FOR THREE CYCLES USE GO TO (200,200,330),ICY	4590
C	4600
C	4610
C	4620
330 II=0	4630
DO 331 I=N2,N3	4640
II=II+1	4650
J=I+M	4660
K=J+M	4670
L=K+M	4680
XS(I)=XB(II)	4690
IPC=II*MULT	4700
XS(J)=XB(IPC)	4710
IPC=IPC+MULT	4720
XS(K)=XB(IPC)	4730
IPC=IPC+MULT	4740
331 XS(L)=XB(IPC)	4750
C ***** TERMINAL SECTION *****	4760
C	4770
C	4780
C	4790
XS(N)=XB(NMULT)	4800
NII=NII+1	4810
IF (NII.LT.NI) GO TO 315	4820
WRITE (IPRNT,432)	4830
GO TO 314	
315 IF (GL.GT.0.00001) GO TO 316	

```

WRITE (IPRNT,433)
GO TO 314
316 IF (ISECS.LE.NSEC) GO TO 317
WRITE (IPRNT,434)
GO TO 314
317 IF (FM.GT.0.001) GO TO 176
WRITE (IPRNT,435)
314 DIS=SQRT(FSM/NP)
WRITE (IPRNT,415)
WRITE (IPPNT,419) FSM,DIS,FM,WFM
WRITE (IPRNT,416)
DO 319 I=1,M
J=I+M
K=J+M
L=K+M
XS(I)=0.43429*XS(I)
IF (IDECK.EQ.1) GO TO 319
WRITE (IPCH,404) XS(I),XS(J),XS(K),XS(I)
319 WRITE (IPRNT,410) XS(I),XS(J),XS(K),XS(L)
XS(N)=0.43429*XS(N)
IF (IDECK.EQ.1) GO TO 322
WRITE (IPCH,404) XS(N)
322 WRITE (IPRNT,413) XS(N)
WRITE (IPRNT,429)
GO TO 20

C
C
400 FORMAT ('1PITHA AND JONES. PROGRAM XI (PC-117) SPECTRAL BAND FIT
1 OPTIMIZATION PROGRAM,VERSION WITH MOVING SUBSPACE. '/')
401 FOEMAT (20A4)
402 FORMAT (1X,20A4)
403 FORMAT (9I5)
404 FORMAT (4F15.5)
405 FORMAT (8(I5,I4,1X))
407 FORMAT (3X,2HFS,E12.4,5X,2HGL,E12.4,5X,3HWFM,F7.1,5X,2HFM,E12.4,5X
1,3HNIT,I3,4X,15HBANDS ADJUSTED ,I3,3H TO,I3,5X,5HISECS,I5)
408 FORMAT ('0INPUT PARAMETERS.')
409 FORMAT (20X,4HDOWN,E14.6,7X,2HUP,E14.6,7X,6HCHANGE,F14.6)
410 FORMAT (1X,4(6X,F15.5))
411 FORMAT (1X,'TROUBLE WITH EVALUATION OF P,CHECK MATRIX DATA OUTPUT.
1')
412 FOEMAT (1X,'TERMINATED BY TROUBLE WITH SOLUTION OF EQUATIONS. ')
413 FORMAT (4X,7HALPHA =F8.5/, '0SOLVED FOR PRODUCT,CAUCHY OR GAUSS FUN
1CTION. '/' (PURE CAUCHY IF X(4)=0 OR PURE GAUSS IF X(3)=0) ')
414 FORMAT (64X,1HP,E14.6,8X,3HFSP,E14.6)
415 FORMAT (11X, '-----
1-----')
416 FORMAT ('0',15X,4HX(1),17X,4HX(2),17X,4HX(3),17X,4HX(4))
418 FORMAT (4X,7HALPHA =,F8.5,/,11X,'-----
1-----')
419 FORMAT (18X,3HFSM,E14.6,7X,3HDIS,E14.6,7X,2HFM,E14.6,7X,3HWFM,F7.1
1)
423 FORMAT ('0',19X,2HNIP,I6,17X,2HWB,F8.1,13X,2HWI,F5.1)
424 FORMAT (4X,5HMINAD,I4,13X,5HMAXAD,I4,12X,5HADMIN,E14.6,5X,5HADMAX,

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1E14.6/4X,5HMINA1,I4,1X,5HMINA2,I4,3X,4HAMIN,E14.6,3X,5HMAXA1,I4, 5380
23X,5HMAXA2,I4,3X,4HAMAX,E14.6) 5390
425 FOFMAT ('OTHE MAXIMAL ALLOWED TRANSMITTANCE HAS BEEN EXCEEDED.') 5400
426 FOFMAT ('OTHE MINIMAL ALLOWED TRANSMITTANCE HAS BEEN EXCEEDED.') 5410
427 FOFMAT ('OMINIMAL HALF-WIDTH FOR BAND AT',F7.1,6H CM.-1) 5420
428 FOFMAT ('OMAXIMAL HALF-WIDTH FOR BAND AT',F7.1,6H CM.-1) 5430
429 FOFMAT ('OFSM IS THE VALUE OF THE MINIMIZATION FUNCTION.'//, 5440
1'ODIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEA 5450
2N SQUARE OF THE RESIDUALS).'//,'OPM IS THE MAXIMUM OFDINATE DIFFERE 5460
3NCE.'//,'OWFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE. 5470
4') 5480
430 FOFMAT ('OPESTRAINTS TO HOLD THE HALF-WIDTHS BETWEEN 1 AND 50 CM.- 5490
1-1 HAVE BEEN APPLIED.') 5500
432 FOFMAT ('CTERMINATED BY ITERATION LIMIT.'//) 5510
433 FOFMAT ('OTERMINATED BY LOW VALUE OF GI.'//) 5520
434 FOFMAT ('OTERMINATED BY TIME LIMITATION.'//) 5530
435 FOFMAT ('OTERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VA 5540
1LUE.'//) 5550
END 5560
```

```
C
C *****
C
C SUBROUTINE SORT (IX,IY,WB,WI,NP,IPRNT,KLENUP,IWB,IWI)
C
C SUBROUTINE SORT CHECKS FOR ERRORS IN THE INPUT WAVENUMBER DATA.
C A LIMITED NUMBER OF WAVENUMBER SEQUFNCE ERRORS ARE CORRECTED
C BUT SEQUENCE ERRORS IN EXCESS OF 160 DATA POINTS (20 CARDS)
C OR ANY OTHER TYPE OF WAVFNUMBER ERROR WILL TERMINATE THE
C COMPUTATION,AS ALSO WILL A DISCREPANCY BETWEEN IWB AND THE
C STARTING WAVENUMBER.
C THE WAVENUMBER POSITIONS OF THE CORRECTIONS AND OF A TERMINATING
C ERROR ARE RECORDED.
C IF CORRECTIONS ARE MADE , CORPECTED INPUT DATA ARE LISTED IN FULL.
C IF A TERMINATING ERROR IS FOUND THE UNCORRECTED INPUT DATA ARE
C LISTED IN FULL.
C
C DIMENSION IX(2000),IY(2000),ITEMPX(160),X1(160),ITEMPY(160)
C IF (IX(1).EQ.IWB) GO TO 10
C WRITE (IPRNT,456)
C KLENUP=2
C RETURN
10 MM=1
C DO 11 I=2,NP
C IW=IWB-IWI*(I-1)
C IF (IW.EQ.IX(I)) GO TO 11
C XX=IX(I)
C TEST=(WB-0.1*XX)/WI
C NTEST=TEST+0.005
C IF (ABS(TEST-NTEST).GT.0.005) GO TO 12
C ITEMPIX(MM)=IX(I)
C ITEMPIY(MM)=IY(I)
C MM=MM+1
C IF (MM.GT.160) GO TO 13
11 CONTINUE
C IF (MM.GT.1) GO TO 14
C WRITE (IPRNT,451)
15 KLENUP=1
C RETURN
12 XX1=IX(I-1)*0.1-WI
C WRITE (IPRNT,452) XX1
16 KLENUP=2
C RETURN
13 WRITE (IPRNT,453)
C WRITE (IPRNT,455) (IX(I),IY(I), I=1,NP)
C GO TO 16
14 NN=MM-1
C DO 17 MM=1,NN
C K1=1+(IWB-ITEMPIX(MM))/IWI
C IX(K1)=ITEMPIX(MM)
C IY(K1)=ITEMPIY(MM)
17 X1(MM)=IX(K1)*C.1
C WRITE (IPRNT,450) (X1(MM),MM=1,NN)
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WRITE (IPRNT,454) (IX(I),IY(I),I=1,NP) 6110
GO TO 15 6120
450 FORMAT ('0WAVENUMBER CORRECTIONS AT',12(2X,F6.1,2X)) 6130
451 FORMAT ('0WAVENUMBER SEQFNCE IS CORRECT.') 6140
452 FORMAT ('0TERMINATED BY ERROR AT',F6.1,6H CM.-1) 6150
453 FORMAT ('0TERMINATED BY MULTIPLE WAVENUMBER SEQUENCE ERRORS.') 6160
454 FORMAT ('0REAPRANGED INPUT.',11(2X,I5,I4)) 6170
455 FORMAT ('0UNCORRECTED INPUT.',11(2X,I5,I4)) 6180
456 FORMAT ('0TERMINATED BY AN ERROR IN THE STARTING WAVENUMBER.') 6190
END 6200
```

```
C
C *****
C
C SUBROUTINE POINT (X,MULT,NMULT,II,W,AC,PC,PG,YS)
C
C SUBROUTINE POINT CALCULATES THE ORDINATES OF THE COMPUTED BAND
C ENVELOPE IN UNITS OF NAPIERIAN ABSORBANCE.
C
DIMENSION X(21),PC(5),PG(5),YS(2000)
AC=0.0
DO 10 I=1,MULT
J=I+MULT
K=J+MULT
L=K+MULT
P=W-X(J)
RSQ=R*R
PC(I)=1.0/(1.0+X(K)*X(K)*RSQ)
PG(I)=X(L)*X(L)*RSQ
IF (PG(I).LT.10.0) GO TO 14
PG(I)=0.0
GO TO 16
14 PG(I)=EXP(-PG(I))
16 AC= X(I)*PC(I)*PG(I)+AC
10 CONTINUE
AC=AC+X(NMULT)+YS(II)
RETURN
END
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PITHA AND JONES. PROGRAM XI (PC-117) SPECTRAL BAND FIT OPTIMIZATION PROGRAM, VERSION WITH MOVING SUBSPACE.

FEBRUARY 5TH, 1968. SPECTRAL BAND FIT PROGRAM.
TEST RUN ON FOUR BAND TEST DECK (PRODUCT FUNCTION.) MULT=2.

INPUT PARAMETERS.

DOWN 0.100000E-01 UP 0.100000E 04 CHANGE 0.500000E 00
WP 200 WB 1000.0 WI 0.5

WAVENUMBER SEQUENCE IS CORRECT.

X(1)	X(2)	X(3)	X(4)
0.27000	968.50000	0.18000	0.12000
0.62000	957.00000	0.22000	0.18000
0.32000	941.00000	0.12000	0.12000
0.37000	918.00000	0.22000	0.12000

ALPHA = 0.02000

FS	GL	WFM	FM	NIT	BANDS	ISECS
0.2960E 01	0.1217F 02	952.5	0.2766E 00	0	ADJUSTED 1 TO 2	1
0.7930E 00	0.1442E 01	923.0	0.1917E 00	0	ADJUSTED 1 TO 2	2
0.6484E 00	0.1948E 01	923.0	0.1811E 00	1	ADJUSTED 2 TO 3	4
0.4222E 00	0.1912E 01	922.5	0.1697E 00	1	ADJUSTED 2 TO 3	5
0.4145E 00	0.2041E 01	922.5	0.1686E 00	2	ADJUSTED 3 TO 4	7
0.4980E-01	0.8782E 00	921.0	0.5031E-01	2	ADJUSTED 3 TO 4	8
0.1520E-01	0.3982E 00	976.5	0.2200E-01	3	ADJUSTED 1 TO 2	10
0.7260E-02	0.1395E 00	912.5	0.1416E-01	3	ADJUSTED 1 TO 2	11
0.6373E-02	0.1589E 00	912.5	0.1433E-01	4	ADJUSTED 2 TO 3	13
0.5634E-02	0.2422E-01	911.5	0.1395E-01	4	ADJUSTED 2 TO 3	14
0.5549E-02	0.8813E-01	929.5	0.1398E-01	5	ADJUSTED 3 TO 4	16
0.4727E-02	0.9772E-02	929.5	0.1402E-01	5	ADJUSTED 3 TO 4	17
0.4704E-02	0.1018F 00	929.5	0.1385E-01	6	ADJUSTED 1 TO 2	19
0.4346E-02	0.4659E-02	929.5	0.1242E-01	6	ADJUSTED 1 TO 2	20
0.4344E-02	0.2231E-01	929.5	0.1292E-01	7	ADJUSTED 2 TO 3	22
0.4249E-02	0.8666E-02	929.5	0.1260E-01	7	ADJUSTED 2 TO 3	23
0.4237E-02	0.9201E-01	929.5	0.1230E-01	8	ADJUSTED 3 TO 4	25
0.3757E-02	0.337E-01	929.5	0.1250E-01	8	ADJUSTED 3 TO 4	26
0.3690E-02	0.1308E 00	929.5	0.1206E-01	9	ADJUSTED 1 TO 2	28
0.3187E-02	0.1339E-02	929.5	0.1116E-01	9	ADJUSTED 1 TO 2	29
0.3187E-02	0.4029E-01	929.5	0.1116E-01	10	ADJUSTED 2 TO 3	30
0.2831E-02	0.1173E-01	911.5	0.9537E-02	10	ADJUSTED 2 TO 3	32
0.2799E-02	0.1410E 00	911.5	0.9668E-02	11	ADJUSTED 3 TO 4	33
0.1753E-02	0.2589F-01	929.5	0.7358E-02	11	ADJUSTED 3 TO 4	35
0.1703E-02	0.1456F 00	929.5	0.6972E-02	12	ADJUSTED 1 TO 2	36
0.1130E-02	0.1520E-02	935.5	0.6287E-02	12	ADJUSTED 1 TO 2	38
0.1130E-02	0.4343E-01	935.5	0.6284E-02	13	ADJUSTED 2 TO 3	39
0.8693E-03	0.1256E-01	911.5	0.5663E-02	13	ADJUSTED 2 TO 3	41
0.8650E-03	0.1043E 00	923.0	0.5736E-02	14	ADJUSTED 3 TO 4	42
0.3722E-03	0.1918E-01	952.0	0.3921E-02	14	ADJUSTED 3 TO 4	44
0.3667E-03	0.7364E-01	952.0	0.3991E-02	15	ADJUSTED 1 TO 2	45
0.2228E-03	0.3177E-03	911.5	0.2708E-02	15	ADJUSTED 1 TO 2	47
0.2229E-03	0.2690E-01	911.5	0.2707E-02	16	ADJUSTED 2 TO 3	48
0.1594E-03	0.3752E-02	911.5	0.2609E-02	16	ADJUSTED 2 TO 3	50
0.1582E-03	0.4640E-01	911.5	0.2608E-02	17	ADJUSTED 3 TO 4	51
0.6775E-04	0.4838E-02	952.0	0.1808E-02	17	ADJUSTED 3 TO 4	53
0.6751E-04	0.2774E-01	952.0	0.1809E-02	18	ADJUSTED 1 TO 2	54
0.4615E-04	0.9049E-04	911.5	0.1258E-02	18	ADJUSTED 1 TO 2	55
0.4615E-04	0.1200E-01	911.5	0.1257E-02	19	ADJUSTED 2 TO 3	57
0.3540E-04	0.7229E-03	911.5	0.1215E-02	19	ADJUSTED 2 TO 3	58
0.3540E-04	0.1686E-01	911.5	0.1215E-02	20	ADJUSTED 3 TO 4	60
0.2380F-04	0.8310E-03	952.0	0.9263E-03	20	ADJUSTED 3 TO 4	61

TERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VALUE.

OUTPUT PARAMETERS FSM 0.237940E-04 DIS 0.344920E-03 FM 0.926316E-03 WPM 952.0

X(1)	X(2)	X(3)	X(4)
0.29957	969.99731	0.19913	0.10058
0.59913	955.00244	0.19529	0.20371
0.30001	940.00171	0.10156	0.09881
0.39981	919.99707	0.19991	0.10038

ALPHA = 0.05009

SOLVED FOR PRODUCT, CAUCHY OR GAUSS FUNCTION.
(PURE CAUCHY IF X(4)=0 OR PURE GAUSS IF X(3)=0)

FSM IS THE VALUE OF THE MINIMIZATION FUNCTION.

DIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEAN SQUARE OF THE RESIDUALS).

FM IS THE MAXIMUM ORDINATE DIFFERENCE.

WPM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE.

PROGRAM XII

PROGRAM XII

Spectral Band Fit Optimization Program with Slit
Deconvolution Correction

(PC-118)

It is well known that the observed spectrum differs from the true spectrum because of systematic errors of an instrumental nature. An important type of distortion can be expressed by the integral equation

$$T(\nu)_{\text{obs}} = \frac{\int \rho(\nu, \nu') \cdot T(\nu')_{\text{true}} d\nu'}{\int \rho(\nu, \nu') d\nu'} \quad [35]$$

where $\rho(\nu, \nu')$ is the instrument function. A major factor contributing to this type of distortion is the finite spectral slit width, which is determined by the spectral slit function.

In this version of the band fit program, the spectral slit function is introduced into the computation and $TC(W)$ of equation [6] is caused to approximate $T(\nu)_{\text{true}}$ instead of $T(\nu)_{\text{obs}}$. There is an extensive literature dealing with the nature and form of the spectral slit function (16), but it is usually sufficient to approximate it with a symmetric triangular function. Computational methods of dealing with equation [35] from the basis of Program V which is described in Bulletin 11. Program V is incorporated into this version of the band fit program with very little modification; and Bulletin 11 should be consulted for a more detailed discussion of the internal logic of the slit convolution procedure than is included here.

The slit function can be introduced in two ways. If $MODE=1$, a symmetric triangular slit function is assumed, and it is necessary to supply only the spectral slit width (SSW), expressed in cm^{-1} . The program computes and normalizes the spectral slit ordinates. If $MODE=2$, the program calls for an odd number of slit ordinates (maximum 25), spaced at the wavenumber encoding interval WI . These are entered into the program from cards and permit the use of slit functions of Gaussian, trapezoidal or non-symmetric contour.

This program will fit both the product and the sum functions and will apply the same restraints to the half-band width (with $LIMIT=1$) and to the sum function ordinate sign (with $NONEG=1$) as does the Basic Version.

A. The Input Data

Cards 1 and 2 are the same as for the Basic Version.

Card 3 carries eleven fixed point instructions in format 11I5. The first ten are identical with those used with the Basic Version (p. 11) and the sequence is the same. The eleventh is MODE which determines the manner of introducing the slit function ordinates as discussed above.

Card 4 is the same as for the Basic Version (p. 12).

Card 5 is the same as for the Basic Version (p. 12).

Card 6 If operating with MODE=1 this card carries the spectral slit width in cm.^{-1} in format F15.5. If operating with MODE=2 this card carries the number of slit ordinates (KK) in format I5. KK must be an odd number.

Card Deck 7 is used ONLY WITH MODE = 2 and lists the spectral slit ordinates (which need not be normalized) in format 5F15.9. Note that an odd number of slit ordinates must be supplied, but the terminal values may be zero. It is recommended that not less than 13 ordinates be provided; the maximum number is 25.

Card Deck 8 is the main data deck carrying the NP experimental data points and corresponds to Card Deck 6 of the Basic Version (p. 13).

Card Deck 9 This is a deck of M cards, each carrying four input indices for one band in format 4F15.5. It corresponds to Card Deck 7 of the Basic Version (p. 13).

Card 10 is the terminating card carrying the baseline constant α in format F15.5 and corresponds with Card 8 of the Basic Version (p. 13).

B. Description of the Program

There are only minor changes from the Basic Version in the earlier part of the program where the data are read in. Before entering the Input Section, the slit ordinates are evaluated, normalized, and weighted for quadrature. For MODE=1 Newton-Cotes

weightings are used if the number of ordinates is less than seven-teen otherwise Simpson's Rule is applied. Simpson Rule weightings are always used with $MODE=2$. Between statements 30 and 102 a number of constants are evaluated for $MODE=1$. These include LL , the spectral slit width expressed in integral multiples of the wavenumber encoding interval (WI), and KK , the total number of slit ordinates. The normalized and weighted ordinates are stored in the array $SY(J)$. These operations are completed in the sections headed Computation of the Slit Ordinates and Slit Ordinates for Mode 2 and for Mode 1 by Simpson's Rule.

In the Input Section two new floating point arrays are created ($W(I)$ and $Y(I)$), into which the wavenumber positions and the intensity ordinates are transferred from $IX(I)$ and $IY(I)$ respectively. The $W(I)$ array is expanded at each end by LL spaces, and zeroes are entered in the corresponding spaces of the $Y(I)$ array. The need for this expansion of the wavenumber range by $m-1$ units for an m element slit function vector has been illustrated previously in a numerical example on page 927 of reference (9).

In the calculation of A , G and FS a difficulty arises because of the integral form of the function. To deal with this an array $AP(I, JJ)$ is introduced in the DO loop ending at statement 206 in the (G, AQ, F) Section. This contains the row elements of the A matrix for KK consecutive terms of the function $TC(W)$; the second index denotes the wavenumber position. Thus the elements $AP(I, LL)$ are identical with the row of the A matrix of $T(\nu)$ true for the wavenumber ν , while $AP(I, LL-1)$ is the row corresponding to the wavenumber $\nu+WI$. KK wavenumber positions are first calculated, after which, on multiplication by the $SY(I)$ elements, the row of the A matrix corresponding to $T(\nu)_{obs}$ is generated in the DO loop ending at statement 215. The same data in $AP(I, JJ)$ are used also to generate the G vector, and FS in a similar manner. It should be emphasized that it is only necessary to compute all KK wavenumber positions of $AP(I, JJ)$ separately in the initial step. $KK-1$ of them can be carried forward to the next round of computation for the succeeding values of $T(\nu)_{obs}$ by displacement of their positions, with only one new datum being introduced. These operations are all performed in the (G, AQ, F) Section and further details should be clear from comparison with the Basic Version. The computation of $TC(W)$ at statement 302 is likewise modified from that in the Basic Version in accord with the requirements of equation [35].

SUBROUTINE POINT is also modified to provide values of the transmittance ($T(I)$) and the quantities PC and PG for KK consecutive wavenumber values. As above, all KK values need only be evaluated initially; the subsequent values are obtained by increasing the subscripts by unity and computing one additional term at the low wavenumber end.

The other sections of the program resemble the Basic Version closely, and the terminating controls as well as the restraints under LIMIT=1 and NONEG=1 are the same. In the printed output for MODE 1 the normalized and weighted slit elements in the SY(J) array are recorded while in MODE 2 the raw input slit ordinates are also listed.

The Test Data for this program are the four band product and sum function curves of Fig. 1 and Fig. 2 after they have been convolved with appropriate slit functions using Program V of Bulletin 11 for this purpose. The Fig. 1 product curve is initially convolved with a symmetric triangular slit function of half width 5.0 cm.^{-1} . The Fig. 2 sum function curve is initially convolved with an asymmetric triangular slit function.

Note that this program calls for the library routines SETCLK and RDCLK which are discussed in Bulletin 11. If they are not available appropriate alterations must be made to the program.

*****	10
* SPECTRAL BAND FIT OPTIMIZATION PROGRAM	20
* WITH SLIT DECONVOLUTION CORRECTION.	35
*****	45
J. PITHA AND R. N. JONES, DIVISION OF CHEMISTRY, NATIONAL RESEARCH COUNCIL OF CANADA, SUSSEX DRIVE, OTTAWA, CANADA.	80
PROGRAM XII (PC-118) SLIT DECONVOLUTING VERSION JULY 12TH. 1967	110
THIS PROGRAM WILL FIT A CAUCHY, GAUSS, PRODUCT, OR SUM FUNCTION TO AN INFRARED ABSORPTION BAND ENVELOPE AFTER CORRECTION FOR THE SPECTRAL SLIT DISTORTION.	140
FOR THE SUM FUNCTION THE RESTRAINT THAT THE RATIO X(4)/X(3) IS CONSTANT IS APPLIED.	160
THE SUM FUNCTION REQUIRES A DIFFERENT SET OF INPUT INDEX CARDS CAERYING X(5) IN PLACE OF X(4).	180
THE PROGRAM OPERATES IN TWO MODES.	200
MODE 1. A SYMMETRICAL TRIANGULAR SLIT FUNCTION IS ASSUMED. THE NUMBER OF SLIT ORDINATES IS CALCULATED FROM THE SPECTRAL SLIT WIDTH AND THE ABSCISSAL ENCODING INTERVAL. NEWTON-COTES WEIGHTINGS ARE USED FOR QUADRATURE IF THERE ARE SEVENTEEN OR LESS SLIT ORDINATES. FOR SEVENTEEN TO TWENTY-FIVE SLIT ORDINATES QUADRATURE IS BY SIMPSON'S RULE IN THIS MODE ALL THE SLIT ORDINATES AND WEIGHTINGS ARE COMPUTED AND STORED WITHIN THE PROGRAM, ONLY THE SLIT WIDTH AND THE WAVENUMBER INTERVAL NEED BE SUPPLIED.	210
MODE 2. IN THIS MODE ASYMMETRIC AND NON-TRIANGULAR SLIT FUNCTIONS MAY ALSO BE USED. THE RAW SLIT ORDINATES ARE SUPPLIED BY CARD INPUT AND ARE NORMALIZED AND WEIGHTED IN PROGRAM USING SIMPSON'S RULE. IT IS RECOMMENDED THAT NOT LESS THAN THIRTEEN ORDINATES BE PROVIDED.	300
THIS VERSION IS DIMENSIONED FOR A MAXIMUM OF 20 BANDS, 2000 EXPERIMENTAL DATA POINTS, AND ANY ODD NUMBER OF EQUALLY SPACED SLIT ORDINATES NOT EXCEEDING TWENTY-FIVE.	350
THE SLIT ORDINATE WAVENUMBER INTERVAL MUST BE THE SAME AS THE DATA WAVENUMBER INTERVAL.	380
THE BAND INTENSITY INDICES ARE IN ABSORBANCE UNITS BUT THE COMPUTATIONS WITHIN THE PROGRAM USE NAPIERIAN LOGARITHMS.	410
THE EXPERIMENTAL DATA ARE IN UNITS OF WAVENUMBER X 10 AND TRANSMITTANCE X 1000.	430
THE INPUT WAVENUMBER SEQUENCE IS CHECKED BY SUBROUTINE SORT.	440
FOR DETAILS SEE N.R.C.C. BULLETIN NO. 12.	460
DIMENSION IX(2000), W(2000), IY(2000), Y(2000), X(81), XP(81), XB(81), 1G(81), AM(81), PC(20,25), PG(20,25), AQ(3321), A(81,82), DIA(81), 2GAST(81), AP(81,25), T(25), SY(25), HEAD1(20), HEAD2(20)	480
IRD=1	510
IPCH=2	520

	IPRNT=3	530
C		540
C		550
	11 READ (IRD,401) HEAD1	560
	READ (IRD,401) HEAD2	570
C		580
C	HEAD1 AND HEAD2 ARE HEADING CARDS.THEY MAY CARRY ANY DESIRED	590
C	INFORMATION.	600
C		610
C		620
C	USE NDATA=1 FOR PROCESSING A SINGLE DATA DECK OR THE LAST DECK OF	630
C	A SERIES AND USE NDATA=2 FOR CONSECUTIVE DATA DECKS.	640
C		650
C	USE IDECK=1 FOR PRINTED OUTPUT AND IDECK=2 FOR BOTH PRINTED AND	660
C	CARD OUTPUT.	670
C		680
C	NP IS THE NUMBER OF DATA POINTS.	690
C		700
C	M IS THE NUMBER OF CALCULATED BANDS.	710
C		720
C	USE KURVE=1 FOR THE PRODUCT FUNCTION,KURVE=2 FOR THE SUM FUNCTION.	730
C		740
C	NSEC IS THE MAXIMUM PERMITTED COMPUTATION TIME IN SECONDS.	750
C		760
C	NI IS THE MAXIMUM NUMBER OF PERMITTED ITERATIONS.	770
C	WRITE (IPRNT,400)	775
C		780
	READ (IRD,403) NDATA, IDECK, NP, M, KURVE, NSEC, NI, MLIST, LIMIT, NONEG,	790
	1MODE	800
C		810
C	MLIST CONTROLS THE AMOUNT OF INFORMATION REPORTED ABOUT THE	820
C	PROGRESS OF THE COMPUTATION.	830
C	USE MLIST=1 FOR MINIMUM PROGRESS REPORT AND FINAL OUTPUT ONLY	840
C	USE MLIST=2 FOR ADDITIONAL INFORMATION ON THE EXTREME VALUES	850
C	OF THE B MATRIX ELEMENTS DURING EACH ITERATION.	860
C	USE MLIST=3 TO PRINT RESTRAINTS APPLIED BY LIMIT AND NONEG.	870
C	USE MLIST=4 FOR COMBINATION OF MLIST=2 + MLIST=3.	880
C		890
C	USE LIMIT=1 TO RESTRICT THE HALF-WIDTHS OF THE COMPONENT BANDS	900
C	WITHIN THE RANGE 1-50 CM.-1	910
C	IF LIMIT=2 NO RESTRICTION TO THE HALF-BAND WIDTH IS APPLIED.	920
C		930
C	USE NONEG=1 WITH THE SUM FUNCTION TO RESTRICT X1 AND X5 TO ZERO	940
C	OR POSITIVE VALUES.	950
C	IF NONEG=2 NO RESTRICTION IS APPLIED ----- ALWAYS USE	960
C	NONEG=2 WITH THE PRODUCT FUNCTION.	970
C		980
C		990
	IF (KURVE.EQ.2) GO TO 13	1000
	READ (IRD,404) WB,WI	1010
	GO TO 17	1020
	13 READ (IPD,404) WB,WI,CAY	1030
C		1040
C	CAY DEFINES THE X(4)/X(3) RATIO IN THE SUM FUNCTION CALCULATIONS.	1050

```
C   VALUES OF CAY IN THE RANGE 0.6 - 0.8 ARE SUGGESTED. 1060
C
C   WB AND WI ARE THE STARTING WAVENUMBER AND THE WAVENUMBER ENCODING 1070
C   INTERVAL IN CM.-1 1080
C   BY CONVENTION WI IS POSITIVE FOR A DIMINISHING WAVENUMBER SEQUENCE 1090
C
17 IF (IDECK.EQ.1) GO TO 12 1100
   WRITE (IPCH,401) HEAD1 1120
   WRITE (IPCH,401) HEAD2 1130
12 WRITE (IPRNT,402) HEAD1 1140
   WRITE (IPRNT,402) HEAD2 1150
   WRITE (IPRNT,408) 1160
   READ (IRD,404) DOWN,UP,CHANGE 1170
C 1180
C   DOWN,UP AND CHANGE REGULATE THE SEARCH FOR OPTIMAL DAMPING FACTOR. 1190
C   RECOMMENDED TRIAL VALUES ARE DOWN = 0.01 UP = 1000.0 CHANGE = 0.5 1200
C 1210
C   WRITE (IPRNT,409) DOWN,UP,CHANGE 1220
C 1230
C   IF (MODE.EQ.2) GO TO 15 1240
14 READ (IRD,404) SSW 1250
C 1260
C   SSW IS THE SPECTRAL SLIT WIDTH IN CM.-1 1270
C 1280
C   WRITE (IPRNT,425) NP,WB,WI,SSW 1290
   GO TO 16 1300
15 READ (IRD,403) KK 1310
C 1320
C   KK IS THE NUMBER OF SLIT ORDINATES. 1330
C 1340
C 1350
   LL=(KK-1)/2 1360
   L1=LL+1 1370
   KK1=KK-1 1380
   READ (IRD,426) (SY(J),J=1, KK) 1390
C 1400
C   SY(J) ARE THE SLIT ORDINATE VALUES.THEY NEED NOT BE NORMALIZED. 1410
C   NOTE THAT A CARD LISTING KK IS ONLY NEEDED IF OPERATING IN MODE 2. 1420
C 1430
C 1440
   WRITE (IPRNT,427) 1450
   WRITE (IPRNT,428) (SY(J),J=1, KK) 1460
   WRITE (IPRNT,423) NP,WB,WI 1470
16 IF (NONEG.EQ.2) GO TO 18 1480
   IF (MLIST.LT.3) WRITE (IPRNT,439) 1490
18 IF (LIMIT.EQ.2) GO TO 19 1500
   IF (MLIST.LT.3) WRITE (IPRNT,440) 1510
19 READ (IRD,405) (IX(I),IY(I), I=1,NP) 1520
   IWB=WB*10.0+0.5 1530
   IWI=WI*10.0+0.5 1540
   CALL SORT3 (IX,IY,WB,WI,NP,IPRNT,KLENUP,IWB,IWI) 1550
   IF (KLENUP.EQ.1) GO TO 30 1560
20 UP=0.0 1570
   DOWN=0.0 1580
   CHANGE=0.0 1590
   IF (NDATA.EQ.2) GO TO 11
```

STOP

***** COMPUTATION OF THE SLIT ORDINATES *****

30 IF (MODE.EQ.2) GO TO 120

SLIT ORDINATES FOR MODE ONE BY NEWTON-COTES QUADRATURE.

P=SSW/WI

LL=P+0.5

KK=2*LL+1

L1=LL+1

KK1=KK-1

IF (KK.GT.17) GO TO 120

GO TO (102,103,104,105,106,107,108,109),LL

102 WRITE (IPRNT,429)

GO TO 20

103 KK=5

SY(1)=0.0

SY(2)=0.3333333

SY(3)=SY(2)

GO TO 110

104 KK=7

SY(1)=0.0

SY(2)=0.125

SY(3)=0.250

SY(4)=SY(3)

GO TO 110

105 KK=9

SY(1)=0.0

SY(2)=0.0888889

SY(3)=0.0666667

SY(4)=0.2666667

SY(5)=0.1555555

GO TO 110

106 KK=11

SY(1)=0.0

SY(2)=0.0520833

SY(3)=0.0694444

SY(4)=0.1041667

SY(5)=0.2083333

SY(6)=0.1319444

GO TO 110

107 KK=13

SY(1)=0.0

SY(2)=0.0428571

SY(3)=0.0107143

SY(4)=0.1619043

SY(5)=0.0214286

SY(6)=0.2142857

SY(7)=0.0976190

GO TO 110

108 KK=15

SY(1)=0.0

1600
1610
1620
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1660
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1680
1690
1700
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2100
2110
2120
2130

SY (2)=0.0295717	2140
SY (3)=0.0218750	2150
SY (4)=0.0741319	2160
SY (5)=0.0988426	2170
SY (6)=0.0546875	2180
SY (7)=0.1774305	2190
SY (8)=0.0869213	2200
GO TO 110	2210
109 KK=17	2220
SY (1)=0.0	2230
SY (2)=0.0259620	2240
SY (3)= -0.0081834	2250
SY (4)=0.1388359	2260
SY (5)= -0.0800705	2270
SY (6)=0.2313932	2280
SY (7)= -0.0245503	2290
SY (8)=0.1817284	2300
SY (9)=0.0697707	2310
110 JJ=LL+2	2320
DO 111 K1=1,LL	2330
J=JJ-2*K1	2340
SY (JJ)=SY (J)	2350
111 JJ=JJ+1	2360
WRITE (IPRNT,430)	2370
WRITE (IPRNT,428) (SY (J),J=1,KK)	2380
GO TO 150	2390
	2400
	2410
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	2450
	2460
	2470
	2480
	2490
	2500
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	2570
	2580
	2590
	2600
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	2670

C
C
C
C

*** SLIT ORDINATES FOR MODE 2 AND FOR MODE 1 BY SIMPSON RULE. ****

120 IF (KK.LT.25) GO TO 121
 WRITE (IPRNT,431)
 GO TO 20

121 IF (MODE.EQ.2) GO TO 135
 SY (1)=0.0
 S=0.0
 DO 131 J=2,L1
 S=S+1.0

131 SY (J)=S
 JJ=LL+2
 DO 123 K1=1,LL
 J=JJ-2*K1
 SY (JJ)=SY (J)

123 JJ=JJ+1

135 QR=SY (1)
 DO 124 J=2, KK1, 2
 SY (J)=SY (J) *4.0

124 QR=QR+SY (J)
 DO 125 J=3, KK1, 2
 SY (J)=SY (J) *2.0

125 QR=QR+SY (J)
 QR=QR+SY (KK)
 QR=1/QR
 DO 126 J=1, KK

126	SY (J) = SY (J) * QR	2680
	IF (MODE.EQ.2) GO TO 128	2690
	WRITE (IPRNT,432)	2700
	GO TO 130	2710
128	WRITE (IPRNT,433)	2720
130	WRITE (IPRNT,428) (SY (J) ,J=1, KK)	2730
C		2740
C	***** INPUT SECTION *****	2750
C		2760
150	CALL SETCLK	2770
C		2780
C	SETCLK IS A TIMING SUBROUTINE.	2790
C		2800
	N=4*M+1	2810
	N1=N+1	2820
	NAL=N*N1/2	2830
	NIT=0	2840
	TERM=1000.0	2850
	P1=0.1	2860
	IF (KURVE.EQ.2) GO TO 151	2870
	WRITE (IPRNT,416)	2880
	GO TO 152	2890
151	WRITE (IPRNT,417)	2900
152	DO 153 I=1, M	2910
	J=I+M	2920
	K=J+M	2930
	L=K+M	2940
	READ (IRD,404) X (I) , X (J) , X (K) , X (L)	2950
C		2960
C	X (I) , X (J) , X (K) AND X (L) ARE THE SPECTRAL INDICES FOR EACH BAND.	2970
C	IF (KURVE.EQ.2) GO TO 160	2980
	WRITE (IPRNT,410) X (I) , X (J) , X (K) , X (L)	2990
	GO TO 161	3000
160	KG=X (K) *CAY	3010
	WRITE (IPRNT,406) X (I) , X (J) , X (K) , XG, X (L)	3020
	X (L) =2.30258*X (L)	3030
161	X (I) =2.30258*X (I)	3040
153	CONTINUE	3050
	READ (IRD,404) X (N)	3060
	WRITE (IPRNT,418) X (N)	3070
	X (N) =2.30258*X (N)	3080
	DO 154 I=1, N	3090
154	XB (I) =X (I)	3100
	J1=LL	3110
	DO 155 I=1, NP	3120
	J1=J1+1	3130
	W (J1) =IX (I) *0.1	3140
155	Y (J1) =IY (I) *0.001	3150
	DO 156 I=1, LL	3160
	Y (I) =0.0	3170
156	W (I) =WB+ (L1-I) *WI	3180
	NP=NP+LL	3190
	NP1=NP+1	3200
		3210

```

NPL1=NP+LI
DO 157 I=NP1,NPL1
Y(I)=0.0
157 W(I)=WB-WI*(I-L1)
NP1=NP+15
C
***** (G,AQ,F) SECTION *****
C
200 DO 201 I=1,N
201 G(I)=0.0
DO 202 I=1,NAL
202 AQ(I)=0.0
FS=0.0
FM=0.0
FS1=1.0E10
FS2=1.0E10
P1L=P1
IT=1
203 DO 218 II=L1,NP
CALL POINT3 (X,PC,PG,T,W,II,IK,KK,KK1,L1,M,N,IPRNT,CAY,KURVE,IJ)
IF(II.EQ.L1) GO TO 204
DO 206 JJ=1,KK1
DO 206 I=1,N
206 AP(I,JJ)=AP(I,JJ+1)
204 DO 211 JJ=IJ,KK
LL1=II+JJ-L1
WP=W(LL1)
IF (KURVE.EQ.2) GO TO 210
DO 209 I=1,M
J=I+M
K=J+M
L=K+M
AP(I,JJ)=T(JJ)*PG(I,JJ)*PC(I,JJ)
R=WP-X(J)
SP=2.0*AP(I,JJ)*X(I)*R
AP(J,JJ)=SP*(X(L)*X(L)+X(K)*X(K))*PC(I,JJ)
AP(K,JJ)=-SP*R*X(K)*PC(I,JJ)
209 AP(L,JJ)=-SP*R*X(L)
GO TO 211
210 DO 212 I=1,M
J=I+M
K=J+M
L=K+M
R=WP-X(J)
AP(I,JJ)=T(JJ)*PC(I,JJ)
SS=2.0*T(JJ)*(X(I)*PC(I,JJ)*PC(I,JJ)+CAY*CAY*X(L)*PG(I,JJ))*R*X(K)
AP(J,JJ)=SS*X(K)
AP(K,JJ)=-SS*R
212 AP(L,JJ)=T(JJ)*PG(I,JJ)
211 AP(N,JJ)=T(JJ)
DO 216 I=1,N
AMI=0.0
DO 215 JJ=1,KK
215 AMI=AMI+SY(JJ)*AP(I,JJ)

```

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3700
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3740

216	AM(I)=AMI	3750
	TC=AM(N)	3760
	F=Y(II)-TC	3770
	FA=ABS(F)	3780
	I3=L1+3	3790
	I4=NP-2	3800
	IF(II.LT.I3) GO TO 220	3810
	IF(II.GT.I4) GO TO 220	3820
	IF(FM.GE.FA) GO TO 217	3830
	FM=FA	3840
	WFM=W(II)	3850
217	FS=FS+F*F	3860
220	IM=0	3870
	DO 218 I=1,N	3880
	AMI=AM(I)	3890
	G(I)=G(I)+AMI*F	3900
	DO 218 IJ=I,N	3910
	IM=IM+1	3920
218	AQ(IM)=AQ(IM)+AMI*AM(IJ)	3930
	FSM=FS	3940
	IM=0	3950
	DO 219 I=1,N	3960
	DO 219 IJ=I,N	3970
	IM=IM+1	3980
219	A(I,IJ)=AQ(IM)	3990
	ADMIN=+1.E+10	4000
	ADMAX=-1.E+10	4010
	DO 227 I=1,N	4020
	GO TO (224,222,224,222),MLIST	4030
222	IF(A(I,I).GE.ADMIN) GO TO 221	4040
	ADMIN=A(I,I)	4050
	MINAD=I	4060
221	IF(ADMAX.GE.A(I,I)) GO TO 224	4070
	ADMAX=A(I,I)	4080
	MAXAD=I	4090
224	IF(A(I,I).GT.1.0E-10) GO TO 226	4100
	DIA(I)=0.0	4110
	GO TO 227	4120
226	DIA(I)=1.0/SQRT(A(I,I))	4130
227	GAST(I)=G(I)*DIA(I)	4140
	IM=0	4150
	AMIN=1.0E+10	4160
	AMAX=-1.0E-10	4170
	DO 228 I=1,N	4180
	DIAI=DIA(I)	4190
	DO 228 IJ=I,N	4200
	IM=IM+1	4210
	AQ(IM)=A(I,IJ)*DIAI*DIA(IJ)	4220
	IF(MLIST.EQ.1) GO TO 228	4230
229	IF(I.EQ.IJ) GO TO 228	4240
	IF(AQ(IM).GE.AMIN) GO TO 231	4250
	AMIN=AQ(IM)	4260
	MINA1=I	4270
	MINA2=IJ	4280

```
231 IF (AMAX.GE.AQ(IM)) GO TO 228 4290
    AMAX=AQ(IM) 4300
    MAXA1=I 4310
    MAXA2=IJ 4320
228 CONTINUE 4330
    GL=0.0 4340
    DO 233 I=1,N 4350
    GI=G(I) 4360
233 GL=GL+GI*GI 4370
    SM=-2.0*GL 4380
    GL=SQRT(GL) 4390
C 4400
C SM HAS BEEN APPROXIMATED. SEE COMMENT WRITTEN INTO PROGRAM X. 4410
C 4420
C CALL RDCLK (TIME) 4430
C 4440
C RDCLK IS A TIMING SUBROUTINE. 4450
C 4460
C ISECS=TIME+0.5 4470
C WRITE (IPRNT,407) FS,GL,WFM,FM,NIT,ISECS 4480
C 4490
C ***** MATRIX DATA OUTPUT SECTION ***** 4500
C 4510
C GO TO (250,249,250,249),MLIST 4520
249 WRITE (IPRNT,424) MINAD,MAXAD,ADMIN,ADMAX,MINA1,MINA2,AMIN,MAXA1, 4530
    1MAXA2,AMAX 4540
C 4550
C 4560
C ***** (P,INVERT,XP) SECTION ***** 4570
C 4580
250 IM=0 4590
    DO 251 I=1,N 4600
    DO 251 IJ=I,N 4610
    IM=IM+1 4620
    AQIM=AQ(IM) 4630
    A(I,IJ)=AQIM 4640
251 A(IJ,I)=AQIM 4650
    GO TO (260,261,262,263,311),IT 4660
260 P=P1L 4670
    GO TO 265 4680
261 IF (FS.LE.FS1) GO TO 266 4690
    P=P1L*DOWN 4700
    GO TO 265 4710
266 P=P1L*UP 4720
    GO TO 265 4730
262 P=P1*CHANGE 4740
    GO TO 265 4750
263 X3=1.0/P1 4760
    X4=1.0/P2 4770
    DET=X3*X3*X4*X4*X4-X3*X3*X3*X4*X4 4780
    IF (DET.EQ.0.0) GO TO 269 4790
    AP1=X3*X3*(FS2-FS-SM*X4) 4800
    AP2=X4*X4*(FS1-FS-SM*X3) 4810
    AI=6.0*(AP1-AP2)/DET 4820
```

BI=2.0*(X4*AP2-X3*AP1)/DET	4830
DET=BI*BI-2.0*AI*SM	4840
IF (DET) 269,279,270	4850
270 DET=SQRT(DET)	4860
279 IF (AI.EQ.0.0) GO TO 269	4870
X3=(-BI+DET)/AI	4880
X4=(-BI-DET)/AI	4890
IF (X3.LE.0.0) GO TO 272	4900
IF (X4.LE.0.0) GO TO 275	4910
IF (X4.LE.X3) GO TO 274	4920
275 P=1.0/X3	4930
GO TO 265	4940
272 IF (X4.LE.0.0) GO TO 269	4950
274 P=1.0/X4	4960
GO TO 265	4970
269 P=10000.0	4980
271 WRITE (IPRNT,411)	4990
265 IT=IT+1	5000
DO 278 I=1,N	5010
A(I,I)=A(I,I)+P	5020
278 A(I,N1)=-GAST(I)	5030
DO 282 I=1,N	5040
AII=A(I,I)	5050
IF (AII.EQ.0.0) GO TO 284	5060
PIV=1.0/AII	5070
DO 281 J=I,N1	5080
281 A(I,J)=PIV*A(I,J)	5090
DO 282 K=1,N	5100
IF (I.EQ.K) GO TO 282	5110
Q=A(K,I)	5120
DO 285 J=I,N1	5130
285 A(K,J)=A(K,J)-Q*A(I,J)	5140
282 CONTINUE	5150
GO TO 286	5160
284 WRITE (IPRNT,412)	5170
GO TO 314	5180
286 DO 288 I=1,N	5190
288 XP(I)=X(I)+A(I,N1)*DIA(I)	5200
C	5210
C * BOUNDARY CONDITIONS TO LIMIT THE RANGES OF X(1),X(3),X(4),X(5) *	5220
C	5230
C IF (KURVE.EQ.2) GO TO 540	5240
C	5250
C THE PRODUCT FUNCTION.	5260
C	5270
C IF (LIMIT.EQ.2) GO TO 299	5280
DO 505 I=1,M	5290
J=I+M	5300
K=J+M	5310
L=K+M	5320
XPK=ABS(XP(K))	5330
XPL=ABS(XP(L))	5340
IF (XPL.LE.1.0) GO TO 500	5350
XPL=1.0	5360

	IF (MLIST.LT.3) GO TO 500	5370
	WRITE (IPRNT,435) XP(J)	5380
500	IF (XPK.LE.2.0) GO TO 501	5390
	XPK=2.0	5400
	IF (MLIST.LT.3) GO TO 506	5410
	WRITE (IPRNT,435) XP(J)	5420
	GO TO 506	5430
501	IF (XPK.GT.0.03) GO TO 506	5440
	IF (XPL.GT.0.0333) GO TO 506	5450
	XPL=0.0333	5460
	IF (MLIST.LT.3) GO TO 506	5470
	WRITE (IPRNT,436) XP(J)	5480
506	IF (XP(K).LT.0.0) GO TO 503	5490
	XP(K)=XPK	5500
	GO TO 507	5510
503	XP(K)=-XPK	5520
507	IF (XP(L).LT.0.0) GO TO 504	5530
	XP(L)=XPL	5540
	GO TO 505	5550
504	XP(L)=-XPL	5560
505	CONTINUE	5570
	GO TO 299	5580
		5590
		5600
C		5610
C	THE SUM FUNCTION.	5620
C		5630
540	IF (LIMIT.EQ.1) GO TO 550	5640
	IF (NONEG.EQ.2) GO TO 299	5650
550	DO 556 I=1,M	5660
	J=I+M	5670
	K=J+M	5680
	L=K+M	5690
	XPI=XP(I)	5700
	XPK=ABS(XP(K))	5710
	XPL=ABS(XP(L))	5720
	IF (LIMIT.EQ.2) GO TO 559	5730
	IF (XPK.LT.2.0) GO TO 551	5740
	XPK=2.0	5750
	IF (MLIST.LT.3) GO TO 552	5760
	WRITE (IPRNT,435) XP(J)	5770
	GO TO 552	5780
551	IF (XPK.GE.0.042) GO TO 552	5790
	XPK=0.042	5800
	IF (MLIST.LT.3) GO TO 552	5810
	WRITE (IPRNT,436) XP(J)	5820
552	IF (XP(K).LT.0.0) GO TO 553	5830
	XP(K)=XPK	5840
	GO TO 557	5850
553	XP(K)=-XPK	5860
557	IF (XP(L).LT.0.0) GO TO 554	5870
	XP(L)=XPL	5880
	GO TO 558	5890
554	XP(L)=-XPL	5900
C		
558	IF (NONEG.EQ.2) GO TO 556	

```
559 IF (XPI.GE.0.0) GO TO 555 5910
    XP(I)=XB(I)*0.1 5920
    IF (MLIST.LT.3) GO TO 555 5930
    WRITE (IPRNT,437) XP(J) 5940
555 IF (XP(L).GE.0.0) GO TO 556 5950
    XP(L)=XB(L)*0.1 5960
C 5970
C NOTE THAT IF X1 OR X5 GOES NEGATIVE WE REDUCE IT TO ONE TENTH OF 5980
C THE VALUE FOUND IN THE PREVIOUS ITERATION. 5990
C 6000
C IF (MLIST.LT.3) GO TO 556 6010
C WRITE (IPRNT,438) XP(J) 6020
556 CONTINUE 6030
C 6040
C 6050
C ***** (FSP) SECTION ***** 6060
C 6070
299 FSP=0.0 6080
    DO 301 II=L1,NP 6090
    CALL POINT3 (XP,PC,PG,T,W,II,IK,KK,KK1,L1,M,N,IPRNT,CAY,KURVE,IJ) 6100
    TC=0.0 6110
    DO 302 JJ=1,KK 6120
302 TC=TC+T(JJ)*SY(JJ) 6130
    F=Y(II)-TC 6140
301 FSP=FSP+F*F 6150
    IF (FSM.LE.FSP) GO TO 303 6160
C 6170
C NOTE IF RESTRAINTS ARE APPLIED,THE PROGRAM CAN BRANCH BACK HERE ON 6180
C THE FIRST CYCLE TO REPETITIVELY OUTPUT THE ORIGINAL GUESSED 6190
C INDICES.THIS INDICATES THAT THE GUESSED INDICES (WITHOUT 6200
C RESTRAINTS) FIT BETTER THAN THE COMPUTED INDICES (WITH 6210
C RESTRAINTS). THIS IS ONLY LIKELY FOR SINGLE BANDS,BUT IF SO 6220
C RERUN WITH MLIST=4 AND CHANGE THE INITIAL INPUT INDICES. 6230
C 6240
    FSM=FSP 6250
    DO 305 I=1,N 6260
305 XB(I)=XP(I) 6270
303 IF (FS1.LE.FSP) GO TO 306 6280
    FS2=FS1 6290
    P2=P1 6300
    FS1=FSP 6310
    P1=P 6320
    GO TO 308 6330
306 IF (FS2.LE.FSP) GO TO 308 6340
    P2=P 6350
    FS2=FSP 6360
308 GO TO (250,309,250,309),MLIST 6370
309 WRITE (IPRNT,414) P,FSP 6380
    GO TO 250 6390
311 DO 312 I=1,N 6400
C 6410
C ***** TERMINAL SECTION ***** 6420
C 6430
312 X(I)=XB(I) 6440
```

NIT=NIT+1	6450
TEST=TERM/FSM	6460
TERM=FSM	6470
IF (TEST.GE.1.002) GO TO 315	6480
WRITE (IPRNT,441)	6490
GO TO 314	6500
315 IF (NIT.LE.NI) GO TO 316	6510
WRITE (IPRNT,442)	6520
GO TO 314	6530
316 IF (GL.GE.0.0001) GO TO 317	6540
WRITE (IPRNT,443)	6550
GO TO 314	6560
317 IF (ISECS.LE.NSEC) GO TO 320	6570
WRITE (IPRNT,444)	6580
GO TO 314	6590
320 IF (FM.GT.0.001) GO TO 200	6600
WRITE (IPRNT,445)	6610
314 DIS=SQRT(FSM/NP)	6620
WRITE (IPRNT,415)	6630
WRITE (IPRNT,419) FSM,DIS,FM,WFM	6640
IF (KURVE.EQ.2) GO TO 318	6650
WRITE (IPRNT,416)	6660
DO 319 I=1,M	6670
J=I+M	6680
K=J+M	6690
L=K+M	6700
X(I)=0.43429*X(I)	6710
IF (IDECK.EQ.1) GO TO 319	6720
WRITE (IPCH,420) X(I),X(J),X(K),X(L)	6730
319 WRITE (IPRNT,410) X(I),X(J),X(K),X(L)	6740
X(N)=0.43429*X(N)	6750
IF (IDECK.EQ.1) GO TO 322	6760
WRITE (IPCH,420) X(N)	6770
322 WRITE (IPRNT,413) X(N)	6780
GO TO 328	6790
318 WRITE (IPRNT,417)	6800
DO 325 I=1,M	6810
J=I+M	6820
K=J+M	6830
L=K+M	6840
X(I)=0.43429*X(I)	6850
X(L)=0.43429*X(L)	6860
XG=X(K)*CAY	6870
IF (IDECK.EQ.1) GO TO 325	6880
WRITE (IPCH,421) X(I),X(J),X(K),X(L)	6890
325 WRITE (IPRNT,406) X(I),X(J),X(K),XG,X(L)	6900
X(N)=0.43429*X(N)	6910
IF (IDECK.EQ.1) GO TO 327	6920
WRITE (IPCH,421) X(N)	6930
327 WRITE (IPRNT,422) X(N),CAY	6940
328 WRITE (IPRNT,434)	6950
GO TO 20	6960
	6970
	6980

C
C

400 FORMAT ('1PITHA AND JONES. PROGRAM XII (PC-118) SPECTRAL BAND FI 6990
1T OPTIMIZATION PROGRAM WITH SLIT FUNCTION CORRECTION.'/) 7000
401 FORMAT (20A4) 7010
402 FORMAT (1X,20A4) 7020
403 FORMAT (11I5) 7030
404 FORMAT (4F15.5) 7040
405 FORMAT (8(I5,I4,1X)) 7050
406 FORMAT (1X,5(6X,F15.5)) 7060
407 FORMAT (5X,2HFS,E12.4,8X,2HGL,E12.4,7X,3HWF,M,F6.1,7X,2HFM,E12.4,7X 7070
1,3HNIT,I3,4X,5HISECS,I5) 7080
408 FORMAT ('0INPUT PARAMETERS.') 7090
409 FORMAT (20X,4HDOWN,E14.6,7X,2HUP,E14.6,7X,6HCHANGE,E14.6) 7100
410 FORMAT (1X,4(6X,F15.5)) 7110
411 FORMAT (1X,'TROUBLE WITH EVALUATION OF P,CHECK MATRIX DATA OUTPUT. 7120
1') 7130
412 FORMAT (1X,'TERMINATED BY TROUBLE WITH SOLUTION OF EQUATIONS.') 7140
413 FORMAT (4X,7HALPHA =F8.5/, '0SOLVED FOR PRODUCT,CAUCHY OR GAUSS FUN 7150
1CTION.'/' (PURE CAUCHY IF X(4)=0 OR PURE GAUSS IF X(3)=0) ') 7160
414 FORMAT (64X,1HP,E14.6,8X,3HFSP,E14.6) 7170
415 FORMAT (11X, '----- 7180
1-----'/'1X,17HOUTPUT PARAMETERS) 7190
416 FORMAT ('0',15X,4HX(1),17X,4HX(2),17X,4HX(3),17X,4HX(4)) 7200
417 FORMAT ('0',15X,4HX(1),17X,4HX(2),17X,4HX(3),17X,4HX(4),17X,4HX(5) 7210
1) 7220
418 FORMAT (4X,7HALPHA =,F8.5,/'11X, '----- 7230
1-----') 7240
419 FORMAT (18X,3HFSSM,E14.6,7X,3HLIS,E14.6,7X,2HFM,E14.6,7X,3HWF,M,F7.1 7250
1) 7260
420 FORMAT (4F15.5,5X,7HPRODUCT) 7270
421 FORMAT (4F15.5,9X,3HSUM) 7280
422 FORMAT (4X,7HALPHA =,F8.5/'0SOLVED FOR SUM FUNCTION WITH X4=',F5.2 7290
1,4H X3.) 7300
423 FORMAT ('0',19X,2HNP,I6,17X,2HWB,F8.1,13X,2HWI,F5.1) 7310
424 FORMAT (/4X,5HMINAD,I4,13X,5HMAXAD,I4,12X,5HADMIN,E14.6,5X,5HADMAX 7320
1,E14.6/4X,5HMINA1,I4,1X,5HMINA2,I4,3X,4HAMIN,E14.6,3X,5HMAXA1,I4, 7330
23X,5HMAXA2,I4,3X,4HAMAX,E14.6) 7340
425 FORMAT ('0',9X,2HNP,I6,15X,2HWB,F8.1,11X,2HWI,F5.1,11X,3HSSW,F6.2) 7350
426 FORMAT (5F15.9) 7360
427 FORMAT ('0INPUT SLIT ORDINATES.') 7370
428 FORMAT (5X,10F12.8) 7380
429 FORMAT ('0COMPUTATION TERMINATED--INSUFFICIENT SLIT ORDINATES.') 7390
430 FORMAT ('0SYMMETRIC TRIANGULAR SLIT FUNCTION--NEWTON COTES WEIGHTI 7400
1NGS.') 7410
431 FORMAT ('0COMPUTATION TERMINATED--TOO MANY SLIT ORDINATES.') 7420
432 FORMAT ('0SYMMETRIC TRIANGULAR SLIT FUNCTION--SIMPSON RULE WEIGHTI 7430
1NGS.') 7440
433 FORMAT ('0COMPUTATION BY MODE 2--NORMALIZED SLIT ELEMENTS WITH SIM 7450
1PSON RULE WEIGHTINGS.') 7460
434 FORMAT ('0FSM IS THE VALUE OF THE MINIMIZATION FUNCTION.'/, 7470
1'ODIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEA 7480
2N SQUARE OF THE RESIDUALS).'/, '0FM IS THE MAXIMUM ORDINATE DIFFERE 7490
3NCE.'/, '0WFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE. 7500
4') 7510
435 FORMAT ('0MINIMAL HALF-WIDTH FOR BAND AT',F7.1,6H CM.-1) 7520

436	FORMAT ('C	MAXIMAL HALF-WIDTH FOR BAND AT',F7.1,6H CM.-1)	7530
437	FORMAT ('CX1 HELD POSITIVE AT',F7.1,6H CM.-1)	7540	
438	FORMAT ('OX5 HELD POSITIVE AT',F7.1,6H CM.-1)	7550	
439	FORMAT ('ORESTRAINTS TO HOLD X(1) AND X(5) POSITIVE HAVE BEEN APPL	7560	
	1IED.')	7570	
440	FORMAT ('ORESTRAINTS TO HOLD THE HALF-WIDTHS BETWEEN 1 AND 50 CM.-	7580	
	1-1 HAVE BEEN APPLIED.')	7590	
441	FORMAT ('OTERMINATED BECAUSE OF SLOW CONVERGENCE.'//)	7600	
442	FORMAT ('OTERMINATED BY ITERATION LIMIT.'//)	7610	
443	FORMAT ('OTERMINATED BY LOW VALUE OF GL.'//)	7620	
444	FORMAT ('OTERMINATED BY TIME LIMITATION.'//)	7630	
445	FORMAT ('OTERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VA	7640	
	1LUE.'//)	7650	
	END	7660	

```

C *****
C
C SUBROUTINE SORT3 (IX,IY,WB,WI,NP,IPRNT,KLENUP,IWB,IWI)
C
C SUBROUTINE SORT CHECKS FOR ERRORS IN THE INPUT WAVENUMBER DATA.
C A LIMITED NUMBER OF WAVENUMBER SEQUENCE ERRORS ARE CORRECTED
C BUT SEQUENCE ERRORS IN EXCESS OF 160 DATA POINTS (20 CARDS)
C OR ANY OTHER TYPE OF WAVENUMBER ERROR WILL TERMINATE THE
C COMPUTATION, AS ALSO WILL A DISCREPANCY BETWEEN IWB AND THE
C STARTING WAVENUMBER.
C THE WAVENUMBER POSITIONS OF THE CORRECTIONS AND OF A TERMINATING
C ERROR ARE RECORDED.
C IF CORRECTIONS ARE MADE, CORRECTED INPUT DATA ARE LISTED IN FULL.
C IF A TERMINATING ERROR IS FOUND THE UNCORRECTED INPUT DATA ARE
C LISTED IN FULL.
C
C DIMENSION IX(2000),IY(2000),ITEMPX(160),X1(160),ITEMPY(160)
C IF (IX(1).EQ.IWB) GO TO 10
C WRITE (IPRNT,456)
C KLENUP=2
C RETURN
10 MM=1
C DO 11 I=2,NP
C IW=IWB-IWI*(I-1)
C IF (IW.EQ.IX(I)) GO TO 11
C XX=IX(I)
C TEST=(WB-0.1*XX)/WI
C NTEST=TEST+0.005
C IF (ABS(TEST-NTEST).GT.0.005) GO TO 12
C ITEM PX(MM)=IX(I)
C ITEM PY(MM)=IY(I)
C MM=MM+1
C IF (MM.GT.160) GO TO 13
11 CONTINUE
C IF (MM.GT.1) GO TO 14
C WRITE (IPRNT,451)
15 KLENUP=1
C RETURN
12 XX1=IX(I-1)*0.1-WI
C WRITE (IPRNT,452) XX1
16 KLENUP=2
C RETURN
13 WRITE (IPRNT,453)
C WRITE (IPRNT,455) (IX(I),IY(I), I=1,NP)
C GO TO 16
14 NN=MM-1
C DO 17 MM=1,NN
C K1=1+(IWB-ITEMPX(MM))/IWI
C IX(K1)=ITEMPX(MM)
C IY(K1)=ITEMPY(MM)
17 X1(MM)=IX(K1)*0.1
C WRITE (IPRNT,450) (X1(MM),MM=1,NN)

```

7670
7680
7690
7700
7710
7720
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7740
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7970
7980
7990
8000
8010
8020
8030
8040
8050
8060
8070
8080
8090
8100
8110
8120
8130
8140
8150
8160
8170
8180
8190
8200

```
WRITE (IPPNT,454) (IX(I),IY(I),I=1,NP)
GO TO 15
450 FORMAT ('0WAVENUMBER CORRECTIONS AT',/ ,12(2X,F6.1,2X))
451 FORMAT ('0WAVENUMBER SEQUENCE IS CORRECT.')
452 FORMAT ('0TERMINATED BY ERROR AT',F6.1,6H CM.-1)
453 FORMAT ('0TERMINATED BY MULTIPLE WAVENUMBER SEQUENCE ERRORS.')
454 FORMAT ('0REARRANGED INPUT.',/ ,9(4X,2I5))
455 FORMAT ('0UNCORRECTED INPUT.',/ ,9(4X,2I5))
456 FORMAT ('0TERMINATED BY AN ERROR IN THE STARTING WAVENUMBER.')
END
```

8210
8220
8230
8240
8250
8260
8270
8280
8290
8300

```
C
C *****
C
SUBROUTINE POINT3 (PX,PC,PG,T,W,II,IK,KK,KK1,L1,M,N,IPRNT,CAY,KURV
1E,IJ)
C
C SUBROUTINE POINT CALCULATES THE ORDINATES OF THE COMPUTED BAND
C ENVELOPE IN UNITS OF NAPIERIAN ABSORBANCE.
C
DIMENSION PX(81),PC(20,25),PG(20,25),T(25),W(2000)
JSKIP=1
KSKIP=1
IJ=1
IF (II.GT.L1) GO TO 102
IK=KK
GO TO 103
102 DO 104 JJ=1,KK1
T(JJ)=T(JJ+1)
DO 104 I=1,M
PC(I,JJ)=PC(I,JJ+1)
104 PG(I,JJ)=PG(I,JJ+1)
IJ=KK
IK=KK
103 DO 105 JJ=IJ,IK
LL1=II+JJ-L1
WP=W(LL1)
AC=0.0
DO 106 I=1,M
J=I+M
K=J+M
L=K+M
R=WP-PX(J)
RSQ=R*R
PC(I,JJ)=1.0/(1.0+PX(K)*PX(K)*RSQ)
IF (KURVE.EQ.2) GO TO 108
PG(I,JJ)=PX(L)*PX(L)*RSQ
IF (PG(I,JJ).LT.10.0) GO TO 109
PG(I,JJ)=0.0
GO TO 111
109 PG(I,JJ)=EXP(-PG(I,JJ))
111 AC=PX(I)*PC(I,JJ)*PG(I,JJ)+AC
GO TO 106
108 PG(I,JJ)=CAY*CAY*PX(K)*PX(K)*RSQ
IF (PG(I,JJ).LT.10.0) GO TO 112
PG(I,JJ)=0.0
GO TO 114
112 PG(I,JJ)=EXP(-PG(I,JJ))
114 AC=PX(I)*PC(I,JJ)+PX(L)*PG(I,JJ)+AC
106 CONTINUE
AC=AC+PX(N)
IF (AC.GT.-2.0) GO TO 116
IF (JSKIP.EQ.2) GO TO 107
WRITE (IPRNT,470)
JSKIP=2
8310
8320
8330
8340
8350
8360
8370
8380
8390
8400
8410
8420
8430
8440
8450
8460
8470
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8490
8500
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8550
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8590
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8630
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8650
8660
8670
8680
8690
8700
8710
8720
8730
8740
8750
8760
8770
8780
8790
8800
8810
8820
8830
```

107	T(JJ)=2.7184	8840
	GO TO 105	8850
116	IF (AC.LE.10.C) GO TO 117	8860
	IF (KSKIP.EQ.2) GO TO 117	8870
	WRITE (IPENT,471)	8880
	KSKIP=2	8890
118	T(JJ)=0.0	8900
	GO TO 105	8910
117	T(JJ)=EXP(-AC)	8920
105	CONTINUE	8930
	RETURN	8940
470	FORMAT ('OTHE MAXIMAL ALLOWED TRANSMITTANCE HAS BEEN EXCEEDED.')	8950
471	FORMAT ('OTHE MINIMAL ALLOWED TRANSMITTANCE HAS BEEN EXCEEDED.')	8960
	END	8970

PIIHA AND JONES. PROGRAM XII (PC-118) SPECTRAL BAND FIT OPTIMIZATION PROGRAM WITH SLIT FUNCTION CORRECTION.

MARCH 13TH. 1968. BAND FIT PROGRAM WITH SLIT DECONVOLUTION.
FOUR BAND TEST DECK (PRODUCT) SYMMETRIC TRIANG SLIT WITH SSW 5.0 CM.-1

INPUT PARAMETERS. DOWN 0.100000E-01 UP 0.100000E 04 CHANGE 0.500000E 00
MP 180 MB 995.0 MI 0.5 SSW 5.00

WAVENUMBER SEQUENCE IS CORRECT.

SYMMETRIC TRIANGULAR SLIT FUNCTION--SIMPSON RULE WEIGHTINGS.

0.00000000 0.01333333 0.01333333 0.04000000 0.02666666 0.06666666 0.04000000 0.09333330 0.05333333 0.119
0.06666666 0.11999995 0.05333333 0.09333330 0.04000000 0.06666666 0.02666666 0.04000000 0.01333333 0.013
0.00000000

X(1) X(2) X(3) X(4)
0.27000 968.50000 0.18000 0.12000
0.62000 957.00000 0.22000 0.18000
0.32000 941.00000 0.12000 0.12000
0.37000 918.00000 0.22000 0.12000

ALPHA = 0.02000

FS 0.2276E 01 GL 0.1444E 02 WFM 924.0 FM 0.2241E 00 NIT 0 ISECS 8
FS 0.8185E-01 GL 0.8244E 00 WFM 953.5 FM 0.5457E-01 NIT 1 ISECS 22
FS 0.1825E-02 GL 0.1597E 00 WFM 917.0 FM 0.8025E-02 NIT 2 ISECS 37
FS 0.2109E-04 GL 0.1196E-01 WFM 961.5 FM 0.8969E-03 NIT 3 ISECS 51

TERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VALUE.

OUTPUT PARAMETERS

FSM 0.138526E-04 DIS 0.270015E-03 FM 0.896871E-03 WFM 961.5
X(1) X(2) X(3) X(4)
0.29997 969.99951 0.19999 0.09992
0.60066 954.99707 0.20223 0.19879
0.29994 939.99390 0.09928 0.10058
0.39958 920.00391 0.19950 0.10005
ALPHA = 0.04999

SOLVED FOR PRODUCT, CAUCHY OR GAUSS FUNCTION.
(PURE CAUCHY IF X(4)=0 OR PURE GAUSS IF X(3)=0)

FSM IS THE VALUE OF THE MINIMIZATION FUNCTION.

DIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEAN SQUARE OF THE RESIDUALS).

FM IS THE MAXIMUM ORDINATE DIFFERENCE.

WFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE.

PITHA AND JONES. PROGRAM XII (PC-118) SPECTRAL BAND FIT OPTIMIZATION PROGRAM WITH SLIT FUNCTION CORRECTION.

MARCH 13TH.1968. BAND FIT PROGRAM WITH SLIT DECONVOLUTION.
FOUR BAND TEST DPCK (SUM) ASYM.TRIANG. SLIT BY MODE 2.

INPUT PARAMETERS.

DOWN 0.100000E-01 UP 0.100000E 04 CHANGE 0.500000E 00

INPUT SLIT OPDINATES.

0.00000000 0.09999996 0.19999999 0.29999995 0.39999998 0.50000000 0.59999996 0.69999999 0.79999995 0.899
1.00000000 0.75000000 0.50000000 0.25000000 0.00000000

WP 186 WB 596.5 WI 0.5

WAVENUMBER SEQUENCE IS CORRECT.

COMPUTATION BY MODE 2--NORMALIZED SLIT ELEMENTS WITH SIMPSON RULE WEIGHTINGS.

0.00000000 0.01904763 0.01904763 0.05714289 0.03809526 0.09523815 0.05714289 0.13333338 0.07619047 0.171
0.09523815 0.14285719 0.04761908 0.04761908 0.00000000

X(1)	X(2)	X(3)	X(4)	X(5)
0.18000	968.00000	0.18000	0.14400	0.11000
0.37000	953.00000	0.22000	0.17600	0.22000
0.10000	942.00000	0.11000	0.08800	0.18000
0.26000	919.00000	0.21000	0.16800	0.16000

ALPHA = 0.02000

FS	GL	WFM	FM	WIT	ISECS
0.1185E 01	0.1469E 02	928.5	0.1450E 00	0	6
0.2678E-01	0.4360E 00	957.0	0.3184E-01	1	18
0.1328E-02	0.1157E 00	953.0	0.6925E-02	2	30
0.1643E-04	0.1055E-01	967.5	0.7808E-03	3	42

TERMINATED BECAUSE FM HAS REACHED MINIMAL SIGNIFICANT VALUE.

OUTPUT PARAMETERS

FSM 0.140989E-04 DIS 0.270280E-03 FM 0.780761E-03 WFM 967.5

X(1)	X(2)	X(3)	X(4)	X(5)
0.19999	970.00684	0.20051	0.16041	0.09940
0.39874	954.99780	0.20004	0.16003	0.19916
0.11103	939.99902	0.09926	0.07941	0.19002
0.24609	919.99365	0.20055	0.16044	0.15183

ALPHA = 0.04957

SOLVED FOR SUM FUNCTION WITH X4= 0.80 X3.

FSM IS THE VALUE OF THE MINIMIZATION FUNCTION.

DIS IS THE DISCREPANCE IN THE TRANSMITTANCE DIFFERENCE (ROOT MEAN SQUARE OF THE RESIDUALS).

FM IS THE MAXIMUM ORDINATE DIFFERENCE.

WFM IS THE WAVENUMBER OF THE MAXIMUM ORDINATE DIFFERENCE.

THE UNITED STATES OF AMERICA

DEPARTMENT OF THE INTERIOR

BUREAU OF LAND MANAGEMENT

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ORGANIZATION

PROGRAM XIII

PROGRAM XIII

Calculation of Cauchy-Gauss Shape Ratio and Half-band Widths

(PC-121)

This program retabulates the values of the indices and adds x_4 for the sum program; it also evaluates the following additional parameters for each component band:

1. The Cauchy-Gauss shape ratio
2. The half-band widths

A. The Cauchy-Gauss Shape Ratio

For the product function the shape ratio is defined as

$$SHAPP = ABS(X(3)) / [ABS(X(3)) + ABS(X(4))] \quad [36]$$

It should be noted that X(3) and X(4) indices of negative sign are not uncommon, but the sign is immaterial to the computation of the ordinates as these indices occur in equations [1] and [6] only as squared terms. SHAPP takes a value of unity for a pure Cauchy curve and zero for a pure Gauss curve.

For the sum function the shape ratio is defined as

$$SHAPS = AREAC / [AREAC + AREAG] \quad [37]$$

where

$$AREAC = 1.570796 X(1) \cdot (HLFWC) \quad [38]$$

and

$$AREAG = 1.0645 X(5) \cdot (HLFWG) \quad [39]$$

in which HLFWC and HLFWG are the half-band widths of the Cauchy and Gauss component curves respectively in cm.^{-1} .

B. The Half-Band Widths

There are no simple algebraic expressions for the half-band widths and it is necessary to evaluate them by an iteration method.

(i) The Product Function

If $2b$ is the half-bandwidth in cm.^{-1} we may write from equation [1]

$$0.5 = (1+x_3^2 b^2)^{-1} \cdot \exp - [x_4^2 b^2] \quad [40]$$

On inversion and expansion of the exponential term

$$2.0 = (1 + x_3^2 b^2) (1 + x_4^2 b^2 + \dots) \quad [41]$$

This provides a first approximation to b^2 in the form

$$b^4/2 + (WP)b^2 - 1/2x_3^2 x_4^2 \approx 0 \quad [42]$$

in which

$$WP = (x_3^2 + x_4^2)/2x_3^2 x_4^2 \quad [43]$$

In the program WP is evaluated following statement 13, and the quadratic equation [42] is solved to yield WX as an initial approximation for b^2 ; both roots are computed if they are real and positive, though there will normally be only one real and positive root; the two half-widths so found are designated HLFW1 and HLFW2. WX will differ from b^2 by an amount WF, where

$$WF = 2.0 - [1 + x_3^2 (WX)] \cdot \exp x_4^2 (WX) \quad [44]$$

The gradient dWF/dWX is next calculated; this reduces to the expression

$$\begin{aligned} dWF/dWX &= -P_5 (P_3 (1+P_6) + P_2) \\ &= WFD \end{aligned} \quad [45]$$

where $P_2=x_3^2$; $P_3=x_4^2$; $P_5=\exp P_3 (WX)$; $P_6=P_2 (WX)$.

A correction term WF/WFD is subtracted from WX to provide WXN, the second approximation to b^2 . This iterative process is continued until an acceptable agreement is obtained.

(ii) The Sum Function

For the sum function the treatment is similar, we have initially, with $x_4=kx_3$

$$0.5(x_1+x_5) = x_1(1+x_3^2b^2)^{-1} + x_5 \cdot \exp - [k^2x_3^2b^2] \quad [46]$$

Inversion of equation [46] does not simplify the algebra (cf. equation [42]): the expansion of equation [46] and collection of terms yields

$$b^4 [2x_5x_3^2k^2] + b^2 [x_1-x_5+2x_5k^2] - (x_1+x_5)/x_3^2 = 0 \quad [47]$$

which may be written

$$b^4S_3 + b^2S_5 + S_6 = 0 \quad [48]$$

where $S_1=x_3^2$; $S_2=S_1k^2$; $S_3=2S_2x_5$; $S_4=1/S_1$;

$$S_5= S_3S_4+x_1-x_5; S_6= -S_4(x_1+x_5).$$

Equation [48] is solved to obtain the first approximation of the composite half-band width (WX) following statement 128 in the program. The iterative process resembles that described for the product function with

$$WF = 0.5(x_1+x_5) - S_8x_1 + S_2S_{10} \quad [49]$$

and

$$WFD = x_1S_1S_8^2 + S_2S_{10} \quad [50]$$

where $S_8=1/(1+S_1(WX))$; $S_9=-S_2(WX)$; $S_{10}=x_5 \cdot \exp S_9$.

The half-band widths of the separate component Cauchy and Gauss curves (HLFWC) and (HLFWG) are also evaluated and recorded.

C. The Input Data

Cards 1 and 2 are heading cards HEAD1, HEAD2 (see Program X).

Card 3 carries four fixed point instructions in format 4I5. The instructions are NDATA, M, KURVE and NSEC which have the same connotations as for Program X.

Card 4 carries the ratio CAY in format F15.5. This CARD IS NEEDED ONLY FOR THE SUM FUNCTION AND MUST BE OMITTED WHEN WORKING WITH THE PRODUCT FUNCTION.

Card Deck 5 is a deck of M cards, each carrying the four band indices of a single band in format 4F15.5. The indices are x_1, x_2, x_3 and x_4 for the product function and x_1, x_2, x_3, x_5 for the sum function. The output data cards from the optimization programs X, XI, XIII can be used directly after removing the introductory and heading cards (see also Card Deck 7 on p. 13).

Card 6 This is a terminal card carrying the baseline constant α in format F15.5. This quantity does not enter into the computations, but it is stored and relisted with the output. When processing data not derived from the optimization programs α is liable to be zero, and should be entered as such. Failure to include this card will cause the program to terminate when attempting to process multiple decks with NDATA=2.

No detailed account of the internal logic of the program is called for. In the output of both the product and sum function computations the column headed HLFW-2 will normally be blank, indicating that only one real root of the quadratic equation [42] has been obtained.

The values computed by this program for the half-band widths and shape ratios for a range of values of x_3 and x_4 for the product function are listed in Table II. Similar data for the sum function for a range of values of x_3 with CAY=0.2 to CAY=0.8 are recorded in Table III. These tables will be found useful in selecting appropriate initial values for use with the band fit optimization programs. The boundary conditions limiting x_3 and x_4 in Table I were selected on the basis of these data.

TABLE II

Dependence of the Shape and Half-Band Width on X(3) and X(4)
for the Cauchy-Gauss Product Curve*

<u>SHAPE RATIO</u>	<u>X(3)</u>	<u>X(4)</u>	<u>HALF-WIDTH (cm.⁻¹)</u>
0.0	0.0	0.017	100.3
		0.021	80.1
		0.028	60.1
		0.042	40.0
		0.083	20.0
		0.111	15.0
		0.166	10.0
		0.208	8.0
		0.277	6.0
		0.416	4.0
		0.555	3.0
		0.833	2.0
		1.166	1.4
		1.665	1.0
		3.330	0.5
		0.1	0.002
0.027	61.3		
0.036	46.0		
0.045	36.8		
0.054	30.6		
0.072	23.0		
0.090	18.4		
0.180	9.2		
0.270	6.1		
0.360	4.6		
0.450	3.7		
0.540	3.1		
0.720	2.3		
0.900	1.8		
1.350	1.2		
1.800	0.92		
0.2	0.004	0.016	101.0
		0.020	80.8
		0.040	40.4
		0.080	20.2
		0.120	13.5
		0.160	10.1
		0.200	8.1
		0.240	6.7
		0.320	5.1
		0.400	4.0
		0.560	2.9
		0.800	2.0
		1.200	1.3
1.600	1.0		

Table II - ii.

<u>SHAPE RATIO</u>	<u>X(3)</u>	<u>X(4)</u>	<u>HALF-WIDTH (cm.⁻¹)</u>
0.3	0.005	0.012	128.5
	0.010	0.023	66.7
	0.020	0.047	32.7
	0.030	0.070	22.0
	0.040	0.093	16.5
	0.050	0.117	13.1
	0.060	0.140	11.0
	0.080	0.187	8.2
	0.100	0.233	6.6
	0.150	0.350	4.4
	0.200	0.467	3.3
	0.400	0.932	1.6
	0.600	1.400	1.1
0.4	0.01	0.015	93.8
	0.02	0.030	46.9
	0.03	0.045	31.3
	0.04	0.060	23.4
	0.05	0.075	18.8
	0.06	0.090	15.6
	0.08	0.120	11.7
	0.10	0.150	9.4
	0.15	0.225	6.3
	0.20	0.300	4.7
	0.30	0.450	3.1
	0.40	0.60	2.3
	0.70	1.05	1.3
1.00	1.50	0.9	
0.5	0.01	0.01	122.4
	0.02	0.02	61.2
	0.03	0.03	40.8
	0.04	0.04	30.6
	0.05	0.05	24.5
	0.06	0.06	20.4
	0.08	0.08	15.3
	0.10	0.10	12.2
	0.14	0.14	8.7
	0.20	0.20	6.1
	0.30	0.30	4.1
	0.40	0.40	3.1
	0.60	0.60	2.0
1.00	1.00	1.2	
2.00	2.00	0.6	

Table II - iii.

<u>SHAPE RATIO</u>	<u>X(3)</u>	<u>X(4)</u>	<u>HALF-WIDTH (cm.⁻¹)</u>
0.6	0.015	0.010	99.7
	0.02	0.013	74.9
	0.03	0.020	49.9
	0.04	0.027	37.4
	0.05	0.033	29.9
	0.06	0.040	24.9
	0.08	0.053	18.7
	0.10	0.067	15.0
	0.14	0.093	10.7
	0.20	0.133	7.5
	0.30	0.200	5.0
	0.40	0.267	3.7
	0.60	0.400	2.5
	1.00	0.667	1.5
2.00	1.333	0.75	
0.7	0.015	0.006	115.2
	0.02	0.009	86.2
	0.03	0.013	57.6
	0.04	0.017	43.2
	0.05	0.021	34.5
	0.06	0.026	28.8
	0.08	0.034	21.6
	0.10	0.043	17.3
	0.15	0.064	11.5
	0.20	0.086	8.6
	0.30	0.129	5.7
	0.40	0.171	4.3
	0.60	0.257	2.9
	1.00	0.429	1.7
2.00	0.857	0.9	
0.8	0.02	0.005	94.4
	0.03	0.007	62.9
	0.04	0.010	47.2
	0.05	0.012	37.8
	0.06	0.015	31.5
	0.08	0.020	23.6
	0.10	0.025	18.9
	0.20	0.050	9.4
	0.30	0.075	6.3
	0.40	0.100	4.7
	0.60	0.150	3.1
	1.00	0.250	1.9
	2.00	0.500	0.9

Table II - iv.

<u>SHAPE RATIO</u>	<u>X(3)</u>	<u>X(4)</u>	<u>HALF-WIDTH (cm.⁻¹)</u>
0.9	0.02	0.0022	98.8
	0.03	0.0033	65.9
	0.05	0.0056	39.5
	0.10	0.0111	19.8
	0.15	0.0167	13.1
	0.20	0.0222	9.9
	0.25	0.0278	7.9
	0.30	0.0333	6.6
	0.40	0.0444	4.9
	0.60	0.0667	3.3
	1.00	0.1111	2.0
	1.50	0.1667	1.3
	2.00	0.2222	1.0
1.0	0.017	0.0	119.8
	0.025		80.0
	0.050		40.0
	0.100		20.0
	0.200		10.0
	0.300		6.7
	0.400		5.0
	0.600		3.3
	1.000		2.0
	2.000		1.0

 * Note that these figures have been rounded for tabulation; they are intended to be used only as a guide to the selection of appropriate starting values for X(3) and X(4).

TABLE III

Dependence of the Half-Width on X(3) and CAY for the Cauchy-Gauss Sum Function*

<u>X(1)/X(5)=0.1</u>	X(3)	HALF-WIDTH (cm. ⁻¹)			
		CAY=0.8	CAY=0.6	CAY=0.4	CAY=0.2
	0.02	103.8	135.8	199.2	390.0
	0.04	51.9	67.9	99.6	195.1
	0.06	34.6	45.3	66.4	130.1
	0.08	26.0	33.9	49.8	97.6
	0.10	20.8	27.2	39.8	78.0
	0.20	10.4	13.6	19.9	39.0
	0.30	6.9	9.1	13.3	26.0
	0.40	5.2	6.8	10.0	19.5
	0.60	3.5	4.5	6.6	13.0
	1.00	2.1	2.7	4.0	7.8
	2.00	1.0	1.4	2.0	3.9
<hr/>					
<u>X(1)/X(5)=0.5</u>	0.02	103.0	127.1	171.8	298.8
	0.04	51.5	63.6	85.9	149.4
	0.06	34.3	42.4	57.3	99.6
	0.08	25.7	31.7	43.0	74.7
	0.10	20.6	25.4	34.4	59.8
	0.20	10.3	12.7	17.2	29.9
	0.30	6.9	8.5	11.4	19.9
	0.40	5.1	6.4	8.6	14.9
	0.60	3.4	4.2	5.7	10.0
	1.00	2.1	1.7	3.4	6.0
	2.00	1.0	1.3	1.7	3.0
<hr/>					
<u>X(1)/X(5)=1.0</u>	0.02	102.3	120.6	150.9	218.3
	0.04	51.1	60.3	75.4	109.1
	0.06	34.1	40.2	50.3	72.7
	0.08	25.6	30.1	37.7	54.6
	0.10	20.5	24.1	30.1	43.7
	0.20	10.2	12.1	15.1	21.8
	0.30	6.8	8.0	10.1	14.6
	0.40	5.1	6.0	7.5	10.9
	0.60	3.4	4.0	5.0	7.3
	1.00	2.0	2.4	3.0	4.4
	2.00	1.0	1.2	1.5	2.2

Table III - ii.

X(1)/X(5)=10.0	X(3)	HALF-WIDTH (cm. ⁻¹)			
		CAY=0.8	CAY=0.6	CAY=0.4	CAY=0.2
	0.02	100.5	103.7	106.9	109.5
	0.04	50.2	51.8	53.4	54.8
	0.06	33.5	34.6	35.6	36.5
	0.08	25.1	25.9	26.7	27.4
	0.10	20.1	20.7	21.4	21.9
	0.20	10.0	10.4	10.7	11.0
	0.30	6.7	6.9	7.1	7.3
	0.40	5.0	5.2	5.3	5.5
	0.60	3.3	3.5	3.6	3.6
	1.00	2.0	2.1	2.1	2.2
	2.00	1.0	1.0	1.1	1.1

* Note that these figures have been rounded for tabulation; they are intended to be used only as a guide to the selection of appropriate starting values for X(3).

Most absorption bands are closer to the Cauchy than the Gauss shape and, in our experience an initial ratio of X(1)/X(5)=10.0 is usually acceptable. Under these conditions the half-band width is not very sensitive to the value chosen for CAY, but it becomes increasingly so as X(1)/X(5) diminishes and the band becomes more Gaussian.

C		10
C	*****	20
C	*	30
C	* CALCULATION OF CAUCHY-GAUSS SHAPE RATIO AND *	40
C	*	50
C	* HALF-BAND WIDTHS. *	60
C	*	70
C	*****	80
C		90
C	R.N.JONES AND J.PITHA, DIVISION OF CHEMISTRY, NATIONAL RESEARCH	100
C	COUNCIL OF CANADA, SUSSEX DRIVE, OTTAWA, CANADA.	110
C		120
C		130
C	PROGRAM XIII (PC-121) SHAPE AND HALF-WIDTH CALCULATOR.	140
C	JULY 22ND. 1967.	145
C		150
C	FOR THE SUM FUNCTION THE HALF-WIDTHS AND SHAPES OF THE CAUCHY	160
C	AND GAUSS COMPONENT BANDS ARE SEPARATELY EVALUATED.	170
C	THESE CALCULATIONS DO NOT INVOLVE THE BASELINE CONSTANT, ALPHA,	180
C	BUT, FOR COMPLETENESS, IT IS INCLUDED IN THE OUTPUT TABULATION.	190
C	FOR DETAILS SEE N.R.C.C. BULLETIN NO. 12.	200
C		210
C	===== DON'T FORGET THE CAY CARD FOR THE SUM FUNCTION.=====	220
C		230
C	THE CAY CARD IMMEDIATELY PRECEEDS THE DATA DECK.	240
C		250
C	===== DON'T FORGET THE TERMINAL ALPHA CARD.=====	260
C		270
C	DIMENSION HEAD1(20), HEAD2(20)	280
C	IRD=1	290
C	IPRNT=3	300
C	10 WRITE (IPRNT,400)	310
C	READ (IRD,401) HEAD1	320
C	READ (IRD,401) HEAD2	330
C	READ (IRD,402) NDATA, M, KURVE, NSEC	340
C		350
C	M IS THE NUMBER OF BANDS TO BE CALCULATED.	360
C		370
C	USE KURVE=1 FOR A PRODUCT FUNCTION; KURVE=2 FOR A SUM FUNCTION.	380
C		390
C	WRITE (IPRNT,403) HEAD1	400
C	WRITE (IPRNT,403) HEAD2	410
C	ISKIP=1	420
C	IF (KURVE.EQ.2) GO TO 100	430
C		440
C	***** PRODUCT FUNCTION SECTION *****	450
C		460
C	WRITE (IPRNT,404)	470
C	CALL SETCLK	480
C	DO 50 J=1, M	490
C	IT=0	500
C	X1=0.0	510
C	X2=0.0	520
C	X3=0.0	530

	X4=0.0	540
	HLFW1=0.0	550
	HLFW2=0.0	560
	READ (IRD,405) X1,X2,X3,X4	570
C		580
C		590
	IF (ABS(X4).LT.0.0001) GO TO 11	600
	IF (ABS(X3).LT.0.0001) GO TO 12	610
	GO TO 13	620
C		630
C		640
C		650
	CALCULATION OF SHAPE AND HALF-WIDTH FOR THE PURE CAUCHY CURVE.	660
	11 HLFW1=2.0/X3	670
	SHAPP=1.000	680
	GO TO 4C	690
C		700
C		710
C		720
	CALCULATION OF THE SHAPE AND HALF-WIDTH FOR THE PURE GAUSS CURVE.	730
	12 HLFW1=1.665109/X4	740
	SHAPP = 0.000	750
	GO TO 4C	760
C		765
C		770
C		780
C		790
C		800
	CALCULATION OF THE HALF-WIDTH OF THE PRODUCT CURVE BY ITERATION.	810
	THE SOLUTION OF THE QUADRATIC EQUATION GIVES TWO VALUES,	820
	BOTH ARE COMPUTED IF THEY ARE REAL AND POSITIVE, BUT NORMALLY	830
	ONLY HLFW1 WILL BE OBTAINED.	840
	13 P2=X3*X3	850
	P3=X4*X4	860
	WP=(P2+P3)/(2.0*P2*P3)	870
	P4=WP*WP+1.0/(P2*P3)	880
	IF (P4.LT.0.0) GO TO 17	890
	P4=SQRT(P4)	900
	IF (ISKIP.EQ.2) GO TO 16	910
	WX=P4-WP	920
	GO TO 27	930
	17 WRITE (IPRNT,415)	940
	GO TO 49	950
	16 WX=-WP-P4	960
	27 IF (WX.GT.0.0) GO TO 21	970
	IF (ISKIP.EQ.2) GO TO 30	980
	ISKIP=2	990
	GO TO 16	1000
	21 P5=EXP(P3*WX)	1010
	P6=P2*WX	1020
	WF=2.0-P5*(1.0+P6)	1030
	WFD=-P5*(P3*(1.0+P6)+P2)	1040
	WXN=WX-WF/WFD	1050
	WDIF=ABS(WX-WXN)	1060
	IF (WDIF.LE.(WXN*0.0001)) GO TO 22	
	WX=WXN	
	IT=IT+1	
	IF (IT.LT.5) GO TO 21	

	WRITE (IPRNT,417)	1070
	GO TO 22	1080
22	WX=SQRT(WXN)	1090
	IF (ISKIP.EQ.2) GO TO 25	1100
	HLFW1=2.0*WX	1110
	ISKIP=2	1120
	GO TO 16	1130
25	HLFW2=2.0*WX	1140
30	ISKIP=1	1150
C		1160
C	CALCULATION OF THE SHAPE RATIO OF THE PRODUCT CURVE.	1170
C		1180
	SHAPP= ABS(X3)/(ABS(X3)+ABS(X4))	1190
40	IF (HLFW2.EQ.0.0) GO TO 41	1200
	WRITE (IPRNT,406) X1,X2,X3,X4,SHAPP,HLFW1,HLFW2	1210
	GO TO 49	1220
41	WRITE (IPRNT,407) X1,X2,X3,X4,SHAPP,HLFW1	1230
49	CALL RDCLK (TIME)	1240
	ISECS=TIME+0.5	1250
	IF (ISECS.GT.NSEC) GO TO 52	1260
50	CONTINUE	1270
	GO TO 53	1280
52	WRITE (IPRNT,414)	1290
53	WRITE (IPRNT,408)	1300
C		1310
C	***** TERMINAL SECTION FOR BOTH FUNCTIONS *****	1320
C		1330
51	READ (IRD,405) XN	1340
	WRITE (IPRNT,409) XN	1350
	IF (NDATA.EQ.2) GO TO 10	1360
	STOP	1370
C		1380
C	***** SUM FUNCTION SECTION *****	1390
C		1400
100	WRITE (IPRNT,410)	1410
	READ (IRD,405) CAY	1420
	CALL SETCLK	1430
101	DO 150 J=1,M	1440
	IT=0	1450
	X1=0.0	1460
	X2=0.0	1470
	X3=0.0	1480
	X5=0.0	1490
	HLFW1=0.0	1500
	HLFW2=0.0	1510
	READ (IRD,405) X1,X2,X3,X5	1520
	XX1=X1	1530
	XX3=X3	1540
	XX5=X5	1550
	X1=ABS(X1)	1560
	X3=ABS(X3)	1570
	X5=ABS(X5)	1580
	X4=X3*CAY	1590
	XX4=XX3*CAY	1600

C		1610
C	CALCULATION OF THE HALF-WIDTH OF THE CAUCHY COMPONENT CURVE.	1620
C	HLFWC=2.0/X3	1630
C		1640
C		1650
C	CALCULATION OF THE HALF-WIDTH OF THE GAUSS COMPONENT CURVE.	1660
C		1670
C	HLFWG=1.665109/X4	1680
C		1690
C	CALCULATION OF THE HALF-WIDTH OF THE COMPOSITE CURVE.	1700
C		1710
C	FIRST CHECK FOR ZERO X1 OR X5	1720
C	THIS SIGNIFIES A PURE GAUSS OR PURE CAUCHY CURVE, RESPECTIVELY.	1730
C		1740
	IF (X1.NE.C.0) GO TO 112	1750
	HLFW1=HLFWG	1760
	HLFW2=0.0	1770
	GO TO 130	1780
112	IF (X5.NE.0.0) GO TO 114	1790
	HLFW1=HLFWC	1800
	HLFW2=0.0	1810
	GO TO 130	1820
114	S1=X3*X3	1830
	S2=X4*X4	1840
	S3=2.0*X5*S2	1850
	S4=1.0/S1	1860
	S5=S3*S4+X1-X5	1870
	S6=-S4*(X1+X5)	1880
	S7=S5*S5-4.0*S3*S6	1890
	IF (S7.GE.0.0) GO TO 128	1900
	WRITE (IPRNT,415)	1910
	GO TO 150	1920
128	S7=SQRT(S7)	1930
	IF (ISKIP.EQ.2) GO TO 116	1940
	WX=S7-S5	1950
	GO TO 127	1960
116	WX=-S5-S7	1970
127	WX=WX/(2.0*S3)	1980
	IF (WX.GT.C.0) GO TO 121	1990
	IF (ISKIP.EQ.2) GO TO 130	2000
	ISKIP=2	2010
	GO TO 116	2020
121	S8=1.0/(1.0+S1*WX)	2030
	S9=-S2*WX	2040
	S10=X5*EXP(S9)	2050
	WF=0.5*(X1+X5)-X1*S8-S10	2060
	WFD=X1*S1*S8*S8+S2*S10	2070
	WXN=WX-WF/WFD	2080
	WDIF=ABS(WX-WXN)	2090
	IF (WDIF.LE.WXN*0.0001) GO TO 122	2100
	WX=WXN	2110
	IT=IT+1	2120
	IF (IT.LT.5) GO TO 121	2130
	WRITE (IPRNT,417)	2140

	GO TO 122	2150
122	IF (WXN.GE.0.0) GO TO 129	2160
	WRITE (IPRNT,416)	2170
	IF (ISKIP.EQ.1) GO TO 123	2180
	GO TO 150	2190
129	WX=SQRT (WXN)	2200
	IF (ISKIP.EQ.2) GO TO 125	2210
	HLFW1=2.0*WX	2220
123	ISKIP=2	2230
	GO TO 116	2240
125	HLFW2=2.0*WX	2250
130	ISKIP=1	2260
C		2270
C	CALCULATION OF THE CAUCHY-GAUSS SHAPE RATIO FOR THE SUM BAND.	2280
		2290
	AREAC=1.570796*XX1*HLFWC	2300
	AREAG=1.0645*XX5*HLFWG	2310
	SHAPS=AREAC/(AREAC+AREAG)	2320
	IF (HLFW2.EQ.0.0) GO TO 141	2330
	WRITE (IPRNT,411) XX1,X2,XX3,XX4,XX5,SHAPS,HLFWC,HLFWG,HLFW1,HLFW2	2340
	GO TO 149	2350
141	WRITE (IPRNT,411) XX1,X2,XX3,XX4,XX5,SHAPS,HLFWC,HLFWG,HLFW1	2360
149	CALL RDCLK (TIME)	2370
	ISECS=TIME+0.5	2380
	IF (ISECS.GT.NSEC) GO TO 152	2390
150	CONTINUE	2400
	GO TO 153	2410
152	WRITE (IPRNT,414)	2420
153	WRITE (IPRNT,413) CAY	2430
	GO TO 51	2440
C		2450
C		2460
400	FORMAT ('1PITHA AND JONES. PROGRAM XIII (PC-121) BAND FIT PROG	2470
	1RAM--SHAPES AND HALF-WIDTHS.')	2480
401	FORMAT (20A4)	2490
402	FORMAT (4I5)	2500
403	FORMAT (1X,20A4)	2510
404	FORMAT ('0',10X,4HX(1),8X,4HX(2),7X,4HX(3),7X,4HX(4),7X,5HSHAPE,	2520
	16X,6HHLFW-1,5X,6HHLFW-2)	2530
405	FORMAT (4F15.5)	2540
406	FORMAT ('0',5X,F10.6,2X,F10.3,2F11.6,3F12.6)	2550
407	FORMAT ('0',5X,F10.6,2X,F10.3,2F11.6,2F12.6,7X,1H-)	2560
408	FORMAT ('0THESE DATA ARE FOR THE PRODUCT FUNCTION.')	2570
409	FORMAT (/8X,7HALPHA = ,E14.6)	2580
410	FORMAT ('0',10X,4HX(1),6X,4HX(2),7X,4HX(3),7X,4HX(4),7X,4HX(5),6X,	2590
	15HSHAPE,6X,6HHLFW-C,6X,6HHLFW-G,6X,6HHIFW-1,5X,6HHLFW-2)	2600
411	FORMAT ('0',5X,F10.6,F10.3,4F11.6,4F12.6)	2610
412	FORMAT ('0',5X,F10.6,F10.3,4F11.6,3F12.6,7X,1H-)	2620
413	FORMAT ('0THESE DATA ARE FOR THE SUM FUNCTION WITH CAY =',F5.2)	2630
414	FORMAT ('0TERMINATED BY PROGRAM TIME CONTROL.')	2640
415	FORMAT ('0ROOTS OF THE QUADRATIC EQUATION ARE IMAGINARY.')	2650
416	FORMAT ('0HALF-WIDTH OF THE COMPOSITE CURVE IS IMAGINARY.')	2660
417	FORMAT ('0FIVE ITERATION LIMIT ON NEXT BAND.')	2670
	END	2680

PITHA AND JONES. PPROGRAM XIII (PC-121) BAND FIT PROGRAM--SHAPES AND HALF-WIDTHS.

APRIL 3RD. 1968. FOUR BAND TEST DECF FOR PRODUCT FUNCTION.
TRUE VALUES FROM CALCULATED CURVE.

X(1)	X(2)	X(3)	X(4)	SHAPE	HLPW-1	HLFW-2
0.300000	970.000	0.200000	0.100000	0.666667	8.277420	-
0.600000	955.000	0.200000	0.200000	0.500000	6.122278	-
0.300000	940.000	0.100000	0.100000	0.500000	12.244562	-
0.400000	920.000	0.200000	0.100000	0.666667	8.277420	-

THESE DATA ARE FOR THE PRODUCT FUNCTION.

ALPHA = 0.500000E-01

PITHA AND JONES. PROGRAM XIII (PC-121) BAND FIT PROGRAM--SHAPES AND HALF-WIDTHS.

APRIL 3RD. 1968. FOUR BAND TEST DECK FOR SUM FUNCTION.
TRUE VALUES FROM CALCULATED CURVE.

X(1)	X(2)	X(3)	X(4)	X(5)	SHAPE	HLFW-C	HLFW-G	HLFW-1	HLFW-2
0.200000	970.000	0.200000	0.160000	0.100000	0.739301	10.000000	10.406931	10.163906	
0.400000	955.000	0.200000	0.160000	0.200000	0.739301	10.000000	10.406931	10.163906	
0.100000	940.000	0.100000	0.080000	0.200000	0.414848	20.000000	20.813873	20.594498	
0.250000	920.000	0.200000	0.160000	0.150000	0.702664	10.000000	10.406931	10.162089	

THESE DATA ARE FOR THE SUM FUNCTION WITH CAY = 0.80

ALPHA = 0.500000E-01

Date	Description	Debit	Credit	Balance
1912	Jan 1			
	Jan 2			
	Jan 3			
	Jan 4			
	Jan 5			
	Jan 6			
	Jan 7			
	Jan 8			
	Jan 9			
	Jan 10			
	Jan 11			
	Jan 12			
	Jan 13			
	Jan 14			
	Jan 15			
	Jan 16			
	Jan 17			
	Jan 18			
	Jan 19			
	Jan 20			
	Jan 21			
	Jan 22			
	Jan 23			
	Jan 24			
	Jan 25			
	Jan 26			
	Jan 27			
	Jan 28			
	Jan 29			
	Jan 30			
	Jan 31			

PROGRAM XIV

PROGRAM XIV

Calculation of the Ordinates of Cauchy-Gauss Band Envelopes

(PC-122)

When supplied with the indices of either the product or sum functions, this program generates a set of ordinates for the overlapping band envelope. The calculated ordinates are spaced at equal abscissal intervals determined by the selected value of WI.

This program is dimensioned for a maximum of twenty overlapping bands and two thousand calculated ordinates. The output can be either in units of absorbance or transmittance $\times 1000$, and a card deck in the standard punched format can be obtained as well as the printed listing. When operated in the absorbance mode, the Cauchy and Gauss components of the sum function are listed separately in parallel columns while a third column lists the summed value, included in which is the baseline constant α . On the transmittance $\times 1000$ scale only the summed value, including α , is listed.

This program may also be used to generate a set of ordinates for single bands of pure Cauchy, pure Gauss, product, or sum contour, but a more versatile program that will generate single band of any requisite contour, based on a single valued function, is described in Bulletin 11 (Program VIII).

A. The Input Data

Cards 1 and 2 are heading cards HEAD1, HEAD2 (see Program X).

Card 3 carries six fixed point instructions NDATA, IDECK, NP, M, KURVE, IXIT in format 6I5. The first five have the same connotation as for Program X.

Use IXIT=1 for ordinate output in units of transmittance $\times 1000$.

Use IXIT=2 for ordinate output in absorbance units.

Card 4 carries two floating point instructions for the product function and three for the sum function in formats 2F15.5 or 3F15.5 respectively. They are WB, WI and CAY as described for Program X.

Card Deck 5 This is a set of M cards carrying the input ordinate indices x_1, x_2, x_3, x_4 for the product function and x_1, x_2, x_3, x_5 for the sum function. (See Card Deck 7 on p. 13).

Card 6 is the terminal card carrying the baseline constant α . (See Card 8 on p. 13.)

No detailed account of the internal logic of the program is required beyond the comment statements that are incorporated in the program.

The test data sets are for the four band product and sum band enveloped illustrated in Figs. 1 and 2 on pp. 24,25 of this volume.

C		10
C	*****	20
C	*	30
C	* CALCULATION OF THE ORDINATES OF CAUCHY-GAUSS	40
C	*	50
C	* BAND ENVELOPES.	60
C	*	70
C	*****	80
C		90
C	J. PITHA AND R.N.JONES, DIVISION OF CHEMISTRY, NATIONAL RESEARCH	100
C	COUNCIL OF CANADA, SUSSEX DRIVE, OTTAWA, CANADA.	110
C		120
C	PROGRAM XIV (PC-122)	130
C		140
C	THE ORDINATES CAN BE EVALUATED IN TRANSMITTANCE X 1000 OR IN	150
C	ABSORBANCE.	160
C	FOR THE SUM FUNCTION THE ABSORBANCE OF THE GAUSS AND CAUCHY	170
C	COMPONENTS ARE LISTED SEPARATELY. THEY ARE ALSO SUMMED	180
C	TOGETHER WITH THE BASELINE CONSTANT. THE SUMMED ORDINATES MAY	190
C	BE LISTED IN EITHER ABSORBANCE OR TRANSMITTANCE X 1000.	200
C	THIS PROGRAM IS DIMENSIONED FOR 2000 DATA POINTS AND 20 COMPONENT	210
C	BANDS. IN THE PRODUCT MODE THE PROGRAM WILL GENERATE A PURE CAUCHY	220
C	CURVE IF X(4)=0 AND PURE GAUSS CURVE IF X(3)=0.	230
C		235
C	FOR DETAILS SEE N.R.C.C. BULLETIN NO.12.	240
C		250
C	DIMENSION PC(20), PG(20), X(81), IW(2000), WW(2000), ORD1(2000),	260
C	1ORD2(2000), SUM(2000), HEAD1(20), HEAD2(20), IT(2000)	270
C	EQUIVALENCE (SUM(1), IT(1))	280
C	IRD=1	290
C	IPCH=2	300
C	IPRNT=3	310
C	10 WRITE (IPRNT,400)	320
C	READ (IRD,401) HEAD1	330
C	READ (IRD,401) HEAD2	340
C	READ (IRD,402) NDATA, IDECK, NP, M, KURVE, IXIT	350
C	IF (KURVE.EQ.2) GO TO 12	360
C	READ (IRD,407) WB, WI	370
C	GO TO 13	380
C	12 READ (IRD,407) WB, WI, CAY	390
C		400
C	USE KURVE=1 FOR PRODUCT FUNCTION AND KURVE=2 FOR SUM FUNCTION.	410
C	REMEMBER THAT IF KURVE=2 CAY MUST BE DEFINED.	420
C	USE IXIT=1 FOR OUTPUT IN CM.-1 X 10 AND TRANSMITTANCE X 1000.	430
C	USE IXIT=2 FOR OUTPUT IN CM.-1 AND ABSORBANCE UNITS.	440
C		450
C	13 IF (IDECK.EQ.1) GO TO 11	460
C	WRITE (IPCH,401) HEAD1	470
C	WRITE (IPCH,401) HEAD2	480
C	11 WRITE (IPRNT,404) HEAD1	490
C	WRITE (IPRNT,404) HEAD2	500
C	IF (KURVE.EQ.2) GO TO 14	510
C	WRITE (IPRNT,405)	520
C	GO TO 15	530

14	WRITE (IPRNT,406)	540
15	N=4*M+1	550
	DO 16 I=1,M	560
	J=I+M	570
	K=J+M	580
	L=K+M	590
	READ (IRD,407) X(I),X(J),X(K),X(L)	600
	WRITE (IPRNT,408) X(I),X(J),X(K),X(L)	610
16	CONTINUE	620
	READ (IRD,407) X(N)	630
	WRITE (IPRNT,409) X(N)	640
	WRITE (IPRNT,410) NP,WB,WI	650
	IF (KURVE.EQ.2) GO TO 120	660
	***** COMPUTATION OF THE ORDINATES OF THE PRODUCT FUNCTION *****	670
		680
	DO 21 II=1,NP	690
	FII=II-1	700
	W=WB-WI*FII	710
	AC=0.0	720
	DO 22 I=1,M	730
	J=I+M	740
	K=J+M	750
	L=K+M	760
	R=W-X(J)	770
	RSQ=R*R	780
	PC(I)=1.0/(1.0+X(K)*X(K)*RSQ)	790
	PG(I)=X(L)*X(L)*ESQ	800
	IF (PG(I).LT.10.0) GO TO 23	810
	PG(I)=0.0	820
	GO TO 22	830
23	PG(I)=EXP(-PG(I))	840
22	AC=X(I)*PC(I)*PG(I)+AC	850
	AC=AC+X(N)	860
	IF (AC.LE.0.0006) GO TO 26	870
	IF (AC.LT.10.0) GO TO 30	880
	AC=10.0	890
	GO TO 30	900
26	AC=0.0	910
30	ORD1(II)=AC	920
	WW(II)=W	930
21	IW(II)=W*10.0+C.5	940
	WRITE (IPRNT,420)	950
	IF (IXIT.EQ.2) GO TO 34	960
	DO 31 I=1,NP	970
31	IT(I)=EXP(-ORD1(I)*2.30258)*1000.0+C.5	980
	WRITE (IPRNT,411)	990
	WRITE (IPRNT,412) (IW(I),IT(I),I=1,NP)	1000
	IF (IDECK.EQ.1) GO TO 32	1010
	WRITE (IPCH,413) (IW(I),IT(I),I=1,NP)	1020
32	IF (NDATA.EQ.1) GO TO 33	1030
	GO TO 10	1040
33	STOP	1050
34	WRITE (IPRNT,414)	1060
		1070

C
C
C

```
WRITE (IPFNT,415) (WW(I),ORD1(I),I=1,NP) 1080
IF (IDECK.EQ.1) GO TO 32 1090
WRITE (IPCH,416) (WW(I),ORD1(I),I=1,NP) 1100
GO TO 32 1110
C
C ***** COMPUTATION OF THE ORDINATES OF THE SUM FUNCTION ***** 1120
C
C IN THIS SECTION, ORDINATES OF THE CAUCHY COMPONENT ARE EVALUATED. 1130
C 1140
C 1150
C 1160
120 DO 121 II=1,NP 1170
    FII=II-1 1180
    W=WB-WI*FII 1190
    AC=0.0 1200
    DO 122 I=1,M 1210
        J=I+M 1220
        K=J+M 1230
        L=K+M 1240
        R=(W-X(J))*X(K) 1250
        RSQ=R*R 1260
        PC(I)=1.0/(1.0+RSQ) 1270
122 AC=X(I)*PC(I)+AC 1280
    ORD1(II)=AC 1290
121 IW(II)=W*10.0+0.5 1300
C 1310
C IN THIS SECTION, ORDINATES OF THE GAUSS COMPONENT ARE EVALUATED. 1320
C 1330
C 1340
DO 221 II=1,NP 1350
    FII=II-1 1360
    W=WB-WI*FII 1370
    AC=0.0 1380
    DO 222 I=1,M 1390
        J=I+M 1400
        K=J+M 1410
        L=K+M 1420
        R=(W-X(J))*CAY*X(K) 1430
        PG(I)=R*R 1440
        IF (PG(I).LT.10.0) GO TO 223 1450
        PG(I)=0.0 1460
        GO TO 222 1470
223 PG(I)=EXP(-PG(I)) 1480
222 AC=X(L)*PG(I)+AC 1490
    IF (AC.LT.4.6) GO TO 221 1500
    AC=4.6 1510
221 ORD2(II)=AC 1520
C ***** OUTPUT SECTION ***** 1530
C 1540
C 1550
XN=X(N) 1560
WRITE (IPFNT,421) CAY 1570
IF (IXIT.EQ.1) GO TO 234 1580
WRITE (IPRNT,414) 1590
DO 236 I=1,NP 1600
    WW(I)=IW(I)*0.1 1610
236 SUM(I)=ORD1(I)+ORD2(I)+XN
```

```

WRITE (IPRNT,417) (WW(I),ORD1(I),ORD2(I),SUM(I),I=1,NP) 1620
WRITE (IPRNT,418) 1630
IF (IDECK.EQ.1) GO TO 32 1640
WRITE (IPCH,422) (WW(I),SUM(I),I=1,NP) 1650
GO TO 32 1660
234 WRITE (IPRNT,411) 1670
DO 237 I=1,NP 1680
SUM(I)=ORD1(I)+ORD2(I)+XN 1690
237 IT(I)=0.5+EXP(-SUM(I)*2.30258)*1000.0 1700
WRITE (IPRNT,412) (IW(I),IT(I),I=1,NP) 1710
WRITE (IPRNT,419) 1720
IF (IDECK.EQ.1) GO TO 32 1730
WRITE (IPCH,413) (IW(I),IT(I),I=1,NP) 1740
GO TO 32 1750
C 1760
400 FORMAT ('1PITHA AND JONES, INFRARED BAND FIT---COMPUTATION OF THE O 1770
ORDINATES OF CAUCHY-GAUSS BAND ENVELOPES. '/') 1780
401 FORMAT (20A4) 1790
402 FORMAT (6I5) 1800
403 FORMAT (2(4X,1H1),3I5) 1810
404 FORMAT (1X,20A4) 1820
405 FORMAT ('0',15X,4HX(1),17X,4HX(2),17X,4HX(3),17X,4HX(4)) 1830
406 FORMAT ('0',15X,4HX(1),17X,4HX(2),17X,4HX(3),17X,4HX(5)) 1840
407 FORMAT (4F15.5) 1850
408 FORMAT (1X,4(6X,F15.5)) 1860
409 FORMAT (4X,7HALPHA =,F8.5) 1870
410 FORMAT (10X,2HNP,I6,15X,2HNB,F8.1,11X,2HWI,F5.1) 1880
411 FORMAT ('0ORDINATES IN TRANSMITTANCE X 1000. ----- 1890
1----- '/') 1900
412 FORMAT (11(2X,I5,I4)) 1910
413 FORMAT (8(I5,I4,1X)) 1920
414 FORMAT ('0ORDINATES IN ABSORBANCE UNITS. ----- 1930
1----- '/') 1940
415 FORMAT (8(1X,F6.1,F6.3,2X)) 1950
416 FORMAT (6(F6.1,F6.3,1X)) 1960
417 FORMAT (4(3X,F6.1,3F6.3)) 1970
418 FORMAT ('0', 'CAUCHY, GAUSS, AND THE SUMMED ORDINATES ARE LISTED CON 1980
SECUTIVELY. ') 1990
419 FORMAT ('0THE SUMMED ORDINATES ONLY ARE LISTED. ') 2000
420 FORMAT ('0CALCULATIONS FOR THE PRODUCT FUNCTION. ') 2010
421 FORMAT ('0CALCULATIONS FOR THE SUM FUNCTION WITH CAY=',F4.2) 2020
422 FORMAT (6(F6.1,F6.3,1X)) 2030
END 2040

```


FITTA AND JONES, INFRARED BAND FIT---COMPUTATION OF THE ORDINATES OF CAUCHY-GAUSS BAND ENVELOPES.

MARCH 12TH, 1968. PROGRAM XIV (PC-122) MULTIPLE CURVE GENERATION.
 FOUR BAND TEST DECK FOR SUM FUNCTION. IXIT=1

X(1)	X(2)	X(3)	X(5)
0.20000	970.00000	0.20000	0.10000
0.40000	955.00000	0.20000	0.20000
0.10000	940.00000	0.10000	0.20000
0.25000	920.00000	0.20000	0.15000

ALPHA = 0.05000
 WP 200 NB 1000.0 WI 0.5

CALCULATIONS FOR THE SUM FUNCTION WITH CAY=0.80

ORDINATES IN TRANSMITTANCE X 1000. -----

1000 863	9995 862	9990 862	9985 861	9980 860	9975 859	9970 859	9965 858	9960 857	9955 856	9950 855
9945 854	9940 853	9935 851	9930 850	9925 849	9920 848	9915 846	9910 845	9905 843	9900 842	9895 840
9990 838	9885 836	9880 834	9875 832	9870 829	9865 827	9860 824	9855 821	9850 818	9845 814	9840 810
9835 806	9830 801	9825 796	9820 790	9815 783	9810 776	9805 767	9800 757	9795 746	9790 734	9785 720
9780 705	9775 688	9770 669	9765 649	9760 627	9755 605	9750 581	9745 556	9740 532	9735 507	9730 483
9725 461	9720 440	9715 423	9710 409	9705 400	9700 395	9695 394	9690 398	9685 405	9680 415	9675 427
9670 439	9665 452	9660 463	9655 473	9650 480	9645 484	9640 485	9635 482	9630 475	9625 464	9620 449
9615 431	9610 410	9605 386	9600 361	9595 335	9590 308	9585 283	9580 258	9575 236	9570 217	9565 201
9560 187	9555 180	9550 176	9545 176	9540 180	9535 188	9530 199	9525 212	9520 227	9515 244	9510 261
9505 278	9500 296	9495 312	9490 327	9485 340	9480 352	9475 362	9470 370	9465 376	9460 381	9455 384
9450 386	9445 387	9440 387	9435 387	9430 387	9425 386	9420 386	9415 386	9410 386	9405 387	9400 388
9395 391	9390 394	9385 397	9380 402	9375 407	9370 413	9365 420	9360 427	9355 435	9350 441	9345 452
9340 460	9335 469	9330 478	9325 486	9320 494	9315 502	9310 508	9305 514	9300 518	9295 521	9290 522
9285 521	9280 518	9275 512	9270 504	9265 494	9260 482	9255 467	9250 451	9245 434	9240 415	9235 397
9230 379	9225 361	9220 346	9215 334	9210 325	9205 320	9200 320	9195 324	9190 334	9185 348	9180 366
9175 383	9170 413	9165 440	9160 468	9155 497	9150 526	9145 554	9140 582	9135 608	9130 633	9125 657
9120 673	9115 697	9110 715	9105 730	9100 744	9095 756	9090 767	9085 776	9080 784	9075 791	9070 797
9065 803	9060 808	9055 812	9050 816	9045 820	9040 823	9035 826	9030 829	9025 831	9020 834	9015 836
9010 838	9005 840									

THE SUMMED ORDINATES ONLY ARE LISTED.

PIIHA AND JONES, INFRARED BAND FIT---COMPUTATION OF THE ORDINATES OF CAUCHY-GAUSS BAND ENVELOPES.

MARCH 12TH, 1968. PROGRAM XIV (PC-122) MULTIPLE CURVE GENERATION.
FOUR BAND TEST DECK FOR SUN FUNCTION. IIXIT=2

	X(1)	X(2)	X(3)	X(5)
	0.20000	970.00000	0.20000	0.10000
	0.40000	955.00000	0.20000	0.20000
	0.10000	940.00000	0.10000	0.20000
	0.25000	920.00000	0.20000	0.15000
ALPHA =	0.05000			
NP	200	WB 1000.0	WI 0.5	

CALCULATIONS FOR THE SUN FUNCTION WITH CAY=0.80

ORDINATES IN ABSORBANCE UNITS.

1000.0	0.014	0.000	0.064	999.5	0.014	0.000	0.064	999.0	0.015	0.000	0.065	998.5	0.015	0.000	0.065
998.0	0.015	0.000	0.065	997.5	0.016	0.000	0.066	997.0	0.016	0.000	0.066	996.5	0.017	0.000	0.067
996.0	0.017	0.000	0.067	995.5	0.018	0.000	0.068	995.0	0.018	0.000	0.068	994.5	0.019	0.000	0.069
994.0	0.019	0.000	0.069	993.5	0.020	0.000	0.070	993.0	0.020	0.000	0.070	992.5	0.021	0.000	0.071
992.0	0.022	0.000	0.072	991.5	0.022	0.000	0.072	991.0	0.023	0.000	0.073	990.5	0.024	0.000	0.074
990.0	0.025	0.000	0.075	989.5	0.026	0.000	0.076	989.0	0.027	0.000	0.077	988.5	0.028	0.000	0.078
988.0	0.029	0.000	0.079	987.5	0.030	0.000	0.080	987.0	0.031	0.000	0.081	986.5	0.032	0.000	0.083
986.0	0.034	0.000	0.084	985.5	0.035	0.000	0.086	985.0	0.037	0.000	0.087	984.5	0.039	0.000	0.089
984.0	0.041	0.001	0.091	983.5	0.043	0.001	0.094	983.0	0.045	0.001	0.096	982.5	0.047	0.002	0.099
982.0	0.050	0.003	0.102	981.5	0.053	0.003	0.106	981.0	0.056	0.005	0.110	980.5	0.059	0.006	0.115
980.0	0.063	0.008	0.121	979.5	0.067	0.010	0.127	979.0	0.072	0.013	0.134	978.5	0.077	0.016	0.143
978.0	0.083	0.019	0.152	977.5	0.089	0.024	0.163	977.0	0.096	0.029	0.174	976.5	0.104	0.034	0.188
976.0	0.113	0.040	0.202	975.5	0.122	0.046	0.218	975.0	0.133	0.053	0.236	974.5	0.145	0.060	0.255
974.0	0.158	0.067	0.274	973.5	0.172	0.073	0.295	973.0	0.186	0.080	0.316	972.5	0.201	0.086	0.337
972.0	0.215	0.091	0.356	971.5	0.229	0.095	0.374	971.0	0.240	0.098	0.388	970.5	0.248	0.100	0.398
970.0	0.252	0.101	0.404	969.5	0.253	0.101	0.404	969.0	0.251	0.100	0.400	968.5	0.245	0.097	0.393
968.0	0.238	0.094	0.382	967.5	0.230	0.090	0.370	967.0	0.221	0.086	0.357	966.5	0.213	0.082	0.345
966.0	0.206	0.078	0.334	965.5	0.201	0.075	0.325	965.0	0.197	0.072	0.319	964.5	0.195	0.070	0.315
964.0	0.194	0.070	0.314	963.5	0.196	0.071	0.317	963.0	0.199	0.074	0.323	962.5	0.205	0.079	0.333
962.0	0.212	0.086	0.347	961.5	0.221	0.094	0.365	961.0	0.233	0.104	0.387	960.5	0.247	0.116	0.413
960.0	0.264	0.129	0.442	959.5	0.283	0.143	0.475	959.0	0.304	0.157	0.511	958.5	0.327	0.172	0.549
958.0	0.352	0.186	0.588	957.5	0.377	0.200	0.627	957.0	0.401	0.213	0.664	956.5	0.423	0.225	0.697
956.0	0.440	0.234	0.725	955.5	0.452	0.242	0.744	955.0	0.456	0.248	0.753	954.5	0.452	0.251	0.753
954.0	0.441	0.252	0.744	953.5	0.425	0.251	0.726	953.0	0.404	0.248	0.702	952.5	0.380	0.244	0.674
952.0	0.355	0.238	0.644	951.5	0.331	0.232	0.613	951.0	0.308	0.225	0.583	950.5	0.287	0.218	0.555
950.0	0.269	0.211	0.529	949.5	0.252	0.204	0.506	949.0	0.237	0.199	0.486	948.5	0.224	0.194	0.468
948.0	0.214	0.190	0.453	947.5	0.204	0.187	0.441	947.0	0.197	0.185	0.432	946.5	0.190	0.184	0.424
946.0	0.185	0.184	0.419	945.5	0.181	0.185	0.415	945.0	0.177	0.186	0.413	944.5	0.174	0.188	0.412
944.0	0.172	0.190	0.412	943.5	0.170	0.192	0.412	943.0	0.169	0.194	0.413	942.5	0.167	0.196	0.413
942.0	0.166	0.198	0.414	941.5	0.165	0.199	0.414	941.0	0.163	0.200	0.413	940.5	0.162	0.201	0.412
940.0	0.160	0.201	0.411	939.5	0.158	0.200	0.408	939.0	0.156	0.199	0.405	938.5	0.153	0.197	0.401
938.0	0.151	0.195	0.396	937.5	0.148	0.192	0.390	937.0	0.145	0.189	0.384	936.5	0.142	0.185	0.377
936.0	0.139	0.181	0.369	935.5	0.136	0.176	0.362	935.0	0.133	0.171	0.353	934.5	0.130	0.165	0.345
934.0	0.127	0.160	0.337	933.5	0.125	0.154	0.329	933.0	0.123	0.148	0.321	932.5	0.121	0.142	0.313
932.0	0.119	0.137	0.306	931.5	0.118	0.131	0.299	931.0	0.118	0.126	0.294	930.5	0.118	0.121	0.269
930.0	0.118	0.117	0.286	929.5	0.120	0.114	0.283	929.0	0.121	0.111	0.282	928.5	0.124	0.109	0.283
928.0	0.127	0.109	0.286	927.5	0.131	0.109	0.291	927.0	0.137	0.111	0.297	926.5	0.143	0.113	0.306
926.0	0.150	0.117	0.317	925.5	0.159	0.121	0.330	925.0	0.169	0.126	0.345	924.5	0.180	0.132	0.363
924.0	0.193	0.138	0.381	923.5	0.207	0.145	0.401	923.0	0.221	0.151	0.422	922.5	0.236	0.156	0.442
922.0	0.250	0.161	0.461	921.5	0.263	0.164	0.477	921.0	0.273	0.166	0.489	920.5	0.279	0.167	0.495
920.0	0.280	0.165	0.495	919.5	0.276	0.163	0.489	919.0	0.268	0.158	0.476	918.5	0.256	0.152	0.456
918.0	0.242	0.144	0.436	917.5	0.225	0.136	0.411	917.0	0.208	0.126	0.384	916.5	0.191	0.115	0.357
916.0	0.175	0.105	0.330	915.5	0.160	0.094	0.304	915.0	0.147	0.083	0.279	914.5	0.134	0.072	0.256
914.0	0.123	0.062	0.235	913.5	0.113	0.053	0.216	913.0	0.104	0.045	0.198	912.5	0.096	0.037	0.183
912.0	0.098	0.030	0.169	911.5	0.082	0.025	0.157	911.0	0.076	0.020	0.146	910.5	0.071	0.016	0.137

910.0	0.066	0.012	0.128	909.5	0.062	0.009	0.121	909.0	0.058	0.007	0.115	908.5	0.055	0.005	0.110
908.0	0.052	0.004	0.106	907.5	0.049	0.003	0.102	907.0	0.046	0.002	0.098	906.5	0.044	0.002	0.095
906.0	0.042	0.001	0.093	905.5	0.040	0.001	0.090	905.0	0.038	0.001	0.088	904.5	0.036	0.000	0.086
904.0	0.034	0.000	0.085	903.5	0.033	0.000	0.083	903.0	0.031	0.000	0.082	902.5	0.030	0.000	0.080
902.0	0.029	0.000	0.079	901.5	0.028	0.000	0.078	901.0	0.027	0.000	0.077	900.5	0.026	0.000	0.076

CAUCHY, GAUSS, AND THE SUMMED ORDINATES ARE LISTED CONSECUTIVELY.

[Faint, illegible data table with multiple columns and rows, likely representing Cauchy, Gauss, and summed ordinates.]

PROGRAM XV

PROGRAM XV

Spectrum Subtraction and Band Fit Error Analysis Program

(PC-128)

This program can be used as a general purpose program to obtain difference spectra by subtracting the ordinates of one spectral curve from those of another. Should the two curves be the experimentally measured spectrum and the band envelope computed by one of the band fit optimization programs, the difference is the error spectrum, showing the mismatch of the calculated curve.

Two factors contribute to this mismatch; one is the true mismatch and the second is a random component resulting from the fact that the noise level on the calculated curve is low, being derived only from the round-off error, whereas the peak-to-peak noise level on the experimental curve will normally be of the order of 0.005 to 0.010 transmittance units. A method of separating these error components has been described in a previous publication (2) and is illustrated in Figs. 3-5 taken from simulation studies on part of the spectrum of cyclohexanone in carbon disulfide solution. These calculations which separate "true" misfit error from misfit error due to the greater random noise level on the experimentally measured curve are activated when NOISAN = 2.

When operating the program in this mode, both the experimental ordinates and the calculated ordinates are convolved with a five point quadratic smoothing function. Subtraction of the smoothed experimental curve from the unsmoothed experimental curve extracts the high-frequency noise elements, and this difference curve provides a measure of the mismatch contributed by the higher noise level of the experimental curve (Fig. 4). Subtraction of the smoothed calculated curve from the smoothed experimental curves (Fig. 5) gives a measure of the mathematical mismatch of the calculated curve, after allowance for noise. In doing this it is assumed that the smoothing convolution induces negligible distortion of the computed curve, or of the spectral band structure in the experimental curve.* Another example based on an

*It would be more correct to say that the effect of the smoothing function on these two curves is comparable, so that the difference curve is not significantly affected. If desired this distortion can be evaluated by subtracting the spectrum of the smoothed calculated curve from that of the unsmoothed calculated curve, but this is not incorporated in the program since previous studies have shown it is not necessary (see reference (10)).

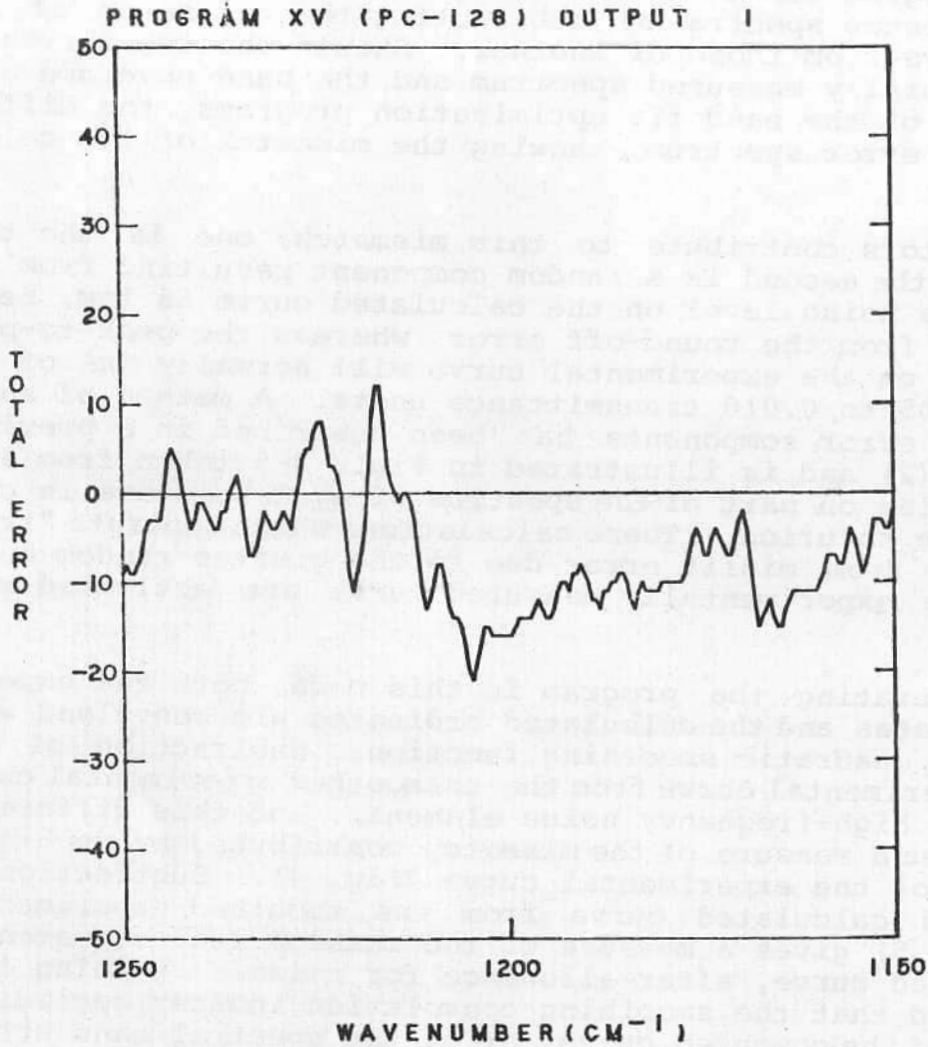


Fig. 3 Total error spectrum obtained by subtraction of the computed ordinates from the measured ordinates. The tabulated data are listed on p. 146.

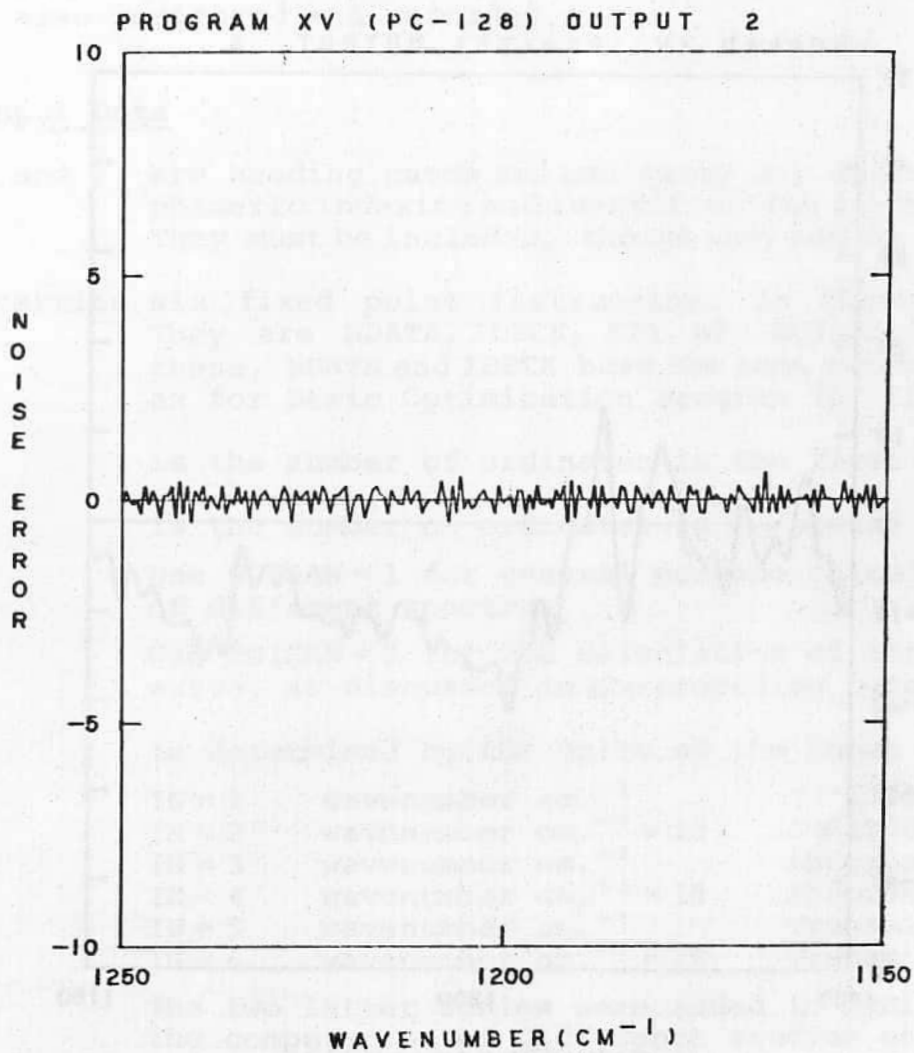


Fig. 4 High frequency noise error obtained by subtraction of the smoothed experimental ordinates from the measured experimental ordinates. The tabulated data are listed on p. 147.

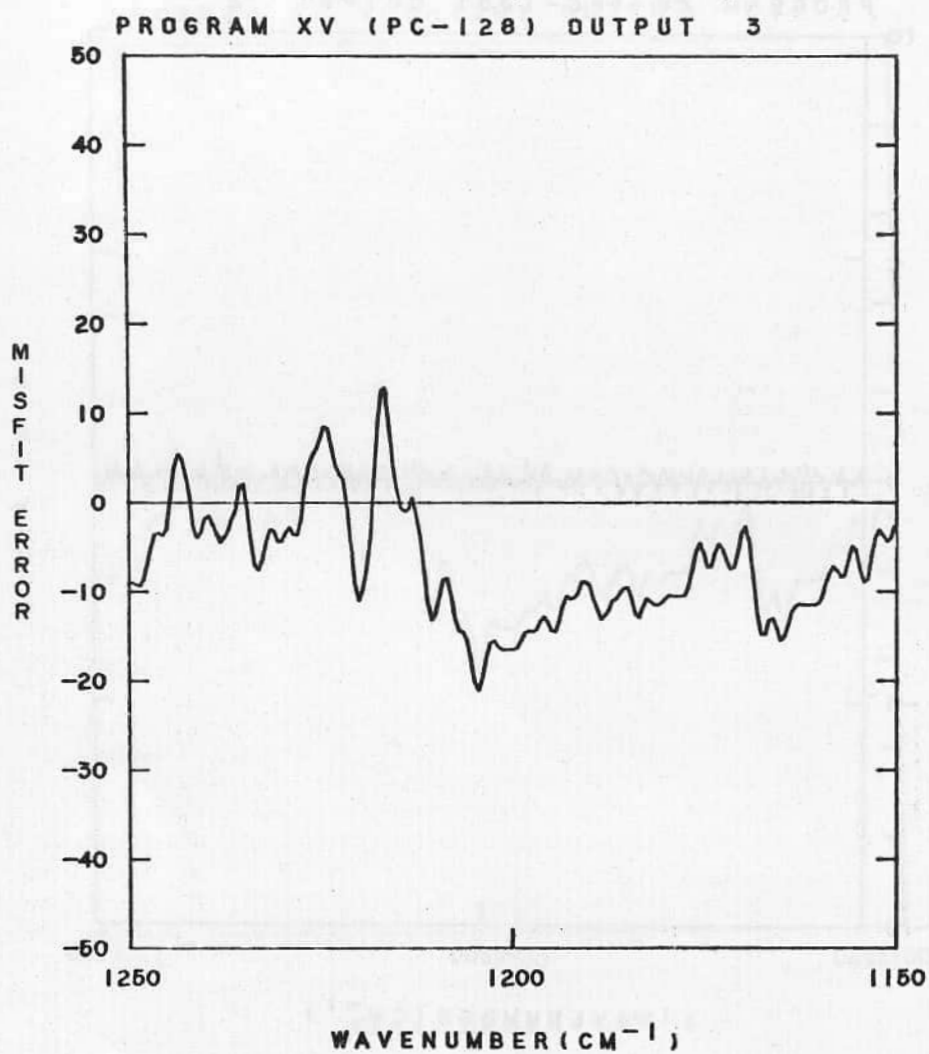


Fig. 5 "True" mismatch error obtained by subtraction of the smoothed computed ordinates from the smoothed measured ordinates. The tabulated data are listed on p. 148.

experimental curve with much higher noise level is given on p. 3045 of reference (2).

These statistical differences are also evaluated numerically in terms of the root-mean-square of the residuals (the discrepancy) and the algebraic sum of the residuals (the average); the ordinate value and the wavenumber of the maximum absolute residual is also monitored and recorded.

A. The Input Data

Cards 1 and 2 are heading cards and can carry any desired alphameric indexing and identification statements. They must be included, though they may be blank.

Card 3 carries six fixed point instructions in format 6I5. They are NDATA, IDECK, NP1, NP2, NOISAN, IN. Of these, NDATA and IDECK have the same connotation as for Basic Optimization Program (p. 11).

NP1 is the number of ordinates in the first curve.

NP2 is the number of ordinates in the second curve.

Use NOISAN = 1 for general purpose calculations of different spectra.

Use NOISAN = 2 for the calculation of the error curve, as discussed in the preceding paragraph.

IN is determined by the units of the input data:

IN = 1	wavenumber cm.^{-1}	$T \times 1000$
IN = 2	wavenumber $\text{cm.}^{-1} \times 10$	$T \times 1000$
IN = 3	wavenumber cm.^{-1}	Absorbance
IN = 4	wavenumber $\text{cm.}^{-1} \times 10$	Absorbance
IN = 5	wavenumber cm.^{-1}	Transmittance
IN = 6	wavenumber $\text{cm.}^{-1} \times 10$	Transmittance

The two latter scales were added to facilitate the computation of difference studies on first and second differential spectra which are discussed in Bulletin 11 in connection with Program IV.

Card 4 carries three floating point instructions in format 3F15.5.

WB1 is the starting wavenumber of the first curve in cm.^{-1} .

WB2 is the starting wavenumber of the second curve in cm.^{-1} .

WI is the constant wavenumber interval in cm.^{-1} . This is positive for a diminishing wavenumber sequence.

WB1 and WB2 must be chosen so that the absolute value of WB1-WB2 does not exceed $100 \times \text{WI}$.

Card Deck 5 is the data deck of the first spectrum consisting of NP1 points; the format depends on the value of IN and is listed in Table I of Bulletin 11.

Card 6 carries the fixed point instruction IXIT in format I5. IXIT determines the format of the output and is discussed in the following section.

Card Deck 7 is the data deck of the second spectrum consisting of NP2 points; the format depends on the value of IN, as for Card Deck 5. When operating in the error mode it is important that the experimental spectrum be listed as Card Deck 5 and the calculated spectrum as Card Deck 7.

B. Description of the Program

The six input formats have been summarized in the preceding section, they are under the control of IN. There are four output formats under the control of IXIT. In all cases the abscissal units are $\text{cm.}^{-1} \times 10$. With IXIT=1 the ordinates are direct ordinate differences in units of transmittance $\times 1000$. If IXIT=2 the ordinate differences are in absorbance units. With IXIT=3 the ordinate scale is transmittance normalized to make the maximum residual ± 1000 , while with IXIT=4 the ordinate range is adjusted so that all residuals lie between +200 and +800. This scale is useful for plotting purposes where the ordinate grid range is 0 to 1000 and the main interest is in the graphical display of the error curve. All four IXIT formats can be used for the general purpose recording of difference spectra, but only IXIT=1 and IXIT=3 are available in the error analysis mode.

The initial section of the program, ending at statement 125, is concerned with the input and reformulation of the data. All data are converted to $\text{cm.}^{-1} \times 10$ and transmittance $\times 1000$ prior to numerical analysis. Between statements 13 and 19 the starting wavenumber is adjusted to the spectrum beginning at the lower wavenumber. The consecutive abscissal data points on the two curves are then checked against one another. If a mismatch is

detected, SUBROUTINE SORT is called to monitor and correct both data decks. The two decks are again compared, and if a mismatch still exists the calculation is terminated. The program branches at the computed GO TO statement 45, in accordance with the selected value of IXIT. The ordinates are next subtracted, the residuals stored in the arrays IY3 and Y3, and the difference spectrum printed out; when operating under IXIT=3 or IXIT=4 the residuals are appropriately scaled in the sections beginning at statements 210 or 220 respectively. A punched card version is also obtained if IDECK=2.

If NOISAN=1 the program now terminates or returns to process another pair of data decks under the control of NDATA. If NOISAN=2 the error calculation routine is entered at statement 310. This mode requires that IXIT=1 or 3, the experimental and calculated ordinates are stored in units of transmittance $\times 1000$ in the fixed point arrays IY1 and IY2 respectively. They are first transferred to the floating point arrays Y1 and Y2 and convolved with a five point quadratic smoothing function (16,17) to yield the smoothed ordinates which are stored in the floating point arrays Y3 and Y4. The total error curve has already been evaluated and recorded before entering the error analysis routine. The noise component is Y1-Y3 and the noise corrected mismatch Y3-Y4. These are calculated in the DO loop ending at statement 311 and are stored in the arrays Y1 and Y2 respectively. The program branches following statement 311; if IXIT=1 it proceeds directly to calculate the statistical parameters AVE and DIS and output the tables of differences. If IXIT=3 it transfers to statement 350 and scales the ordinates to the range ± 1000 . The quantities AVE and DIS are always evaluated in transmittance units so that they can be compared directly with the corresponding quantities obtained in the band fit optimization programs.

C		10
C	*****	20
C	*	30
C	SPECTRUM SUBTRACTION AND BAND FIT	40
C	*	50
C	ERROR ANALYSIS PROGRAM.	60
C	*	70
C	*****	80
C		90
C	J. PITHA AND R. N. JONES, DIVISION OF CHEMISTRY, NATIONAL RESEARCH	100
C	COUNCIL OF CANADA, SUSSEX DRIVE, OTTAWA, CANADA.	110
C		120
C	PROGRAM XV (PC-128)	130
C		140
C	JULY 29TH. 1967	150
C		160
C	THIS IS A PROGRAM FOR SUBTRACTING ONE SPECTRUM FROM ANOTHER.	170
C		180
C	IN CURVE FITTING STUDIES IT CAN ALSO BE USED TO EVALUATE	190
C	THE ERROR BETWEEN THE REAL SPECTRUM AND THE COMPUTED BAND	200
C	ENVELOPE.	210
C		220
C	IT CONTAINS A BRANCH WHICH WILL SEPARATE THE ERROR COMPONENT	230
C	ORIGINATING IN THE NOISE ON THE REAL SPECTRUM FROM THE	240
C	MATHEMATICAL MISFIT OF THE SYNTHESIZED CURVE.	250
C		260
C	THE INPUT ABSCISSAL SCALE CAN BE EITHER CM.-1 OR CM.-1 X 10.	270
C	THE INPUT ORDINATES CAN BE TRANSMITTANCE, TRANSMITTANCE X 1000	280
C	OR ABSORBANCE. THE TRANSMITTANCE SCALE WAS ADDED TO FACILITATE	290
C	DIFFERENCE STUDIES ON FIRST AND SECOND DERIVATIVE SPECTRA	300
C	(COMPARE PROGRAM IV).	310
C		320
C	FOR THE ERROR ANALYSIS THE TRUE DATA SPECTRUM MUST PRECEED THE	330
C	CALCULATED SPECTRUM.	340
C		350
C	INPUT CONTROL	360
C	IN=1 X IN CM.-1 Y IN T X 1000.	370
C	IN=2 X IN CM.-1 X 10. Y IN T X 1000.	380
C	IN=3 X IN CM.-1 Y IN ABSORBANCE UNITS.	390
C	IN=4 X IN CM.-1 X 10. Y IN ABSORBANCE UNITS.	400
C	IN=5 X IN CM.-1 Y IN TRANSMITTANCE.	410
C	IN=6 X IN CM.-1 X 10. Y IN TRANSMITTANCE.	420
C		430
C	FOUR OUTPUT FORMATS ARE PROVIDED.	440
C	OUTPUT CONTROL	450
C	IXIT=1 X IN CM.-1 X 10. Y AS DIFFERENCE IN T X 1000.	460
C	IXIT=2 X IN CM.-1 Y AS DIFFERENCE IN ABSORBANCE.	470
C	IXIT=3 X IN CM.-1 X 10. Y AS RELATIVE DIFFERENCE IN	480
C	TRANSMITTANCE UNITS X 1000.	490
C	NORMALIZED FOR A MAXIMAL	500
C	VALUE OF + OR - 1000.	510
C	IXIT=4 X IN CM.-1 X 10. Y AS RELATIVE DIFFERENCE IN	520
C	TRANSMITTANCE UNITS X 1000.	530
C	NORMALIZED WITHIN THE RANGE	540
C	+200 TO +800.	

C		550
C	NOTE THAT THE SAME SCALES MUST BE USED FOR BOTH SPECTRA.	560
C		570
C	NOTE THAT FOR THE ERPOP ANALYSIS ONLY IEXIT=1 OR IEXIT=3 IS ALLOWED.	580
C		590
C	NOTE THAT THE IEXIT SPECIFICATION CARD IS INSERTED BETWEEN THE TWO	600
C	DATA DECKS. THIS IS A CONVENIENCE TO PREVENT THE OVER-RUN OF	610
C	DATA IN THE EVENT THAT NP1 HAS BEEN PUNCHED INCORRECTLY.	620
C		630
C	IT IS HELPFUL TO LIST IEXIT ON A CARD OF DIFFERENT COLOR.	640
C		650
C	THIS PROGRAM IS DIMENSIONED FOR 2000 DATA POINTS ON EACH CURVE.	660
C	THE INPUT WAVENUMBER SEQUENCES ARE CHECKED BY SUBROUTINE SORT AND	670
C	THE WAVENUMBER SCALES ALIGNED.	680
C	FOR DETAILS SEE N.R.C.C. BULLETIN NO. 12.	690
C		700
C	DIMENSION IX1(2000),IX2(2000),X1(2000),X2(2000),Y1(2000),Y2(2000),	710
C	Y3(2000),Y4(2000),IY1(2000),IY2(2000),IY3(2000),HEAD1(20),HEAD2(20	720
C	2)	730
C	EQUIVALENCE (X1(1),IX2(1),Y3(1)),(X2(1),IY3(1),Y4(1))	740
C	IRD=1	750
C	IPCH=2	760
C	IPRNT=3	770
C	10 WRITE (IPRNT,400)	780
C	READ (IRD,401) HEAD1	790
C	READ (IRD,401) HEAD2	800
C	READ (IRD,402) NDATA,IDECK,NP1,NP2,NOISAN,IN	810
C		820
C	USE NOISAN=1 FOR SIMPLE CURVE SUBTRACTION AND NOISAN=2 FOR	830
C	BAND FIT ERROR ANALYSIS.	840
C	READ (IRD,403) WB1,WB2,WI	850
C		860
C	NOTE THAT THE STARTING WAVENUMBER OF EACH CURVE (WB1),(WB2) AND	870
C	THE NUMBER OF POINTS ON EACH CURVE (NP1,NP2) MUST BE GIVEN.	880
C	THE STARTING WAVENUMBERS FOR THE TWO DECKS MUST AGREE WITHIN ONE	890
C	HUNDRED TIMES THE WAVENUMBER INTERVAL.	900
C	11 GO TO (100,12,110,120,110,120),IN	910
C	12 READ (IRD,404) (IX1(I),IY1(I),I=1,NP1)	920
C	READ (IRD,402) IEXIT	930
C	READ (IRD,404) (IX2(I),IY2(I), I=1,NP2)	940
C	GO TO 13	950
C		960
C	100 READ (IRD,425) (X1(I),IY1(I),I=1,NP1)	970
C	READ (IRD,402) IEXIT	980
C	READ (IRD,425) (X2(I),IY2(I),I=1,NP2)	990
C	DO 101 I=1,NP1	1000
C	101 IX1(I)=X1(I)*10.0+0.5	1010
C	DO 102 I=1,NP2	1020
C	102 IX2(I)=X2(I)*10.0+0.5	1030
C	GO TO 13	1040
C		1050
C	110 READ (IRD,426) (X1(I),Y1(I),I=1,NP1)	1060
C	READ (IRD,402) IEXIT	1070
C	READ (IRD,426) (X2(I),Y2(I),I=1,NP2)	1080

	IF (IN.EQ.5) GO TO 113	1090
	DO 111 I=1, NP1	1100
	IX1(I)=X1(I)*10.0+0.5	1110
111	IY1(I)=EXP(-2.30258*Y1(I))*1000.0+0.5	1120
	DO 112 I=1, NP2	1130
	IX2(I)=X2(I)*10.0+0.5	1140
112	IY2(I)=EXP(-2.30258*Y2(I))*1000.0+0.5	1150
	GO TO 13	1160
113	DO 114 I=1, NP1	1170
	IX1(I)=X1(I)*10.0+0.5	1180
114	IY1(I)=Y1(I)*1000.0+0.5	1190
	DO 115 I=1, NP2	1200
	IX2(I)=X2(I)*10.0+0.5	1210
115	IY2(I)=Y2(I)*1000.0+0.5	1220
	GO TO 13	1230
C		1240
120	READ (IRD,420) (IX1(I),Y1(I),I=1, NP1)	1250
	READ (IRD,402) IXIT	1260
	READ (IRD,420) (IX2(I),Y2(I),I=1, NP2)	1270
	IF (IN.EQ.6) GO TO 123	1280
	DO 121 I=1, NP1	1290
121	IY1(I)=EXP(-2.30218*Y1(I))*1000.0+0.5	1300
	DO 122 I=1, NP2	1310
122	IY2(I)=EXP(-2.30218*Y2(I))*1000.0+0.5	1320
	GO TO 13	1330
123	DO 124 I=1, NP1	1340
124	IY1(I)=Y1(I)*1000.0+0.5	1350
	DO 125 I=1, NP2	1360
125	IY2(I)=Y2(I)*1000.0+0.5	1370
C		1380
13	IF (WB2.GT.WB1) GO TO 14	1390
	WB=WB2	1400
	GO TO 15	1410
14	WB=WB1	1420
15	IF (NP2.LE.NP1) GO TO 17	1430
	NP=NP1	1440
	GO TO 18	1450
17	NP=NP2	1460
18	IF (IDECK.EQ.1) GO TO 19	1470
	WRITE (IPCH,401) HEAD1	1480
	WRITE (IPCH,401) HEAD2	1490
19	WRITE (IPRNT,405) HEAD1	1500
	WRITE (IPRNT,405) HEAD2	1510
	WRITE (IPRNT,406) NP,WB,WI	1520
C		1530
C	IN THIS SECTION THE WAVENUMBER SEQUENCES OF THE TWO CARD DECKS ARE	1540
C	CHECKED AGAINST ONE ANOTHER. IF A MISMATCH IS DETECTED, EACH	1550
C	CARD DECK IS SEQUENCED BY THE SUBROUTINE SORT. THE TWO DECKS	1560
C	ARE RECHECKED AGAINST EACH OTHER AND IF ANY INCONSISTANCY	1570
C	REMAINS THE COMPUTATION IS TERMINATED.	1580
C		1590
	IWI=WI*10.0+0.5	1600
	IWB=WB*10.0+0.5	1610
	K2=1	1620

21	IF (IX1(K2)-IWB) 22,23,24	1630
22	WRITE (IPRNT,4C7)	1640
32	IF (NDATA.EQ.2) GO TO 10	1650
	STOP	1660
24	IF (K2.GT.100) GO TO 22	1670
	K2=K2+1	1680
	GO TO 21	1690
23	IF (K2.EQ.1) GO TO 28	1700
	DO 30 I=1,NP	1710
	IX1(I)=IX1(K2)	1720
	IY1(I)=IY1(K2)	1730
30	K2=K2+1	1740
	WRITE (IPRNT,4C8)	1750
28	K2=1	1760
35	IF (IX2(K2)-IWB) 31,36,33	1770
31	WRITE (IPRNT,4C9)	1780
	GO TO 32	1790
33	IF (K2.GT.100) GO TO 31	1800
	K2=K2+1	1810
	GO TO 35	1820
36	IF (K2.EQ.1) GO TO 40	1830
	DO 39 I=1,NP	1840
	IX2(I)=IX2(K2)	1850
	IY2(I)=IY2(K2)	1860
39	K2=K2+1	1870
	WRITE (IPRNT,410)	1880
40	ISKIP=1	1890
50	DO 44 I=1,NP	1900
	IF (IX1(I).NE.IX2(I)) GO TO 45	1910
44	CONTINUE	1920
46	MAX=0	1930
	AMAY=0.0	1940
	SUM=0.0	1950
	DIS=0.0	1960
	GO TO (160,200,210,210),IXIT	1970
45	IF (ISKIP.EQ.2) GO TO 47	1980
	WRITE (IPRNT,411)	1990
	CALL SORT4 (IX1,IY1,WB,WI,NP,IPRNT,KLENUP,IWB,IWI)	2000
	IF (KLENUP.EQ.2) GO TO 32	2010
	WRITE (IPRNT,412)	2020
	WRITE (IPRNT,413)	2030
	CALL SORT4 (IX2,IY2,WB,WI,NP,IPRNT,KLENUP,IWB,IWI)	2040
	IF (KLENUP.EQ.2) GO TO 32	2050
	WRITE (IPRNT,414)	2060
	ISKIP=2	2070
	GO TO 50	2080
47	WRITE (IPRNT,415)	2090
	GO TO 32	2100
		2110
	** EVALUATION OF THE DIFFERENCE IN UNITS OF TRANSMITTANCE X 1000.	2120
		2130
C		2140
C	160 WRITE (IPRNT,416)	2150
C	DO 161 I=1,NP	2160
	IY3(I)=IY1(I)-IY2(I)	

	YY=FLOAT (IY3 (I))	2170
	IF (ABS (YY) .LE. ABS (AMAY)) GO TO 162	2180
	AMAY=YY	2190
	MAX=IX1 (I)	2200
162	SUM=SUM+YY	2210
161	DIS=DIS+YY*YY	2220
163	AVE=0.001*SUM/NP	2230
	DIS=0.000001*DIS/NP	2240
	DIS=SQRT (DIS)	2250
	AMAX=MAX*0.1	2260
	AMAY=0.001*AMAY	2270
164	IF (IDECK.EQ.1) GO TO 165	2280
	WRITE (IPCH,404) (IX1 (I), IY3 (I), I=1, NP)	2290
165	WRITE (IPRNT,436)	2300
	WRITE (IPRNT,419) (IX1 (I), IY3 (I), I=1, NP)	2310
	WRITE (IPRNT,417) AVE, DIS, AMAX, AMAY	2320
	WRITE (IPRNT,434)	2330
	GO TO 300	2340
C		2350
C	***** EVALUATION OF THE DIFFERENCES IN ABSORBANCE UNITS *****	2360
C		2370
200	WRITE (IPRNT,419)	2380
	DO 202 I=1, NP	2390
	YY=ALOG10 (FLOAT (IY2 (I))) -ALOG10 (FLOAT (IY1 (I)))	2400
	Y3 (I)=YY	2410
	IF (ABS (YY) .LE. ABS (AMAY)) GO TO 201	2420
	AMAY=YY	2430
	MAX=IX1 (I)	2440
201	SUM=SUM+YY	2450
202	DIS=DIS+YY*YY	2460
	AVE=SUM/NP	2470
	DIS=DIS/NP	2480
	DIS=SQRT (DIS)	2490
	AMAX=MAX*0.1	2500
	IF (KLENUM.EQ.1) GO TO 204	2510
	DO 205 I=1, NP	2520
	X2 (I)=IX1 (I)*0.1	2530
205	CONTINUE	2540
204	IF (IDECK.EQ.1) GO TO 203	2550
	WRITE (IPCH,420) (X2 (I), Y3 (I), I=1, NP)	2560
203	WRITE (IPRNT,436)	2570
	WRITE (IPRNT,421) (X2 (I), Y3 (I), I=1, NP)	2580
	WRITE (IPRNT,417) AVE, DIS, AMAX, AMAY	2590
	WRITE (IPRNT,435)	2600
	GO TO 300	2610
C		2620
C	***** EVALUATION OF NORMALIZED TRANSMITTANCE DIFFERENCES WITH THE	2630
C	MAXIMUM OR MINIMUM = 1000. *****	2640
C		2650
210	NMIN=100	2660
	NMAX=-100	2670
	DO 211 I=1, NP	2680
	IY3 (I)=IY1 (I)-IY2 (I)	2690
	NMIN=MINO (NMIN, IY3 (I))	2700

```
211 NMAX=MAX0(NMAX,IY3(I)) 2710
    IF (IXIT.EQ.4) GO TO 220 2720
    WRITE (IPRNT,422) 2730
    IF ((NMAX+NMIN).GT.0) GO TO 213 2740
    SLOPE =-1000.0/NMIN 2750
    GO TO 214 2760
213 SLOPE=1000.0/NMAX 2770
214 DO 216 I=1,NP 2780
    YY=FLOAT(IY3(I)) 2790
    IF (ABS(YY).LE.ABS(AMAY)) GO TO 215 2800
    MAX=IX1(I) 2810
    AMAY=YY 2820
215 SUM=SUM+YY 2830
    DIS=DIS+YY*YY 2840
216 IY3(I)=IY3(I)*SLOPE 2850
    GO TO 163 2860
C 2870
C ***** EVALUATION OF TRANSMITTANCE DIFFERENCES NORMALIZED TO A 2880
C SCALE OF + 200 TO + 800. ***** 2890
C THIS ORDINATE RANGE IS CONVENIENT FOR PLOTTING DIFFERENCE SPECTRA 2900
C FOR VISUAL DISPLAY ON A GRID SCALED FROM ZERO TO 1000. 2910
C 2920
C 2930
220 WRITE (IPRNT,423) 2940
    SLOPE=600.0/(NMAX-NMIN) 2950
    CEPT=200.5-SLOPE*NMIN 2960
    WRITE (IPRNT,424) NP,NMIN,NMAX,CEPT,SLOPE 2970
    DO 230 I=1,NP 2980
    YY=FLOAT(IY3(I)) 2990
    IF (ABS(YY).LE.ABS(AMAY)) GO TO 221 3000
    MAX=IX1(I) 3010
    AMAY=YY 3020
221 SUM=SUM+YY 3030
    DIS=DIS+YY*YY 3040
230 IY3(I)=CEPT+SLOPE*IY3(I) 3050
    GO TO 163 3060
C 3070
C ***** ERROR ANALYSIS ***** 3080
C BOTH THE EXPERIMENTAL AND THE CALCULATED CURVES ARE SMOOTHED 3090
C WITH A FIVE POINT QUADRATIC CONVOLUTE FUNCTION. 3100
C THE HIGH FREQUENCY COMPONENTS ELIMINATED FROM THE TRUE CURVE BY 3110
C SMOOTHING ARE OBTAINED FROM THE ORDINATE DIFFERENCES IN THE 3120
C TRUE CURVE BEFORE AND AFTER SMOOTHING. THESE ARE EQUATED WITH 3130
C THE NOISE ERROR. 3140
C THE NOISE-CORRECTED CURVE MISFIT ERROR IS EQUATED WITH THE 3150
C DIFFERENCE BETWEEN THE TRUE AND CALCULATED CURVES AFTER EACH 3160
C HAS BEEN SUBJECTED TO THE SMOOTHING ROUTINE.FOR A GRAPHICAL 3170
C ILLUSTRATION AND DISCUSSION SEE CANADIAN J.CHEM. FIG.7 3180
C PAGE 3045 VOL.44 (1966). 3190
C 3200
300 IF (NOISAN.EQ.1) GO TO 32 3210
    ISKIP = 1 3220
    GO TO (310,305,310,305),IXIT 3230
305 WRITE (IPRNT,427) 3240
```

	GO TO 32	3250
	NNP=NP-2	3260
310	DO 311 I=3,NNP	3270
	IYS=-3*(IY1(I-2)+IY1(I+2))+12*(IY1(I-1)+IY1(I+1))+17*IY1(I)	3280
	Y3(I)=C.285714E-1*IYS	3290
	IYS=-3*(IY2(I-2)+IY2(I+2))+12*(IY2(I-1)+IY2(I+1))+17*IY2(I)	3300
	Y4(I)=0.285714E-1*IYS	3310
	Y1(I)=IY1(I)	3320
	Y2(I)=IY2(I)	3330
	Y1(I)=Y1(I)-Y3(I)	3340
	Y2(I)=Y3(I)-Y4(I)	3350
311	CONTINUE	3360
321	MAX=0	3370
	AMAY=0.0	3380
	SUM=0.0	3390
	DIS=0.0	3400
	IF (IXIT.EQ.3) GO TO 350	3410
	DO 325 I=3,NNP	3420
	YY=Y1(I)	3430
	IF (ABS(YY).LE.ABS(AMAY)) GO TO 322	3440
	AMAY=YY	3450
	MAX = IX1(I)	3460
322	SUM=SUM+YY	3470
325	DIS=DIS+YY*YY	3480
	AVE=0.001*SUM/NNP	3490
	DIS=0.000001*DIS/NNP	3500
	DIS=SQRT(DIS)	3510
	AMAX=MAX*0.1	3520
	AMAY=0.001*AMAY	3530
	GO TO (330,340),ISKIP	3540
330	WRITE (IPRNT,428)	3550
	WRITE (IPRNT,438)	3560
	WRITE (IPRNT,437) (IX1(I),Y1(I),I=3,NNP)	3570
	WRITE (IPRNT,417) AVE,DIS,AMAX,AMAY	3580
	IF (IDECK.EQ.1) GO TO 333	3590
	WRITE (IPCH,432)	3600
	WRITE (IPCH,439) (IX1(I),Y1(I),I=3,NNP)	3610
333	ISKIP=2	3620
	DO 334 I=3,NNP	3630
334	Y1(I)=Y2(I)	3640
	GO TO 321	3650
340	WRITE (IPRNT,429)	3660
	WRITE (IPRNT,438)	3670
	WRITE (IPRNT,437) (IX1(I),Y2(I),I=3,NNP)	3680
	WRITE (IPRNT,417) AVE,DIS,AMAX,AMAY	3690
	IF (IDECK.EQ.1) GO TO 32	3700
	WRITE (IPCH,433)	3710
	WRITE (IPCH,439) (IX1(I),Y2(I),I=3,NNP)	3720
	GO TO 32	3730
		3740
C	**** ERFOR ANALYSIS WITH NORMALIZATION OF MAX.ORDINATE = 1000. ***	3750
C		3760
C		3770
350	DO 356 I=3,NNP	3780
	YY=Y1(I)	

	IF (ABS (YY) .LE. ABS (AMAY)) GO TO 355	3790
	AMAY=YY	3800
	MAX=IX1 (I)	3810
355	SUM=SUM+YY	3820
	DIS=DIS+YY*YY	3830
356	IY1 (I) =Y1 (I) *SLOPE+0.5	3840
	AVE=0.001*SUM/NNP	3850
	DIS=0.000001*DIS/NNP	3860
	DIS=SQRT (DIS)	3870
	AMAX=MAX*C.1	3880
	AMAY=0.001*AMAY	3890
	GO TO (360,370),ISKIP	3900
360	WRITE (IPENT,430)	3910
	WRITE (IPRNT,418) (IX1 (I), IY1 (I), I=3, NNP)	3920
	WRITE (IPRNT,417) AVE,DIS,AMAX,AMAY	3930
	IF (IDECK.EQ.1) GO TO 365	3940
	WRITE (IPCH,432)	3950
	WRITE (IPCH,404) (IX1 (I), IY1 (I), I=3, NNP)	3960
365	GO TO (361,370),ISKIP	3970
361	ISKIP=2	3980
	DO 363 I=3, NNP	3990
363	Y1 (I) =Y2 (I)	4000
	MAX=0	4010
	AMAY=0.0	4020
	SUM=0.0	4030
	DIS=0.0	4040
	GO TO 350	4050
370	WRITE (IPRNT,431)	4060
	WRITE (IPRNT,418) (IX1 (I), IY1 (I), I=3, NNP)	4070
	WRITE (IPRNT,417) AVE,DIS,AMAX,AMAY	4080
	IF (IDECK.EQ.1) GO TO 32	4090
	WRITE (IPCH,433)	4100
	WRITE (IPCH,404) (IX1 (I), IY1 (I), I=3, NNP)	4110
	GO TO 32	4120
C		4130
400	FORMAT ('1PITHA AND JONES,BAND FIT ERROR ANALYSIS AND CURVE SUBTRA 1CTION. '/')	4140
401	FORMAT (20A4)	4150
402	FORMAT (6I5)	4160
403	FORMAT (3F15.5)	4170
404	FORMAT (8 (I5,I4,1X))	4180
405	FORMAT (1X,20A4)	4190
406	FORMAT ('0',10X,2HNP,I5,15X,2HNB,F8.1,11X,2HWI,F5.1)	4200
407	FORMAT ('0ERROR IN STARTING WAVENUMBER OF FIRST CURVE.')	4210
408	FORMAT ('0STARTING WAVENUMBER OF FIRST CURVE ADJUSTED.')	4220
409	FORMAT ('0ERROP IN STARTING WAVENUMBER OF SECOND CURVE.')	4230
410	FORMAT ('0STARTING WAVENUMBER OF SECOND CURVE ADJUSTED.')	4240
411	FORMAT ('0FIRST CARD DECK.')	4250
412	FORMAT ('0FIRST CARD DECK HAS BEEN CHFCKED.')	4260
413	FORMAT ('0SECOND CARD DECK.')	4270
414	FORMAT ('0SECOND CARD DECK HAS BEEN CHECKED.')	4280
415	FORMAT ('0SUBROUTINE SORT HAS FAILED TO ALIGN THE INPUT DATA.')	4290
416	FORMAT ('0CORDINATES ARE ABSOLUTE TRANSMITTANCE X 1000'/)	4300
417	FORMAT (//5X,9HAVERAGE =,E13.5,5X,13HDISCREPANCE =,E13.5,5X,7HMAX	4310
		4320

```
1X =,F7.1,5X,7HMAX Y =,F8.5/) 4330
418 FORMAT (9(4X,2I5)) 4340
419 FORMAT ('COORDINATES ARE ABSORBANCE DIFFERENCES.'/) 4350
420 FORMAT (6(F6.1,F6.3,1X)) 4360
421 FORMAT (9(1X,F6.1,F7.3)) 4370
422 FORMAT ('COORDINATES NORMALIZED TO MAX.ERROR=1000.'/) 4380
423 FORMAT ('COORDINATES NORMALIZED TO RANGE +800 TO +200'/) 4390
424 FORMAT (10X,3HNP=,I5,5X,5HMIN=,I5,5X,5HMAX=,I5,5X,5HCEPT=,F6.2, 4400
15X,6HSLOPE=,F6.2) 4410
425 FORMAT (7(F6.1,I4,1X)) 4420
426 FORMAT (6(F6.1,F6.3,1X)) 4430
427 FORMAT ('ERROR ANALYSIS DOES NOT OPERATE ON THIS ORDINATE SCALE.' 4440
1/) 4450
428 FORMAT ('1 NOISE ERROR.-----' 4460
1----- '/') 4470
429 FORMAT ('1 CURVE MISFIT ERROR.-----' 4480
1----- '/') 4490
430 FORMAT ('1 NOISE ERROR ON SCALE OF MAX.TOTAL ERROR = 1000.-----' 4500
1----- '/') 4510
431 FORMAT ('1 CURVE MISFIT ERROR ON SCALE OF MAX. TOTAL ERROR = 1000.' 4520
1----- '/') 4530
432 FORMAT ('NOISE ERROR COMPONENT') 4540
433 FORMAT ('NOISE CORRECTED CURVE MISFIT ERROR') . 4550
434 FORMAT (/5X,'AVERAGE,DISCREPANCE,AND MAX Y ARE IN UNITS OF TRANSMI 4560
TTANCE.') 4570
435 FORMAT (/5X,'AVERAGE,DISCREPANCE,AND Y MAX ARE IN ABSORBANCE UNITS 4580
1.') 4590
436 FORMAT (//' DIFFERENCE SPECTRUM. -----' 4600
1----- '/') 4610
437 FORMAT (8(2X,I5,1X,F6.1)) 4620
438 FORMAT ('COORDINATES ARE ABSOLUTE TRANSMITTANCE X 1000.0'/) 4630
439 FORMAT (6(I5,F7.2,1X)) 4640
END 4650
```

```
C 4660
C ***** 4670
SUBROUTINE SOFT4 (IX,IY,WB,WI,NP,IPRNT,KLENUP,IWB,IWI) 4680
C 4690
SUBROUTINE SOFT CHECKS FOR ERRORS IN THE INPUT WAVENUMBER DATA. 4700
C A LIMITED NUMBER OF WAVENUMBER SEQUENCE ERRORS ARE CORRECTED 4710
C BUT SEQUENCE ERRORS IN EXCESS OF 160 DATA POINTS (20 CARDS) 4720
C OR ANY OTHER TYPE OF WAVENUMBER ERROR WILL TERMINATE THE 4730
C COMPUTATION,AS ALSO WILL A DISCREPANCY BETWEEN IWB AND THE 4740
C STARTING WAVENUMBER. 4750
C THE WAVENUMBER POSITIONS OF THE CORRECTIONS AND OF A TERMINATING 4760
C ERROR ARE RECORDED. 4770
C IF CORRECTIONS ARE MADE THE CORRECTED INPUT DATA ARE LISTED IN FUL 4780
C IF A TERMINATING ERROR IS FOUND THE UNCORRECTED INPUT DATA ARE 4790
C LISTED IN FULL. 4800
C DIMENSION IX(2000),IY(2000),ITEMPX(160),X1(160),ITEMPY(160) 4810
C MM=1 4820
C DO 11 I=2,NP 4830
C IW=IWB-IWI*(I-1) 4840
C IF (IW.EQ.IX(I)) GO TO 11 4850
C XX=IX(I) 4860
C TEST=(WB-0.1*XX)/WI 4870
C NTEST=TEST+0.005 4880
C IF (ABS(TEST-NTEST).GT.0.005) GO TO 12 4890
C ITEMPIX(MM)=IX(I) 4900
C ITEMPY(MM)=IY(I) 4910
C MM=MM+1 4920
C IF (MM.GT.160) GO TO 13 4930
11 CONTINUE 4940
C IF (MM.GT.1) GO TO 14 4950
C WRITE (IPRNT,451) 4960
15 KLENUP=1 4970
C RETURN 4980
12 XX1=IX(I-1)*0.1-WI 4990
C WRITE (IPRNT,452) XX1 5000
16 KLENUP=2 5010
C RETURN 5020
13 WRITE (IPRNT,453) 5030
C WRITE (IPRNT,455) (IX(I),IY(I), I=1,NP) 5040
C GO TO 16 5050
14 NN=MM-1 5060
C DO 17 MM=1,NN 5070
C K1=1+(IWB-ITEMPIX(MM))/IWI 5080
C IX(K1)=ITEMPIX(MM) 5090
C IY(K1)=ITEMPY(MM) 5100
17 X1(MM)=IX(K1)*0.1 5110
C WRITE (IPRNT,450) (X1(MM), MM=1,NN) 5120
C WRITE (IPRNT,454) (IX(I),IY(I),I=1,NP) 5130
C GO TO 15 5140
C 5150
450 FORMAT ('OWAVENUMBER CORRECTIONS AT',/ ,12(2X,F6.1,2X)) 5160
451 FORMAT ('ONO ERRORS. ') 5170
452 FORMAT ('OTERMINATED BY EPROR AT',F6.1,6H CM-1.) 5180
453 FORMAT ('OTERMINATED BY MULTIPLE WAVENUMBER SEQUENCE ERRORS. ') 5190
```

```
454 FORMAT ('OREAPEANGED INPUT.'//,9(4X,2I5))
455 FORMAT ('OUNCORRECTED INPUT.'//,9(4X,2I5))
END
```

5200
5210
5220

UNRECORDED DATA ON THIS TAP - CHECK FOR TAP POSITION AND DATE

FILE NAME: DATE:

RECORDED AND RECORDED INFORMATION:

NO.	DATE	TIME	TYPE	NO.	DATE	TIME	TYPE	NO.	DATE	TIME	TYPE
1	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
2	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
3	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
4	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
5	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
6	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
7	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
8	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
9	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
10	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
11	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
12	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
13	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
14	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
15	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
16	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
17	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
18	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
19	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
20	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
21	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
22	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
23	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
24	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
25	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
26	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
27	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
28	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
29	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
30	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
31	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
32	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
33	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
34	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
35	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
36	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
37	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
38	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
39	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
40	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
41	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
42	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
43	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
44	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
45	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
46	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
47	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
48	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
49	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00
50	1954	12:00	1	1954	12:00	1	1954	12:00	1	1954	12:00

RECORDED ON 12/11/54 12:00 PM

UNRECORDED ON 12/11/54 12:00 PM

PITHA AND JONES, BAND FIT ERROR ANALYSIS AND CURVE SUBTRACTION.

APRIL 28TH 1969 PROGRAM IV (PC-128) IXIT=1 NOISAN=2
TEST RUN ON CYCLOHEXANONE SPECTRUM AS COMPUTED BY THE PRODUCT FUNCTION.

MP 208 NB 1251.0 WI 0.5

ORDINATES ARE ABSOLUTE TRANSMITTANCE X 1000

DIFFERENCE SPECTRUM. -----

12510	-9	12505	-9	12500	-9	12495	-8	12490	-9	12485	-9	12480	-8	12475	-7	12470	-4
12465	-3	12460	-3	12455	-3	12450	-3	12445	0	12440	4	12435	5	12430	4	12425	3
12420	0	12415	-2	12410	-4	12405	-3	12400	-1	12395	-1	12390	-2	12385	-3	12380	-4
12375	-4	12370	-2	12365	-2	12360	0	12355	1	12350	2	12345	0	12340	-4	12335	-7
12330	-7	12325	-6	12320	-4	12315	-2	12310	-3	12305	-4	12300	-4	12295	-3	12290	-2
12295	-3	12280	-4	12275	-1	12270	1	12265	4	12260	5	12255	5	12250	7	12245	6
12240	8	12235	6	12230	3	12225	3	12220	2	12215	0	12210	-4	12205	-9	12200	-11
12195	-4	12190	-7	12185	-4	12180	2	12175	9	12170	12	12165	12	12160	8	12155	3
12150	1	12145	0	12140	-1	12135	0	12130	0	12125	-1	12120	-3	12115	-7	12110	-11
12105	-13	12100	-12	12095	-10	12090	-8	12085	-8	12080	-10	12075	-13	12070	-14	12065	-14
12060	-15	12055	-17	12050	-20	12045	-21	12040	-19	12035	-17	12030	-15	12025	-15	12020	-16
12015	-16	12010	-16	12005	-16	12000	-16	11995	-16	11990	-15	11985	-14	11980	-14	11975	-14
11970	-14	11965	-13	11960	-12	11955	-13	11950	-14	11945	-14	11940	-13	11935	-11	11930	-10
11925	-10	11920	-11	11915	-9	11910	-9	11905	-8	11900	-9	11895	-10	11890	-12	11885	-12
11890	-13	11875	-11	11870	-11	11865	-10	11860	-10	11855	-9	11850	-9	11845	-10	11840	-12
11835	-13	11830	-11	11825	-10	11820	-11	11815	-11	11810	-11	11805	-11	11800	-10	11795	-10
11790	-10	11785	-10	11780	-10	11775	-10	11770	-9	11765	-7	11760	-5	11755	-4	11750	-5
11745	-7	11740	-7	11735	-5	11730	-4	11725	-5	11720	-6	11715	-7	11710	-7	11705	-5
11700	-3	11695	-2	11690	-4	11685	-8	11680	-12	11675	-15	11670	-14	11665	-13	11660	-12
11655	-14	11650	-15	11645	-15	11640	-13	11635	-12	11630	-11	11625	-11	11620	-11	11615	-11
11610	-11	11605	-11	11600	-11	11595	-10	11590	-9	11585	-7	11580	-7	11575	-7	11570	-6
11565	-8	11560	-6	11555	-4	11550	-5	11545	-7	11540	-9	11535	-8	11530	-6	11525	-3
11520	-3	11515	-3	11510	-4	11505	-4	11500	-2	11495	-1	11490	-1	11485	-3	11480	-4
11475	-3																

AVERAGE = -0.66027E-02 DISCREPANCE = 0.91368E-02 MAX X = 1204.5 MAX Y = -0.02100

AVERAGE, DISCREPANCE, AND MAX Y ARE IN UNITS OF TRANSMITTANCE.

NOISE ERROR

ORDINATES ARE ABSOLUTE TRANSMITTANCE X 1000.0

12500	0.0	12495	0.2	12490	0.0	12485	-0.1	12480	0.0	12475	-0.3	12470	0.3	12465	-0.1
12460	0.2	12455	0.0	12450	-0.4	12445	0.1	12440	0.1	12435	0.3	12430	-0.4	12425	0.4
12420	-0.3	12415	0.3	12410	-0.5	12405	0.2	12400	0.0	12395	0.3	12390	-0.2	12385	0.1
12380	-0.1	12375	-0.2	12370	0.3	12365	-0.3	12360	0.0	12355	-0.1	12350	0.3	12345	-0.1
12340	0.2	12335	-0.4	12330	0.2	12325	-0.2	12320	0.1	12315	0.2	12310	0.0	12305	0.0
12300	-0.3	12295	0.0	12290	0.3	12285	0.1	12280	-0.5	12275	0.2	12270	0.0	12265	0.1
12260	0.2	12255	-0.3	12250	0.2	12245	-0.1	12240	0.3	12235	0.1	12230	-0.3	12225	0.1
12220	0.1	12215	0.2	12210	0.3	12205	-0.5	12200	-0.1	12195	0.1	12190	0.1	12185	-0.4
12180	-0.1	12175	0.2	12170	0.3	12165	0.1	12160	0.1	12155	-0.3	12150	0.2	12145	0.0
12140	-0.1	12135	-0.1	12130	0.3	12125	-0.1	12120	0.1	12115	0.2	12110	-0.3	12105	-0.1
12100	0.0	12095	0.0	12090	-0.1	12085	0.4	12080	0.0	12075	-0.5	12070	0.3	12065	-0.3
12060	0.5	12055	-0.2	12050	0.0	12045	-0.2	12040	-0.1	12035	0.1	12030	0.2	12025	0.0
12020	0.0	12015	-0.3	12010	0.3	12005	-0.1	12000	0.0	11995	0.1	11990	-0.3	11985	0.2
11980	0.2	11975	-0.3	11970	0.1	11965	-0.2	11960	0.3	11955	-0.1	11950	-0.1	11945	0.0
11940	-0.2	11935	0.2	11930	0.0	11925	0.3	11920	-0.5	11915	0.4	11910	-0.4	11905	0.3
11900	0.0	11895	0.0	11890	-0.2	11885	0.3	11880	-0.4	11875	0.3	11870	-0.1	11865	0.0
11860	0.0	11855	-0.2	11850	0.3	11845	0.2	11840	-0.3	11835	-0.3	11830	0.3	11825	0.1
11820	-0.1	11815	0.1	11810	-0.2	11805	0.0	11800	0.2	11795	0.0	11790	-0.3	11785	0.3
11780	0.0	11775	-0.1	11770	0.0	11765	-0.3	11760	0.3	11755	0.1	11750	0.2	11745	-0.3
11740	-0.3	11735	0.3	11730	0.0	11725	0.1	11720	0.0	11715	0.0	11710	-0.3	11705	0.1
11700	-0.1	11695	0.3	11690	0.1	11685	0.0	11680	-0.1	11675	-0.3	11670	0.3	11665	-0.3
11660	0.6	11655	-0.3	11650	0.1	11645	-0.3	11640	0.3	11635	-0.2	11630	0.2	11625	-0.1
11620	0.0	11615	0.0	11610	0.0	11605	0.1	11600	-0.2	11595	0.2	11590	-0.3	11585	0.3
11580	0.0	11575	0.0	11570	0.0	11565	-0.3	11560	-0.1	11555	0.4	11550	-0.1	11545	0.2
11540	-0.4	11535	0.1	11530	-0.1	11525	0.3	11520	-0.3	11515	0.3	11510	-0.2	11505	-0.1
11500	0.0	11495	0.0	11490	0.3	11485	0.1								

AVERAGE = 0.27460E-05

DISCREPANCE = 0.22315E-03

MAX X = 1166.0

MAX Y = 0.00060

CURVE MISFIT ERROR.-----

ORDINATES ARE ABSOLUTE TRANSMITTANCE X 1000.0

12500	-8.7	12495	-8.5	12490	-8.7	12485	-8.9	12480	-8.3	12475	-6.5	12470	-4.4	12465	-3.0
12460	-2.9	12455	-3.3	12450	-2.6	12445	0.2	12440	3.6	12435	4.9	12430	4.3	12425	2.6
12420	0.3	12415	-2.3	12410	-3.6	12405	-2.9	12400	-1.3	12395	-1.0	12390	-1.9	12385	-3.1
12380	-4.0	12375	-3.6	12370	-2.7	12365	-1.4	12360	-0.3	12355	1.3	12350	1.7	12345	-0.2
12340	-3.9	12335	-6.7	12330	-7.2	12325	-5.9	12320	-3.8	12315	-2.5	12310	-2.8	12305	-3.9
12300	-3.9	12295	-2.9	12290	-2.3	12285	-3.2	12280	-3.2	12275	-1.6	12270	1.4	12265	3.7
12260	4.8	12255	5.5	12250	6.7	12245	8.1	12240	7.8	12235	5.7	12230	3.7	12225	2.7
12220	2.1	12215	-0.2	12210	-4.3	12205	-8.7	12200	-10.6	12195	-9.4	12190	-7.1	12185	-3.7
12180	2.3	12175	8.5	12170	12.2	12165	11.7	12160	7.9	12155	3.5	12150	0.9	12145	-0.3
12140	-0.6	12135	-0.3	12130	0.0	12125	-0.9	12120	-3.3	12115	-7.0	12110	-10.9	12105	-12.7
12100	-12.1	12095	-9.9	12090	-8.2	12085	-8.1	12080	-10.2	12075	-12.7	12070	-13.9	12065	-14.2
12060	-15.0	12055	-17.3	12050	-19.8	12045	-20.7	12040	-19.3	12035	-16.8	12030	-15.3	12025	-15.1
12020	-15.7	12015	-16.1	12010	-16.0	12005	-16.0	12000	-16.1	11995	-15.8	11990	-15.0	11985	-14.2
11980	-13.9	11975	-14.1	11970	-13.8	11965	-12.9	11960	-12.3	11955	-12.9	11950	-13.9	11945	-14.0
11940	-12.8	11935	-11.2	11930	-10.0	11925	-10.3	11920	-10.2	11915	-9.7	11910	-8.5	11905	-8.4
11900	-8.7	11895	-10.3	11890	-11.5	11885	-12.6	11880	-12.2	11875	-11.7	11870	-10.6	11865	-10.3
11860	-9.7	11855	-9.2	11850	-9.0	11845	-10.2	11840	-12.0	11835	-12.5	11830	-11.3	11825	-10.3
11820	-10.7	11815	-11.1	11810	-11.1	11805	-10.7	11800	-10.3	11795	-9.9	11790	-10.0	11785	-10.0
11780	-10.1	11775	-9.9	11770	-8.9	11765	-7.0	11760	-5.0	11755	-4.2	11750	-5.2	11745	-6.7
11740	-6.7	11735	-5.2	11730	-4.3	11725	-4.8	11720	-6.1	11715	-7.0	11710	-6.7	11705	-5.1
11700	-2.9	11695	-2.3	11690	-4.1	11685	-7.9	11680	-12.2	11675	-14.4	11670	-14.3	11665	-12.7
11660	-12.6	11655	-13.7	11650	-15.1	11645	-14.7	11640	-13.3	11635	-11.8	11630	-11.2	11625	-10.9
11620	-11.0	11615	-11.0	11610	-11.0	11605	-11.1	11600	-10.8	11595	-10.2	11590	-8.7	11585	-7.4
11580	-6.7	11575	-7.3	11570	-7.9	11565	-7.7	11560	-5.9	11555	-4.4	11550	-4.9	11545	-7.2
11540	-8.6	11535	-8.2	11530	-5.7	11525	-3.6	11520	-2.7	11515	-3.3	11510	-3.9	11505	-3.7
11500	-2.3	11495	-0.9	11490	-1.3	11485	-2.8								

AVERAGE = -0.66262E-02

DISCREPANCE = 0.91124E-02

MAX X = 1204.5

MAX Y = -0.02066

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SUMMARY

Three computer programs for fitting infrared band contours are described and listed. These programs utilize Cauchy (Lorentz), Gauss, Cauchy-Gauss product, and Cauchy-Gauss sum functions, and will optimize the parameters for fitting single bands or multiple overlapping band systems using a non-linear least squares algorithm.

Supplementary programs are included for the evaluation of the half-widths and shape characteristics of the synthesized component bands, also for the computation of the ordinates of the synthesized band envelope, and for an analysis of the misfit with the true spectrum. This latter program also serves as a general purpose program for subtracting spectral ordinates.

The programs are written in FORTRAN IV. They are designed for card input and output in a standardized format that facilitates their interfacing with other programs developed in our laboratory for the numerical analysis of infrared and ultraviolet spectrophotometric absorption curves.