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### Ultrasonic evaluation of friction stir welds and dissimilar intermixing using synthetic aperture focusing technique

Lévesque, D.; Toubal, L.; Cao, X.; Dubourg, L.

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## **Ultrasonic evaluation of friction stir welds and dissimilar intermixing using synthetic aperture focusing technique**

D. Lévesque<sup>1</sup>, L. Toubal<sup>1</sup>, X. Cao<sup>2</sup> and L. Dubourg<sup>2</sup>

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Friction stir welding (FSW) is a recently developed solid-state joining process that uses a specially shaped rotating tool to produce lap or butt joints. At the National Research Council, an inter-institute collaboration was started in 2007 with the goal of exploiting the NDE expertise and applying it for the characterization of friction stir welds for various industrial applications. In particular, very good performance was obtained using ultrasonic immersion or laser-ultrasonics combined with the synthetic aperture focusing technique (SAFT) for detecting lack of penetration in butt joints, discontinuities such as wormholes and hooking in lap joints. Dissimilar metal welds of aluminum and magnesium by FSW are also considered for automotive and aerospace applications. Complex vortex flows are produced during the FSW process that may create intercalated lamellar structures with the possible formation of intermetallic compounds, causing variable hardness and degradation in mechanical properties. A modified version of SAFT that takes into account the difference of ultrasonic velocity in the joint between that of Al and Mg has been developed to study the dissimilar intermixing. Welded samples in the butt configuration with different welding speeds and seam offsets are tested using the immersion technique with the modified SAFT. Results will be presented for both defect detection and weld characterization, and the capabilities and limitations will be discussed.

**Submitted to:** Signal processing for NDT

# NDT in Canada 2009

## *Ultrasonic evaluation of friction stir welds and dissimilar intermixing using synthetic aperture focusing technique*

D. Lévesque<sup>1</sup>, L. Toubal<sup>1</sup>,  
X. Cao<sup>2</sup> and L. Dubourg<sup>2</sup>

<sup>1</sup>Industrial Materials Institute, Boucherville, Qc

<sup>2</sup>Aerospace Manufacturing Technology Centre, Montréal, Qc  
National Research Council Canada



# NDT in Canada 2009

## Agenda

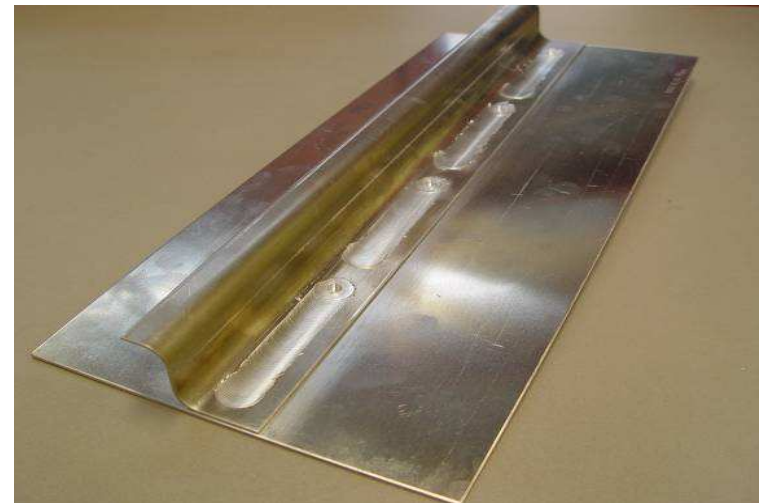
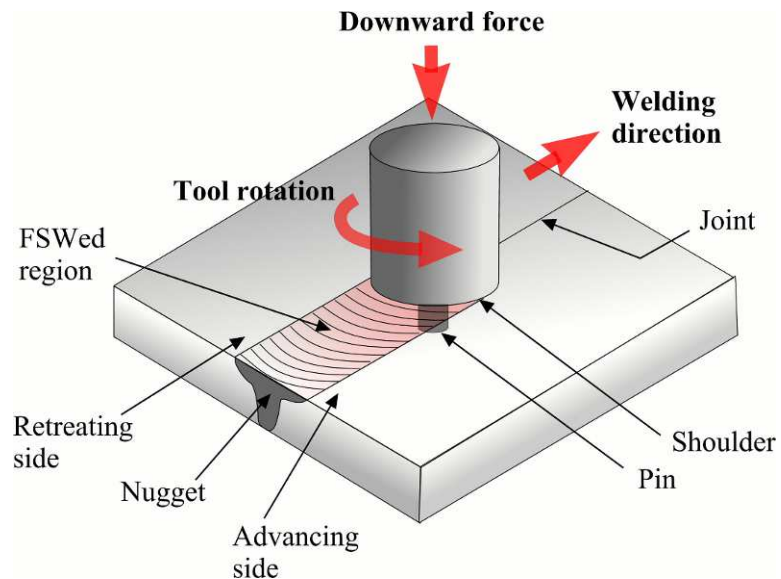
- Friction stir welding (FSW)
- SAFT imaging
  - principles
  - improvements
- Results
  - Lap joints, butt joints
  - Dissimilar metal welds
- Comparison with destructive methods



# NDT in Canada 2009

## Friction stir welding

- Manufacturing of aircraft panels
- Rivet replacement: saving of weight, productivity and aerodynamics
- Some challenges: hooking, lack of penetration, wormholes, kissing bond



# NDT in Canada 2009

## Material flow

### Low k: hot condition (overstirring)

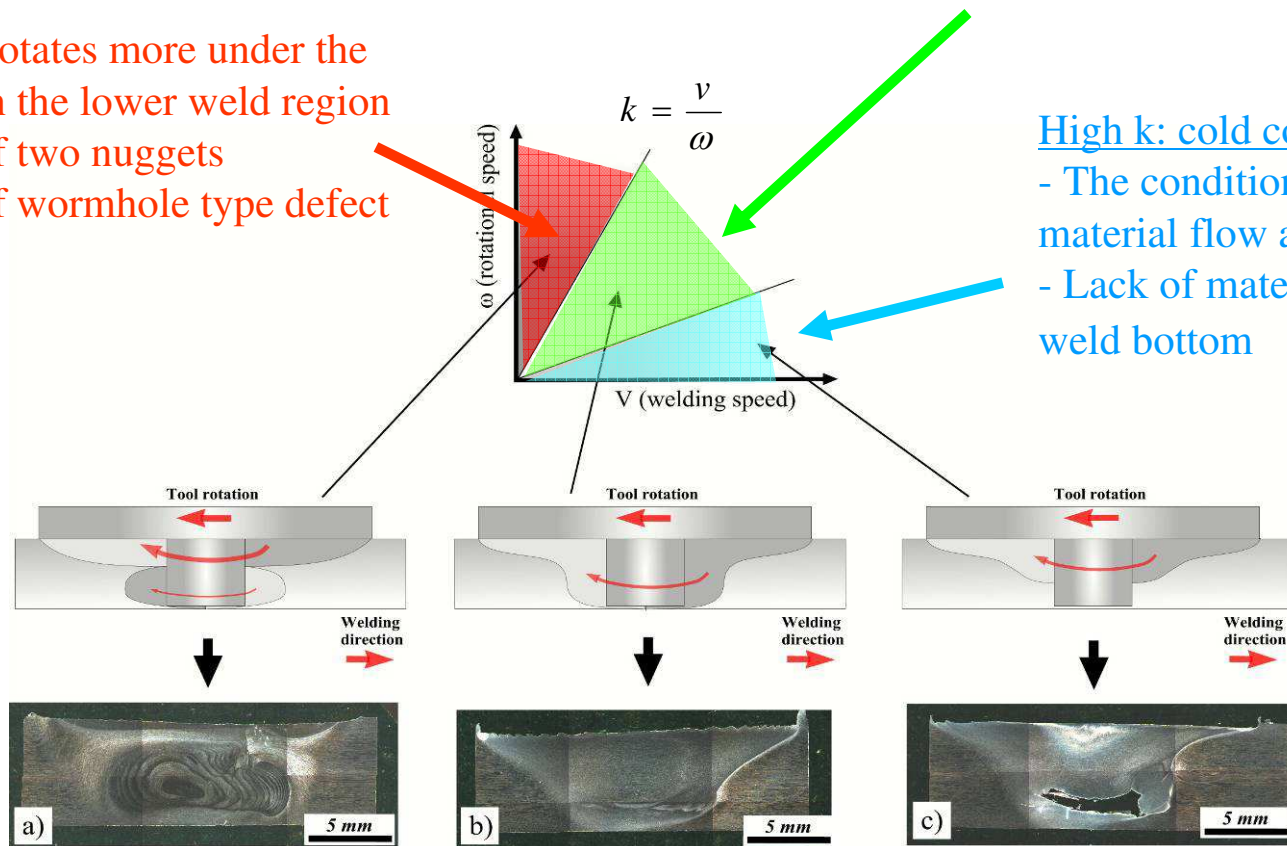
- High heat generation and stirring under the shoulder
- The material rotates more under the shoulder than in the lower weld region
- Appearance of two nuggets
- Appearance of wormhole type defect

### Intermediate k: stable condition

- The flow of the boundary layer is stable
- Sound and defect-free weld

### High k: cold condition

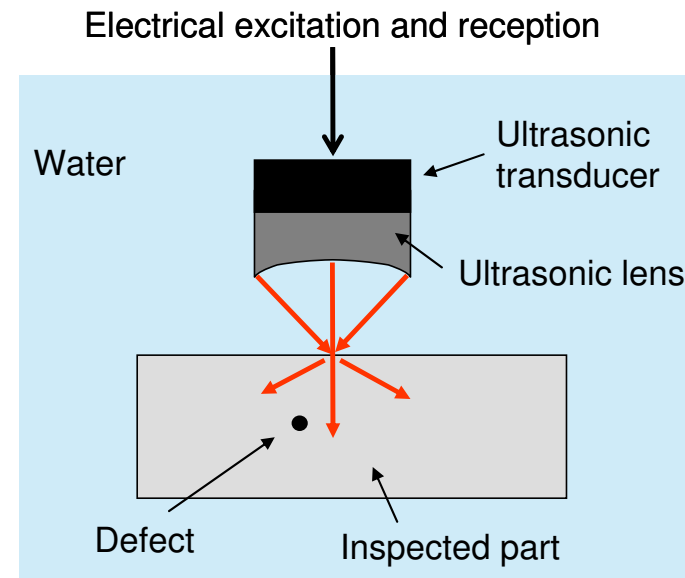
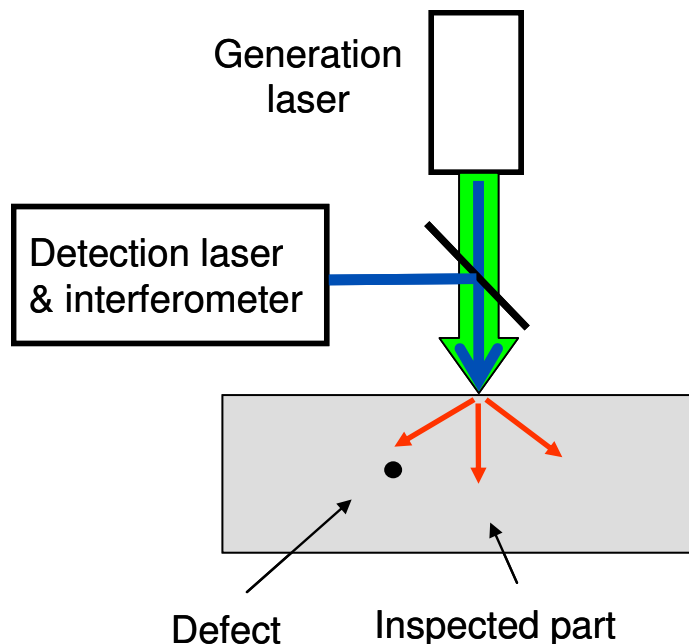
- The conditions for stable material flow are not reached
- Lack of material feeding in the weld bottom



# NDT in Canada 2009

## Synthetic aperture focusing technique (SAFT)

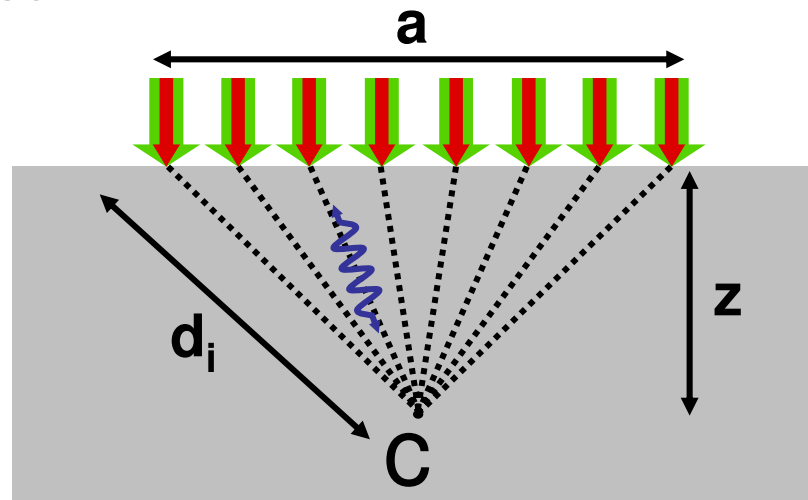
- Source of ultrasound and detection zone overlap at the surface of the part
- Laser-ultrasonics or conventional piezoelectric transducer focused on the surface
- Mechanical scanning along two axis (can also use a transducer array for one or two-axis scan)
- Numerical acquisition of all the A-scans



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## Time domain SAFT

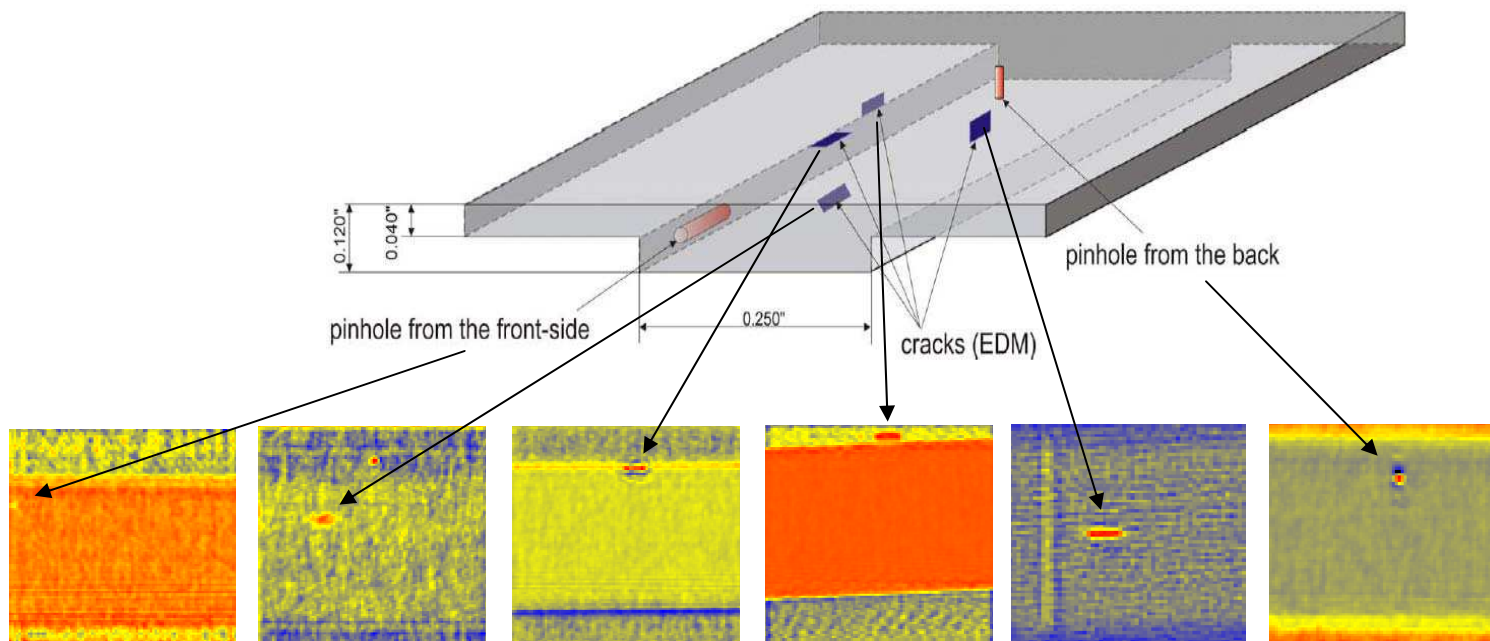
- For any point C in the volume:
  - 1- Locate the amplitude of each signal at time  $2d_i/v$
  - 2- Sum the contributions in the aperture a
- Large amplitude obtained if a flaw is located at C; otherwise, a reduction of noise.



- In practice, computation in the Fourier domain: F-SAFT

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## Sample with artificial defects



Thickness: 3 mm

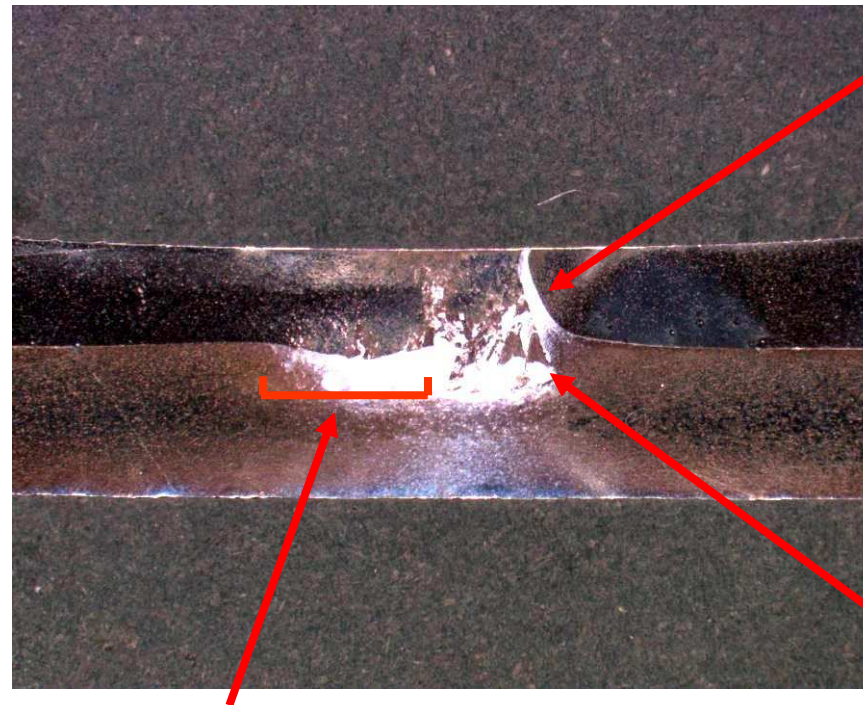
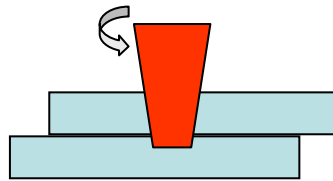
Pin holes: 0.5 mm dia; EDM slots: 0.175 mm width



# NDT in Canada 2009

## FSW lap joint

- Al sample, 4 mm thick



**Defect: large hooking on AS**

7075 1,5-mm plate

2024 2,5-mm plate

**Defect: wormhole**

**Defect: kissing-bond on RS**

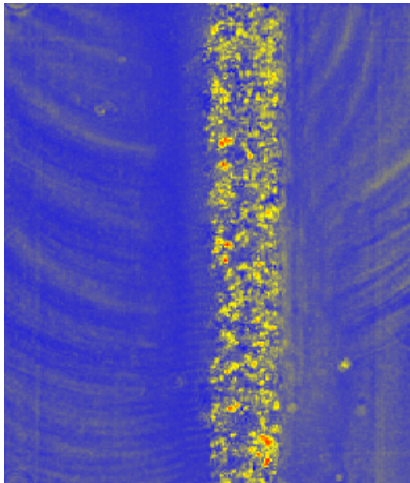
RS: retreating side  
AS: advancing side



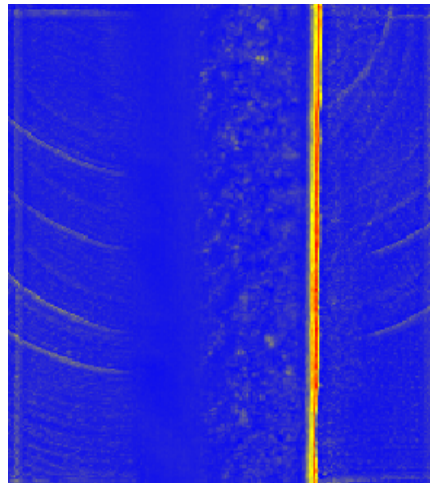
# NDT in Canada 2009

## SAFT results: tool side

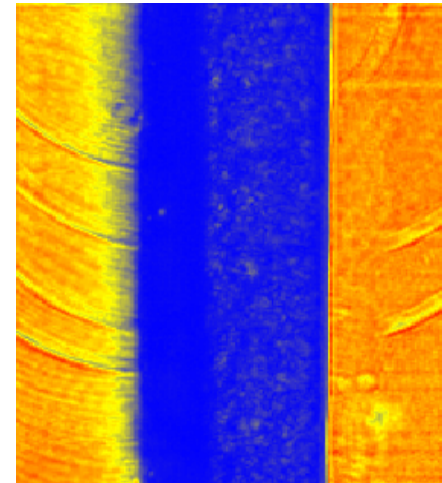
C-scan 0.8 mm  
*above* interface



C-scan 0.25 mm  
*above* interface



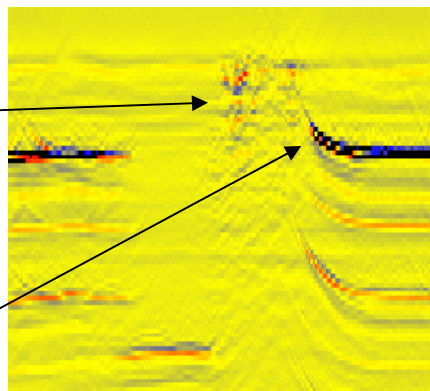
C-scan (slice) at  
interface



B-scan across  
the weld

wormhole  
related

hooking



← interface

← secondary  
echoes

← backwall



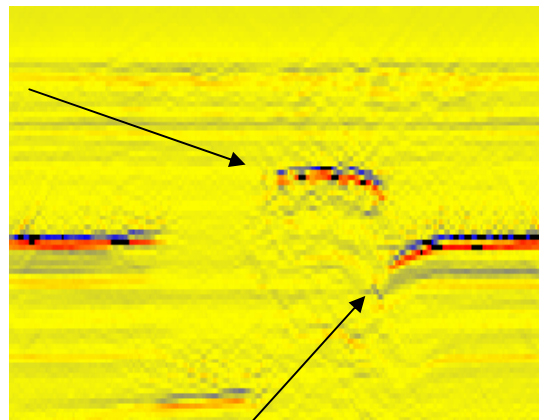
# NDT in Canada 2009

## SAFT results: opposite side

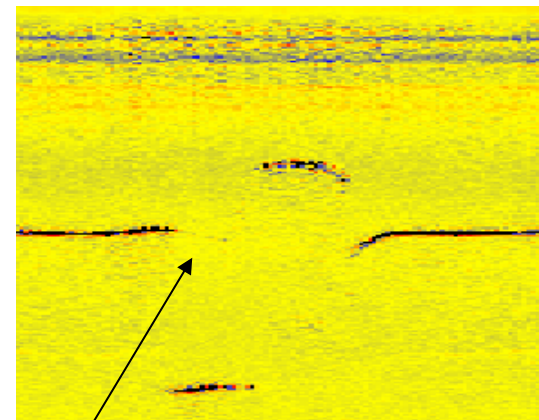
Immersion  
Frequency up to 50 MHz

Laser-ultrasonics  
Frequency up to 220 MHz

wormhole  
B-scan across  
the weld



hooking

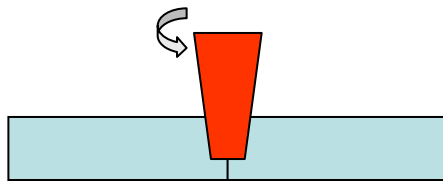


kissing bond

# NDT in Canada 2009

## FSW butt joint

- Al sample, 2 mm thick



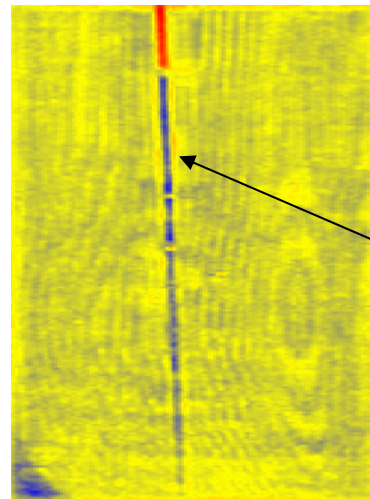
LOP height: 600  $\mu\text{m}$

LOP width: 10  $\mu\text{m}$

# NDT in Canada 2009

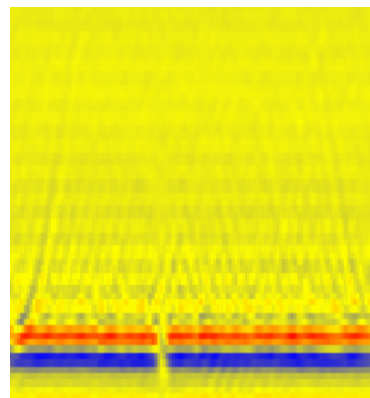
## SAFT results: tool side

C-scan (slice)  
near bottom face



Lack of penetration

B-scan across  
the weld



Backwall



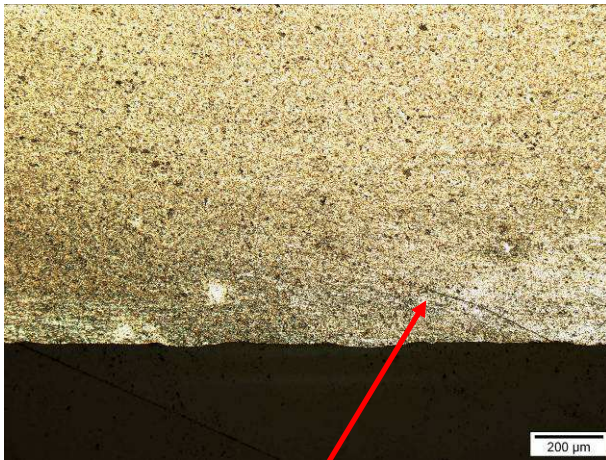
# NDT in Canada 2009

## Sample with variable pin length

Al sample  
2.56 mm thick (0.1 inch)

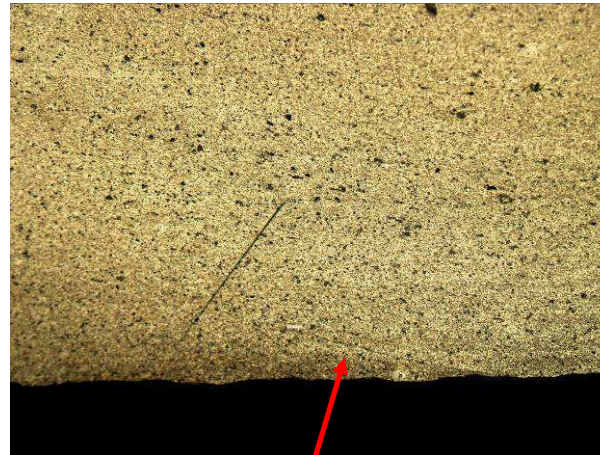


Pin penetration= 1.9 mm



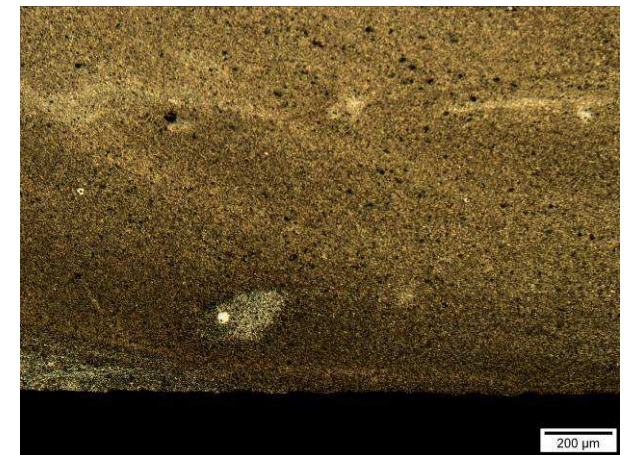
Lack of penetration

Pin penetration= 2.1 mm



Small lack of penetration

Pin penetration= 2.2 mm



Full penetration

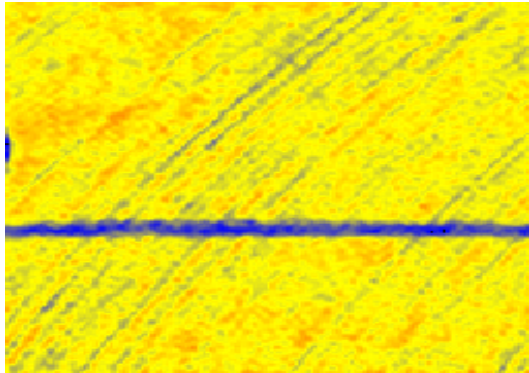
➤ No visible defect for a pin penetration  $\geq 2.2$  mm



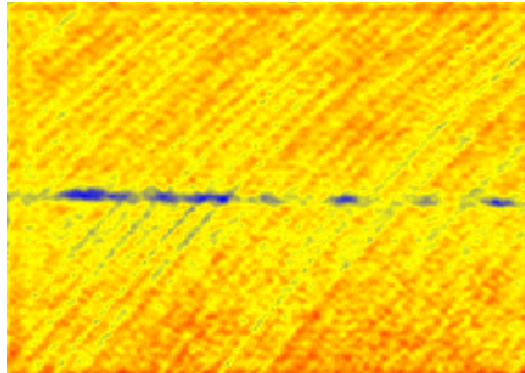
# NDT in Canada 2009

## SAFT results: tool side

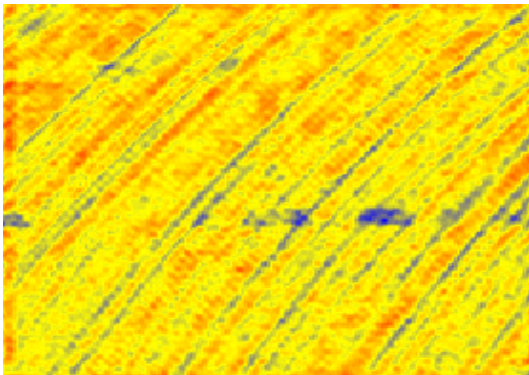
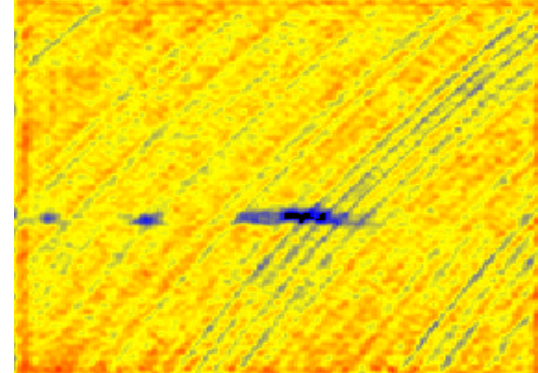
1.4 mm



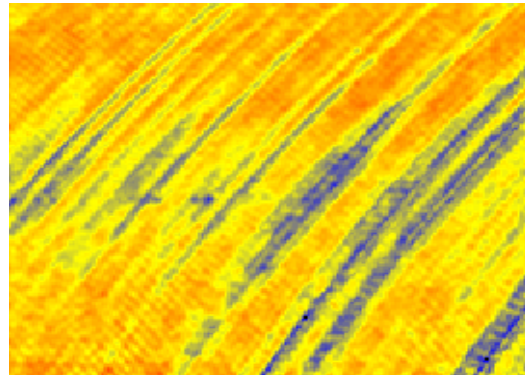
1.6 mm



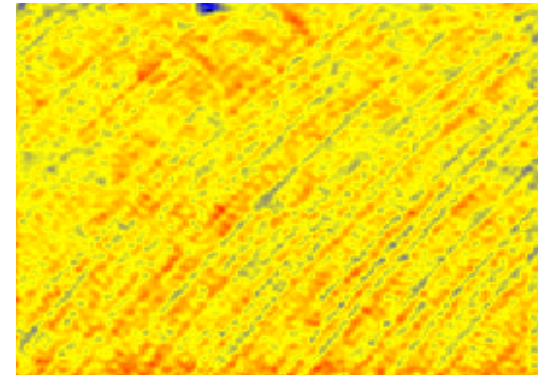
1.8 mm



2.0 mm



2.1 mm



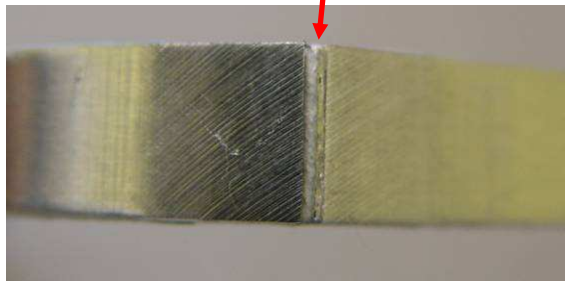
2.2 mm



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## Bend test results

Failure



1.25 to 1.3 mm

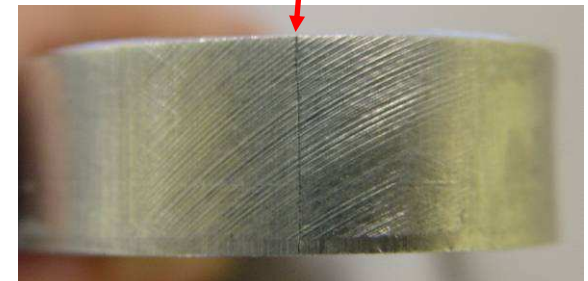
Failure



1.45 to 1.5 mm

Small failures observed  
by microscopy

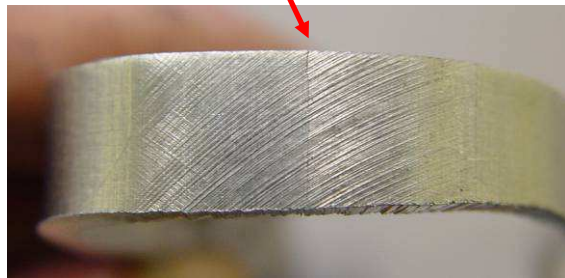
Failure



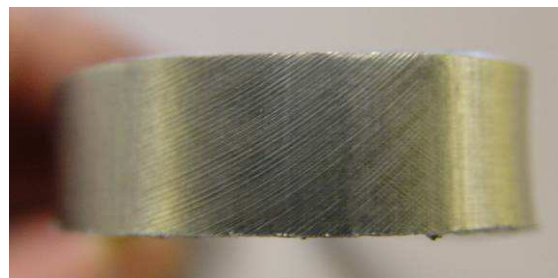
1.65 to 1.7 mm

Very small and irregular failures  
observed by microscopy

Failure



1.85 to 1.9 mm



1.95 to 2.0 mm



2.05 to 2.1 mm

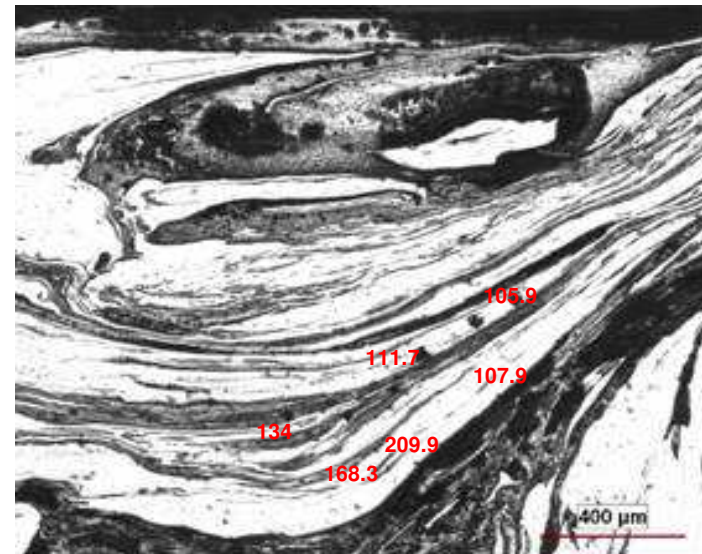
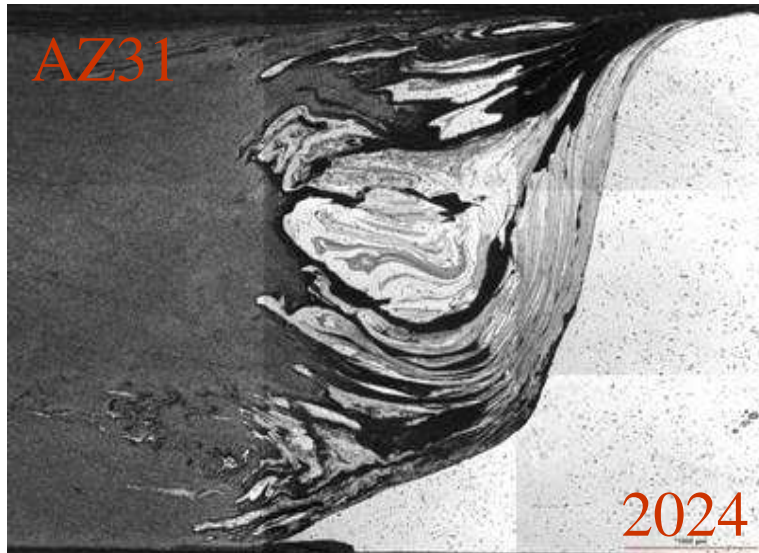
➤ No failure for a pin penetration  $\geq 2.14$  mm



# NDT in Canada 2009

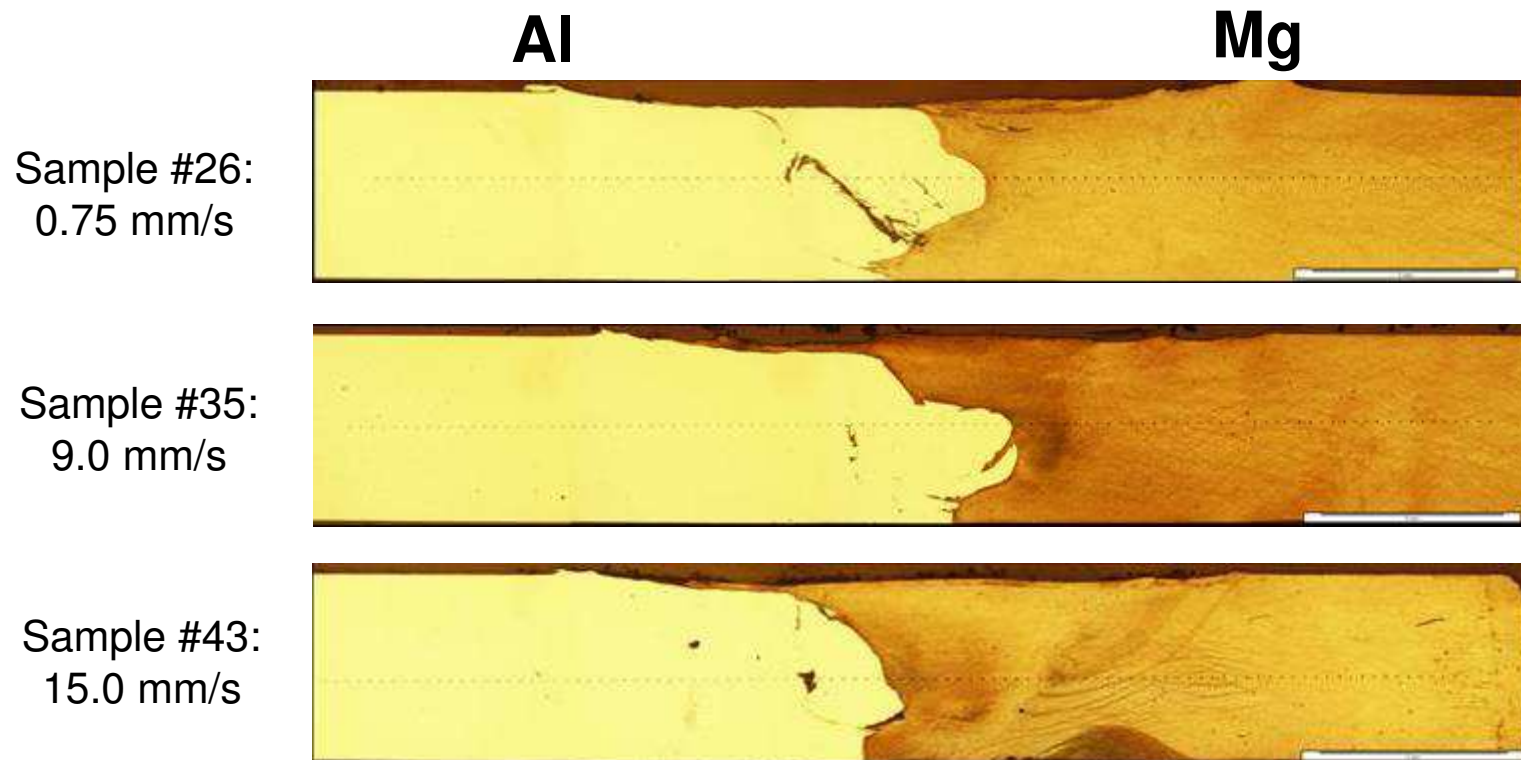
## Dissimilar FSW welds

- Determination of process parameters for FSW of butt joints Mg AZ31 and Al 2024.
- Complex vortex flow characterized by intercalated lamellar structure.
- High hardness probably due to the formation of  $\text{Al}_{12}\text{Mg}_{17}$ .
- Low hardness probably due to loose structure.



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## Effect of welding speed



Rotational speed: 250 RPM  
Thickness: 5 mm

$v \downarrow$ ,  $T \uparrow$ , intermetallic  $\uparrow$

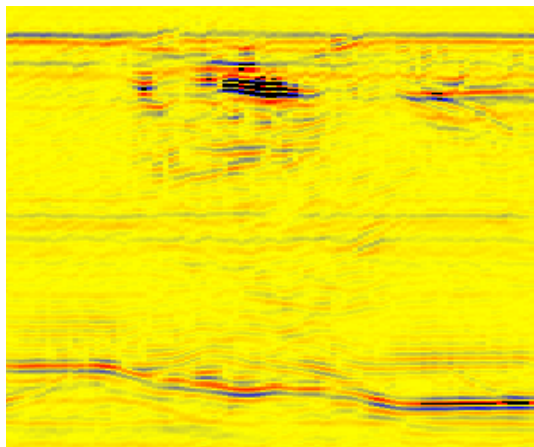


# NDT in Canada 2009

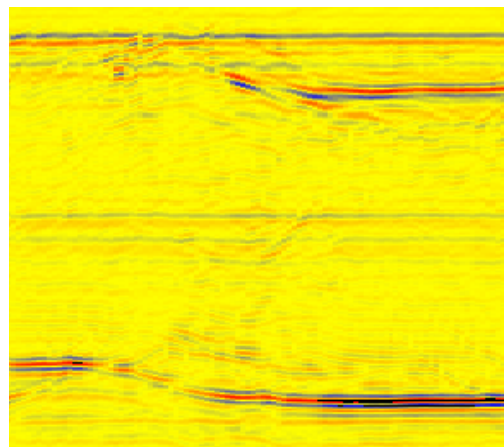
## Measurement: tool side

- B-scan

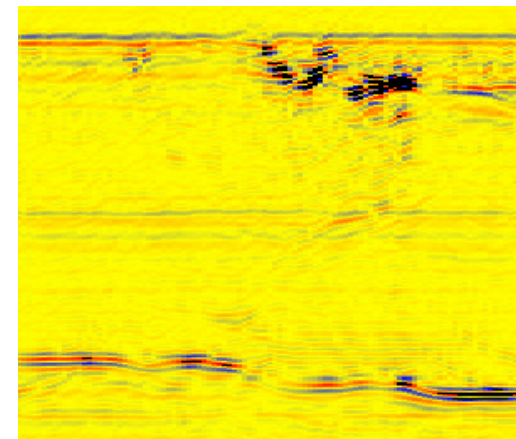
Line 20



Line 85



Line 110



Al (left) - Mg (right)

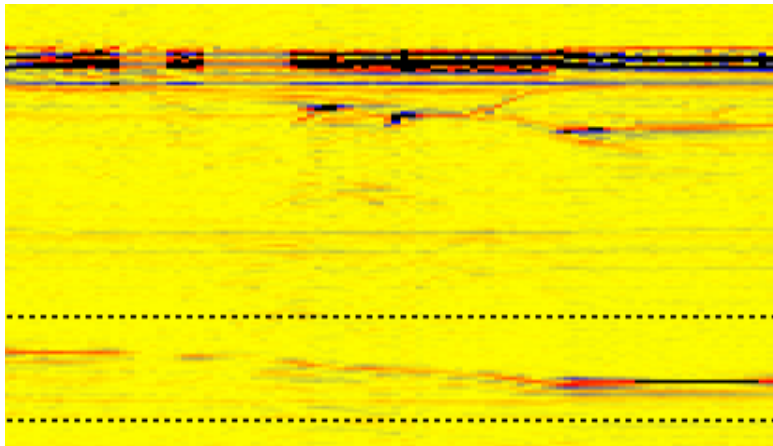
Scan: 10 mm wide, 20 mm along weld axis



# NDT in Canada 2009

## SAFT: improvements

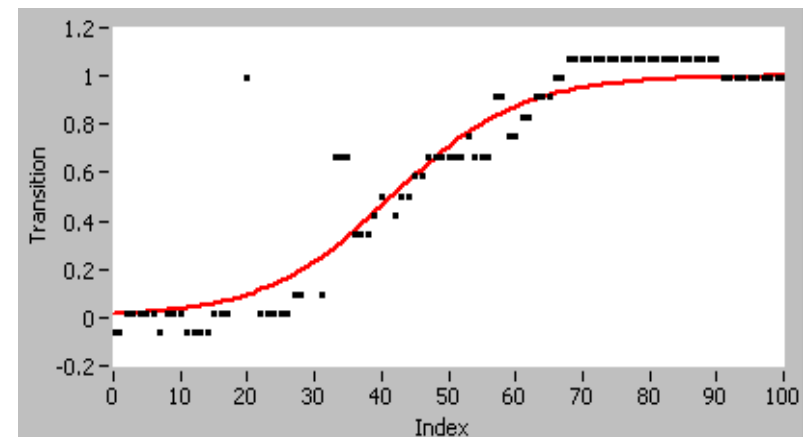
**B-scan:  
Butt joint, 5 mm thick**



**Al (left)  
6.4 mm/us**

**Mg (right)  
5.8 mm/us**

**Transition:  
Fit of the bottom echo**



This information from the backwall echo is used in the SAFT reconstruction

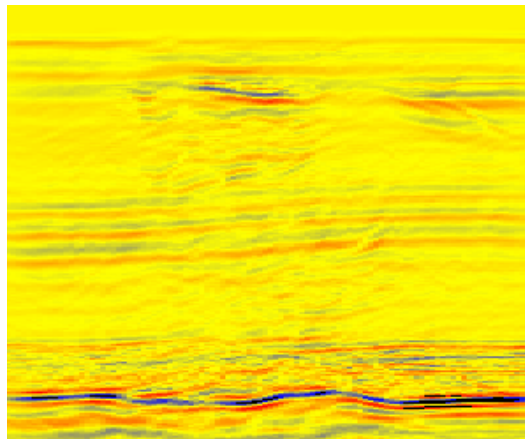


# NDT in Canada 2009

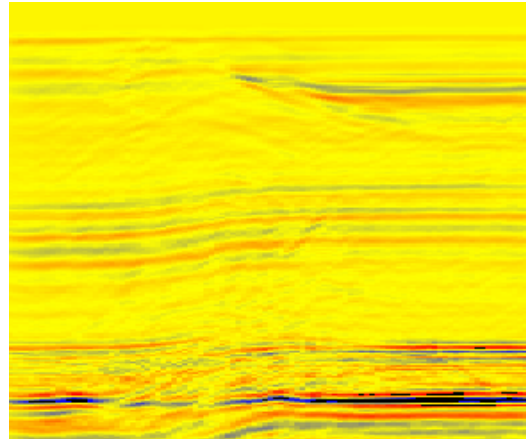
## SAFT results

- B-scan

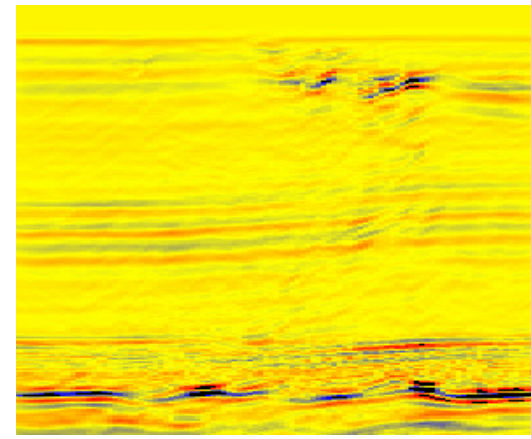
Line 20



Line 85



Line 110



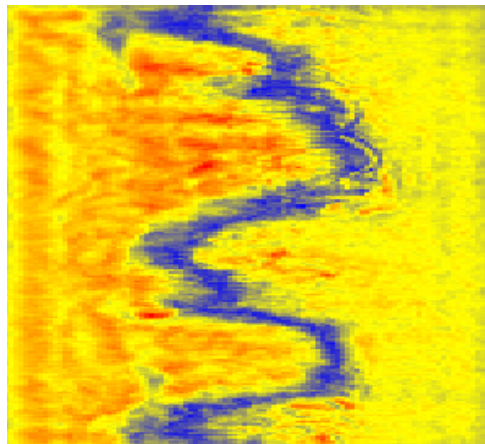
Al (left) - Mg (right)

# NDT in Canada 2009

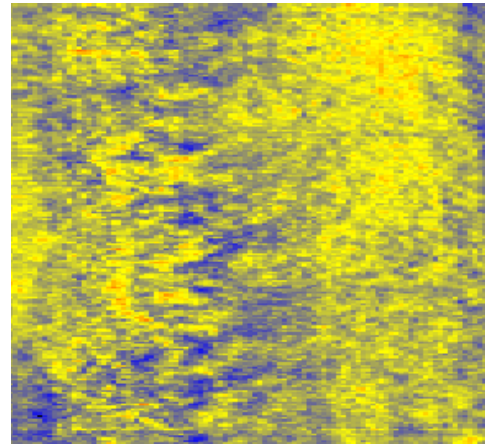
## SAFT results: mid-plane

- C-scan

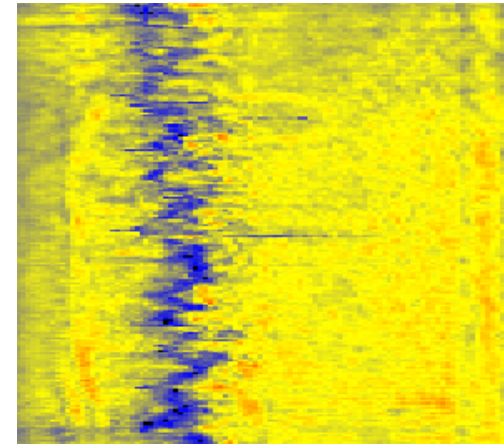
0.75 mm/s



9.0 mm/s



15.0 mm/s



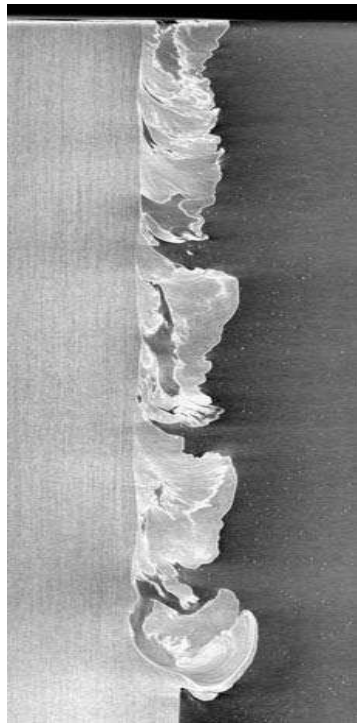
Al (left) - Mg (right)

# NDT in Canada 2009

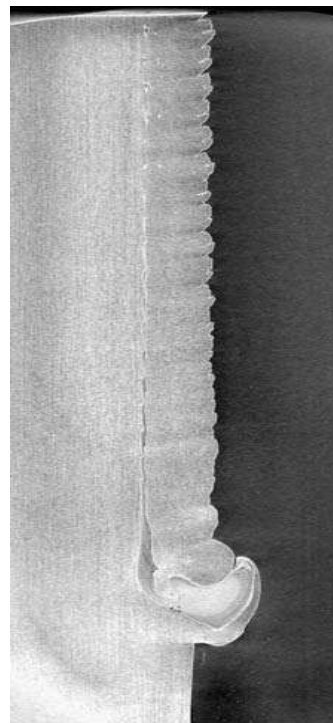
## Testing by Micro-CT

- Front views, mid-plane

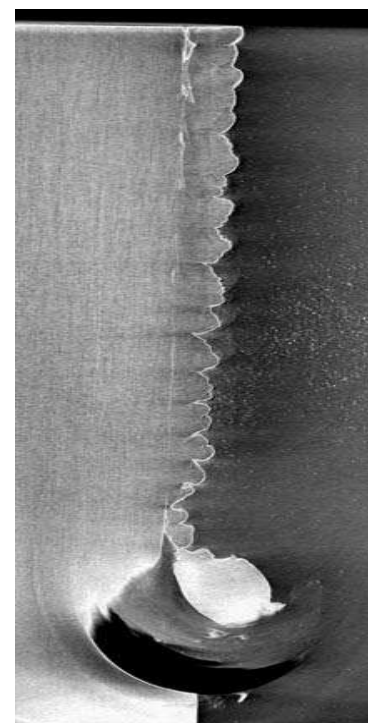
0.75 mm/s



9.0 mm/s



15.0 mm/s

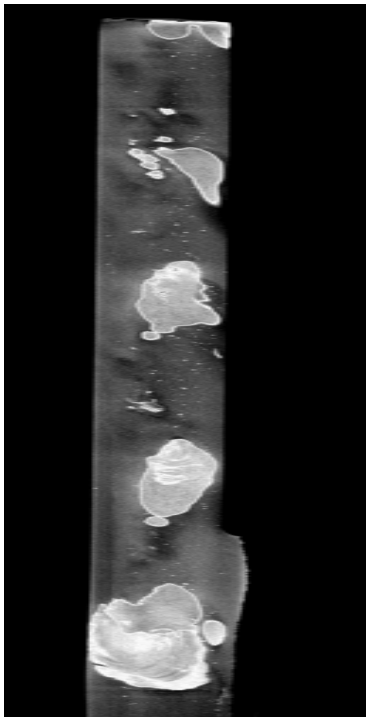


# NDT in Canada 2009

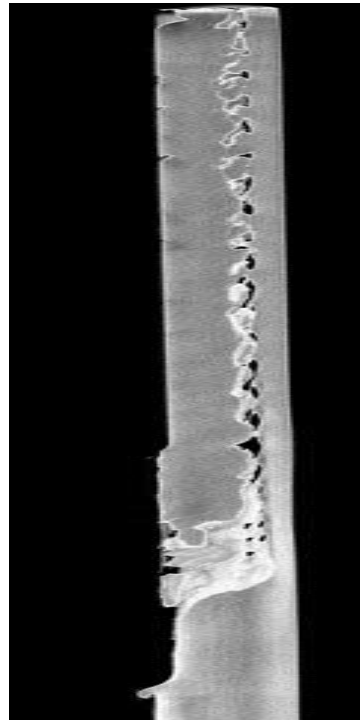
## Testing by Micro-CT

- Side views

0.75 mm/s



9.0 mm/s



15.0 mm/s



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## Conclusion

- Performance of SAFT demonstrated in different configurations of FSW. Ability to detect wormhole, hooking and lack of penetration.
- High frequency laser-ultrasonics seems to be able to detect kissing bond in FSW.
- Defect can be irregular: without NDE, many cross-sectional views required.
- SAFT can be modified to visualize material intermixing in dissimilar metal welds.



# NDT in Canada 2009

## References

1. D. Kleiner and C.R. Bird, "Signal processing for quality assurance in friction stir welds", *Insight*, Vol. 46, pp. 85-87, 2004.
2. S. Iwaki et al., Imperfections in friction stir welded zones and their precision non-destructive testing. Studies on characteristics of friction stir welded joints in structural thin aluminium alloys, *Welding Intern.* 20, pp. 197-205, 2006.
3. D. Lévesque, A. Blouin, C. Néron and J.-P. Monchalin, Performance of laser-ultrasonic F-SAFT imaging, *Ultrasonics* 40, pp. 1057-1063, 2002.
4. D. Lévesque et al., "Synthetic aperture focusing technique for the ultrasonic evaluation of friction stir welds", *Review of Progress in Quantitative NDE* Vol. 27, ed. by D.O. Thompson and D.E. Chimenti, AIP, New York, pp. 263-270, 2008.



# NDT in Canada 2009

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X. Cao and L. Dubourg

National Research Council Canada

*Thank You!*

